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## Non-dipole second order parameters of the photoelectron angular distribution for elements $Z = 1\text{--}100$ in the photoelectron energy range 1–10 keV

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### Abstract

Presented here are the photoelectron angular distribution non-dipole parameters associated with the terms of the second order  $O[(kr)^2]$  ( $k$  is the photon energy and  $r$  is the radius of the ionized atomic shell) for both unpolarized and linearly polarized radiation. The parameters are given for atomic shells with binding energies lower than 2 keV of all elements  $1 \leq Z \leq 100$  for four values of photoelectron energy in the range 1–10 keV. In this range, the second-order terms are shown to make a significant contribution (up to  $\sim 30\%$ ) to the angular differential cross section. The inclusion of these terms becomes all the more important in calculations of the differential cross section ratio for the fixed geometry of angles which is measured experimentally in the case of linearly polarized radiation. The Dirac–Fock–Slater potential is used in the calculations. The hole left by the emitted electron is taken into account in the frozen orbital approximation.

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## 1. Introduction

In recent publications [1,2], we presented extensive tables of the photoelectron angular distribution parameters  $\beta$ ,  $\gamma$ , and  $\delta$  together with the total photoionization cross section  $\sigma_i$  for all atomic shells with the binding energy  $\varepsilon < 2$  keV of all elements  $1 \leq Z \leq 100$  in the photoelectron energy range 0.1–5.0 keV. The parameter  $\beta$ , known popularly as “dipole,” allows one to describe the photoelectron angular distribution in the context of the electric dipole approximation. Two non-dipole parameters  $\gamma$  and  $\delta$  provide a means for the description of the photoelectron angular distribution with regard to the terms of the first order  $O(kr)$  where  $k$  is the photon energy and  $r$  is the average radius of the ionized atomic subshell. In the present work, we supplement these data by the parameters associated with terms of the order  $O[(kr)^2]$  in the photoelectron energy range 1–10 keV where the second-order terms may contribute significantly to the angular distribution.

With allowance made for the  $O(kr)$  terms, the photoelectron angular distribution is written [3] for unpolarized and circularly polarized radiation as

$$\frac{d\sigma_i}{d\Omega} = \frac{\sigma_i}{4\pi} \left[ 1 - \frac{\beta}{2} P_2(\cos \underline{\theta}) + \left( \frac{\gamma}{2} \sin^2 \underline{\theta} + \delta \right) \cos \underline{\theta} \right] \quad (1)$$

and for linearly polarized radiation in the form

$$\frac{d\sigma_i}{d\Omega} = \frac{\sigma_i}{4\pi} [1 + \beta P_2(\cos \theta) + (\gamma \cos^2 \theta + \delta) \sin \theta \cos \varphi]. \quad (2)$$

Here  $P_2(x)$  is the second order Legendre polynomial and the angles  $\underline{\theta}$ ,  $\theta$ , and  $\varphi$  are defined in Fig. 1.

The influence of the  $O(kr)$  terms on the differential cross section at a low photoelectron energy  $E$ , beginning with the photoionization threshold, as well as peculiarities of the parameters  $\beta$ ,  $\gamma$ , and  $\delta$  have been investigated in detail using different atomic models [3–8].

Recently it was found [9] that for the 2p-subshells of Ne, terms of the next order  $O[(kr)^2]$  make a noticeable contribution ( $\sim 10\%$ ) to the ratio of differential sections  $\zeta$  [see Eq. (36)] calculated at the fixed geometry of angles  $\theta$  and  $\varphi$  even at a fairly low photoelectron energy  $E \lesssim 2$  keV. The second order terms are associated mainly with quadrupole

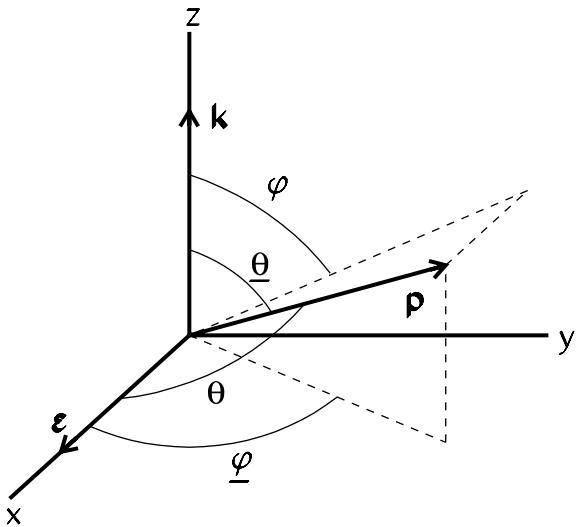


Fig. 1. Notations of angles and directions:  $\mathbf{k}$  is the photon momentum vector;  $\mathbf{p}$  is the direction of the photoelectron;  $\boldsymbol{\varepsilon}$  is the photon polarization vector;  $\underline{\theta}$  is the angle between vectors  $\mathbf{k}$  and  $\mathbf{p}$ ;  $\varphi$  is the angle between  $\boldsymbol{\varepsilon}$  and the plane passing through the  $z$ -axis and the vector  $\mathbf{p}$ ;  $\theta$  is the angle between  $\mathbf{p}$  and  $\boldsymbol{\varepsilon}$ ; and  $\varphi$  is the angle between  $\mathbf{k}$  and the plane passing through  $\mathbf{p}$  and  $\boldsymbol{\varepsilon}$ .

pole (the multipolarity of radiation field  $L = 2$ ) and octupole ( $L = 3$ ) amplitudes. Taking account of these terms requires an additional two parameters  $\Delta\beta_{\text{unp}}$  and  $\xi$  in the case of unpolarized radiation and four parameters  $\Delta\beta_{\ell p}$ ,  $\eta$ ,  $\mu$ , and  $\xi$  in the case of linearly polarized radiation. The parameters  $\Delta\beta_{\text{unp}}$  and  $\Delta\beta_{\ell p}$  are the second order corrections to the dipole parameter  $\beta$ .

The values of  $\Delta\beta_{\ell p}$ ,  $\eta$ ,  $\mu$ , and  $\xi$  for rare gas atoms were presented in [10]. The effect of the  $O[(kr)^2]$  terms on the intensity of the  $X$ -ray photoelectron spectra for photoionization of the 1s-, 2s-, 2p-, and 3d-shells of atoms with  $Z \leq 54$  in the photoelectron energy range 1–10 keV was studied in [11–13]. The calculations showed that the effect of the second order terms may be considerable, reaching 14% for the  $2p_{1/2}$ -shell of the Na atom and 24% for the  $3d_{3/2}$ -shell of the Zn atom at  $E = 10$  keV. For lower energy the contribution may be also noticeable, for example,  $\sim 10\%$  for the  $3d_{3/2}$ -shell of Zn at  $E = 5$  keV. Moreover, the ratio  $\zeta$  which is measured experimentally changes by  $\sim 50\%$  at  $E = 5$  keV and

a factor of two at  $E = 10$  keV for the  $3d_{3/2}$ -subshell of Zn. Such a considerable contribution has to be taken into account in calculations of the photoelectron angular distribution.

In Table 1 we present results for the parameters  $\Delta\beta_{\text{unp}}$ ,  $\Delta\beta_{\ell p}$ ,  $\eta$ ,  $\mu$ , and  $\xi$  associated with terms of the order  $O[(kr)^2]$  in the photoelectron angular distribution [see Eqs. (24) and (25)]. To prevent too great a bulk of data, we restrict ourselves to only four values of the photoelectron energy  $E = 1, 3, 5$ , and  $10$  keV. The energy  $E = 10$  keV was not included in [1,2]. Therefore, for this energy, parameters  $\sigma_i$ ,  $\beta$ ,  $\gamma$ , and  $\delta$  for all shells and elements under consideration are given in Table 2.

### 1.1. Basic formulas and method of calculation

The full relativistic treatment of the photoeffect leads to the following expressions for the differential cross section in the  $i$ th atomic subshell for unpolarized and linearly polarized radiation, respectively [14]

$$\frac{d\sigma_i}{d\Omega}(\underline{\theta}, \underline{\varphi}) = \frac{\sigma_i}{4\pi} \sum_n B_n P_n(\cos \underline{\theta}) \quad (3)$$

and

$$\frac{d\sigma_i}{d\Omega}(\underline{\theta}, \underline{\varphi}) = \frac{\sigma_i}{4\pi} \sum_n [B_n P_n(\cos \underline{\theta}) - B_n^{(2)} P_n^{(2)}(\cos \underline{\theta}) \cos 2\underline{\varphi}] \quad (4)$$

Here  $P_n(x)$  is the Legendre polynomial,  $P_n^{(2)}(x)$  is the associated Legendre polynomial, and the angle  $\underline{\varphi}$  is defined in Fig. 1. Coefficients  $B_n$  and  $B_n^{(2)}$  are double sums over multipoles  $\tau L$  of a radiation field:

$$B_n = \frac{4\pi^2\alpha}{k\sigma_i} \sum_{\tau_1 L_1, \tau_2 L_2} B_n(\tau_1 L_1 \tau_2 L_2), \quad (5)$$

$$B_n^{(2)} = \frac{4\pi^2\alpha}{k\sigma_i} \sum_{\tau_1 L_1, \tau_2 L_2} B_n^{(2)}(\tau_1 L_1 \tau_2 L_2), \quad (6)$$

$$B_0 = 1, \quad B_0^{(2)} = B_1^{(2)} = 0, \quad (7)$$

where  $\alpha = e^2/hc$  is the fine structure constant,  $\tau$  is the electric ( $\tau = E$ ) or magnetic ( $\tau = M$ ) type of transition, and  $B_n(\tau_1 L_1 \tau_2 L_2)$  and  $B_n^{(2)}(\tau_1 L_1 \tau_2 L_2)$  result from interference of amplitudes having multipoles  $\tau_1 L_1$  and  $\tau_2 L_2$ . Unless otherwise noted, we use relativistic units, that is,  $\hbar = m_0 = c = 1$ . The values of  $B_n^{(2)}(\tau_1 L_1 \tau_2 L_2)$  and  $B_n(\tau_1 L_1 \tau_2 L_2)$  are related as

$$B_n^{(2)}(\tau_1 L_1 \tau_2 L_2) = (-1)^{L_1 + \ell_1 + \ell_2} \frac{C_{L_1 - 1, L_2 - 1}^{n-2}}{C_{L_1, L_2}^{n-2}} \times \sqrt{\frac{(n-2)!}{(n+2)!}} B_n(\tau_1 L_1 \tau_2 L_2), \quad (8)$$

where  $\ell$  is the electron orbital momentum and  $C_{j_1 m_1 j_2 m_2}^{JM}$  is the Clebsch–Gordan coefficient. The terms  $B_n(\tau_1 L_1 \tau_2 L_2)$  of the order  $O[(kr)^m]$  with  $m \leq 2$  are written as follows. The dipole electric term of the order  $O(1)$  is

$$B_2(E1E1) = -\sqrt{6} \sum_{\kappa_1 \kappa_2} A_2 W(11j_1 j_2; 2j_i) Q_{01}(\kappa_1) Q_{01}(\kappa_2). \quad (9)$$

Terms of the first order  $O(kr)$  are:

$$B_1(E1M1) = 6\sqrt{3} \sum_{\kappa_1 \kappa_2} A_1 W(11j_1 j_2; 1j_i) Q_{01}(\kappa_1) Q_{11}(\kappa_2), \quad (10)$$

$$B_1(E1E2) = 6\sqrt{3} \sum_{\kappa_1 \kappa_2} A_1 W(12j_1 j_2; 1j_i) Q_{01}(\kappa_1) Q_{12}(\kappa_2), \quad (11)$$

$$B_3(E1E2) = 6\sqrt{2} \sum_{\kappa_1 \kappa_2} A_3 W(12j_1 j_2; 3j_i) Q_{01}(\kappa_1) Q_{12}(\kappa_2). \quad (12)$$

Terms of the second order  $O[(kr)^2]$  are:

$$B_2[\mathcal{A}(E1E1)] = 2\sqrt{3} \sum_{\kappa_1 \kappa_2} A_2 W(11j_1 j_2; 2j_i) Q_{01}(\kappa_1) Q_{21}(\kappa_2), \quad (13)$$

$$B_2(M1M1) = -3\sqrt{\frac{3}{2}} \sum_{\kappa_1 \kappa_2} A_2 W(11j_1 j_2; 2j_i) Q_{11}(\kappa_1) Q_{11}(\kappa_2), \quad (14)$$

$$B_2(E1M2) = 10\sqrt{3} \sum_{\kappa_1 \kappa_2} A_2 W(12j_1 j_2; 2j_i) Q_{01}(\kappa_1) Q_{22}(\kappa_2), \quad (15)$$

$$B_2(M1E2) = -3\sqrt{30} \sum_{\kappa_1 \kappa_2} A_2 W(12j_1 j_2; 2j_i) Q_{11}(\kappa_1) Q_{12}(\kappa_2), \quad (16)$$

$$B_2(E2E2) = -\frac{15}{\sqrt{14}} \sum_{\kappa_1 \kappa_2} A_2 W(22j_1 j_2; 2j_i) Q_{12}(\kappa_1) Q_{12}(\kappa_2), \quad (17)$$

$$B_2(E1E3) = 8\sqrt{3} \sum_{\kappa_1 \kappa_2} A_2 W(13j_1 j_2; 2j_i) Q_{01}(\kappa_1) Q_{23}(\kappa_2), \quad (18)$$

$$B_4(E2E2) = -6\sqrt{\frac{10}{7}} \sum_{\kappa_1 \kappa_2} A_4 W(22j_1 j_2; 4j_i) Q_{12}(\kappa_1) Q_{12}(\kappa_2), \quad (19)$$

$$B_4(E1E3) = 12 \sum_{\kappa_1 \kappa_2} A_4 W(13j_1 j_2; 4j_i) Q_{01}(\kappa_1) Q_{23}(\kappa_2). \quad (20)$$

In Eqs. (9)–(20),  $j$  is the total momentum of the electron,  $\kappa = (\ell - j)(2j + 1)$  is the relativistic quantum number, and  $W(L_1 L_2 j_1 j_2; n j_i)$  is the Racah coefficient. The summation extends over all final states allowed by selection rules. The second order correction to the term  $B_2(E1E1)$  (Eq. (9)) arising from the interference of electric dipole amplitudes is specified by  $B_2[\mathcal{A}(E1E1)]$ . The coefficients  $A_n$  ( $n = 1, 2, 3, 4$ ) can be written as

$$A_n = \frac{4\pi^2\alpha}{k\sigma_i} (-1)^{j_1 + j_2 + |\kappa_i|} \sqrt{(2j_1 + 1)(2j_2 + 1)} C_{j_1, j_2}^{n-2} \times \begin{cases} \sin(\delta_{\kappa_1} - \delta_{\kappa_2}) & n = 1, 3 \\ \cos(\delta_{\kappa_1} - \delta_{\kappa_2}) & n = 2, 4. \end{cases} \quad (21)$$

Here  $\delta_{\kappa_1} - \delta_{\kappa_2}$  is the phase shift for the two final continuum states characterized by  $\kappa_1$  and  $\kappa_2$ . The reduced matrix element  $Q_{AL}(\kappa)$  has the form:

$$Q_{AL}(\kappa) = \sqrt{\frac{(2\bar{\ell}_\kappa + 1)(2\ell_i + 1)}{(2A + 1)}} C_{\bar{\ell}_\kappa 0 \ell_i 0}^{40} \mathcal{A} \begin{pmatrix} \bar{\ell}_\kappa & 1/2 & j_\kappa \\ \ell_i & 1/2 & j_i \\ A & 1 & L \end{pmatrix} R_{1A} \\ + \sqrt{\frac{(2\ell_\kappa + 1)(2\bar{\ell}_i + 1)}{(2A + 1)}} C_{\ell_\kappa 0 \bar{\ell}_i 0}^{40} \mathcal{A} \begin{pmatrix} \ell_\kappa & 1/2 & j_\kappa \\ \bar{\ell}_i & 1/2 & j_i \\ A & 1 & L \end{pmatrix} R_{2A}, \quad (22)$$

where  $\bar{\ell} = 2j - \ell$  and  $\mathcal{A} \begin{pmatrix} \ell_1 & 1/2 & j_1 \\ \ell_2 & 1/2 & j_2 \\ A & 1 & L \end{pmatrix}$  is the normalized coefficient of recoupling of four angular momenta. The radial integrals  $R_{1A}$  and  $R_{2A}$  are written as:

$$R_{1A} = \int_0^\infty G_i(r) F_\kappa(r) j_A(kr) dr, \quad (23)$$

$$R_{2A} = \int_0^\infty G_\kappa(r) F_i(r) j_A(kr) dr,$$

where  $j_A(kr)$  is the spherical Bessel function of order  $A$ , and  $G(r)$  and  $F(r)$  are the large and small components of the Dirac electron wavefunction multiplied by  $r$ . The initial bound electron state is denoted by index  $i$  as above. The index  $\kappa$  denotes the final continuum state. Methods of calculation of a bound and continuum wavefunction including the phase convention were described in detail in [15].

Furthermore, we keep in the sum (4) the terms of order no more than  $O[(kr)^2]$  and go from angles  $\underline{\theta}$  and  $\underline{\varphi}$  to  $\theta$  and  $\varphi$  in the case of linearly polarized radiation. Taking into account Eq. (8), one can obtain the convenient expression for the photoelectron angular distribution [9]

$$\frac{d\sigma_i}{d\Omega}(\theta, \varphi) = \frac{\sigma_i}{4\pi} [1 + (\beta + \Delta\beta_{\ell p}) P_2(\cos \theta) + (\gamma \cos^2 \theta + \delta) \sin \theta \cos \varphi + \eta P_2(\cos \theta) \cos 2\varphi + \mu \cos 2\varphi + \xi(1 + \cos 2\varphi) P_4(\cos \theta)]. \quad (24)$$

In a like manner, the following expression for the unpolarized radiation can be obtained:

$$\frac{d\sigma_i}{d\Omega}(\underline{\theta}) = \frac{\sigma_i}{4\pi} \left[ 1 - \frac{1}{2} (\beta + \Delta\beta_{\text{unp}}) P_2(\cos \underline{\theta}) + \left( \frac{\gamma}{2} \sin^2 \underline{\theta} + \delta \right) \cos \underline{\theta} + \xi P_4(\cos \underline{\theta}) \right]. \quad (25)$$

Table A

Terms  $B_2(\tau_1 L_1 \tau_2 L_2)$  and  $B_4(\tau_1 L_1 \tau_2 L_2)$  of the order  $O[(kr)^2]$  [Eqs. (13)–(20)], entering in coefficients  $B_2$  and  $B_4$

Z	Shell	E (keV)	$B_2(\tau_1 L_1 \tau_2 L_2)$						$B_4(\tau_1 L_1 \tau_2 L_2)$	
			$\Delta(E1E1)$	M1M1	E1M2	M1E2	E2E2	E1E3	E2E2	E1E3
29	2p <sub>1/2</sub>	1	3.67–4	−1.12–8	6.54–4	−2.63–5	2.06–3	6.32–4	−8.82–4	−1.16–3
		5	2.76–3	2.02–7	2.41–3	5.17–5	1.40–2	3.72–2	−1.71–2	−3.04–2
		10	4.75–3	8.23–7	5.03–3	3.35–4	2.92–2	8.86–2	−3.93–2	−6.12–2
54	3d <sub>3/2</sub>	1	4.16–4	7.52–8	−5.02–4	−7.21–5	2.03–3	−1.52–3	−2.56–4	7.80–4
		5	3.06–3	4.45–7	−1.62–3	2.37–5	1.83–2	3.92–2	−1.68–2	−2.65–2
		10	5.56–3	2.09–6	−3.06–3	5.74–4	4.04–2	1.11–1	−4.64–2	−6.09–2

The decimal order is given to the right of a value. For example, the value 3.67–4 is equal to 0.000367.

The parameters involved in Eqs. (24) and (25) are the following combinations of the terms  $B_n(\tau_1 L_1 \tau_2 L_2)$ . The dipole parameter  $\beta$  is

$$\beta = -2B_2(E1E1), \quad (26)$$

the non-dipole first-order parameters  $\gamma$  and  $\delta$  are:

$$\gamma = -5B_1(E1E2), \quad (27)$$

$$\delta = B_1(E1M1) + B_1(E1E2) + B_3(E1E2), \quad (28)$$

the non-dipole second order parameters  $\Delta\beta_{\text{unp}}$ ,  $\Delta\beta_{\ell p}$ ,  $\eta$ ,  $\mu$ , and  $\xi$  are:

$$\Delta\beta_{\text{unp}} = -2\{B_2(M1M1) + B_2[\Delta(E1E1)] + B_2(E1M2) + B_2(M1E2) + B_2(E2E2) + B_2(E1E3)\}, \quad (29)$$

$$\Delta\beta_{\ell p} = B_2(M1M1) - 2B_2[\Delta(E1E1)] - B_2(M1E2) + B_2(E2E2) - \frac{3}{4}B_2(E1E3), \quad (30)$$

$$\eta = -B_2(M1M1) - \frac{2}{3}B_2(E1M2) - \frac{1}{3}B_2(M1E2) - B_2(E2E2) - \frac{5}{12}B_2(E1E3) - \frac{5}{6}B_4(E2E2) - \frac{5}{6}B_4(E1E3), \quad (31)$$

$$\xi = B_4(E2E2) + B_4(E1E3), \quad (32)$$

$$\mu = -(n + \xi). \quad (33)$$

As evident from Eqs. (29)–(33), the parameters are related in the following way:

$$\Delta\beta_{\text{unp}} = \Delta\beta_{\ell p} - \frac{1}{2}(5\mu - \eta). \quad (34)$$

It should be noted that the small terms  $B_2(M1M1)$  and  $B_2(M1E2)$  have been ignored in papers [9,10]. In addition, there is no clear evidence whether or not the term  $B_2[\Delta(E1E1)]$  has been included. For reference, the second order terms  $B_2(\tau_1 L_1 \tau_2 L_2)$  and  $B_4(\tau_1 L_1 \tau_2 L_2)$  are listed in Table A. As seen from this table, the magnitudes of  $B_2(E2E2)$  and  $B_2(E1E3)$  are the largest, the dipole–octupole amplitude exceeding the quadrupole–quadrupole one at  $E \gtrsim 1$  keV. The magnitude of the term  $B_2[\Delta(E1E1)]$  is approximately of the same order as  $B_2(E1M2)$ . Of the two second-order terms  $B_4(E2E2)$  and  $B_4(E1E3)$ , the dipole–octupole term also exceeds the quadrupole–quadrupole one for all energies under consideration.

As revealed by the calculations, the parameters  $\Delta\beta_{\text{unp}}$ ,  $\Delta\beta_{\ell p}$ ,  $\eta$ ,  $\mu$ , and  $\xi$  depend monotonically on the energy at  $E \geq 1$  keV in many cases, for example, for all s-shells of light atoms with  $Z \lesssim 20$ , for p-shells of atoms with  $Z \lesssim 30$ , and for d-shells of atoms with  $Z \lesssim 50$ . Such  $E$ -de-

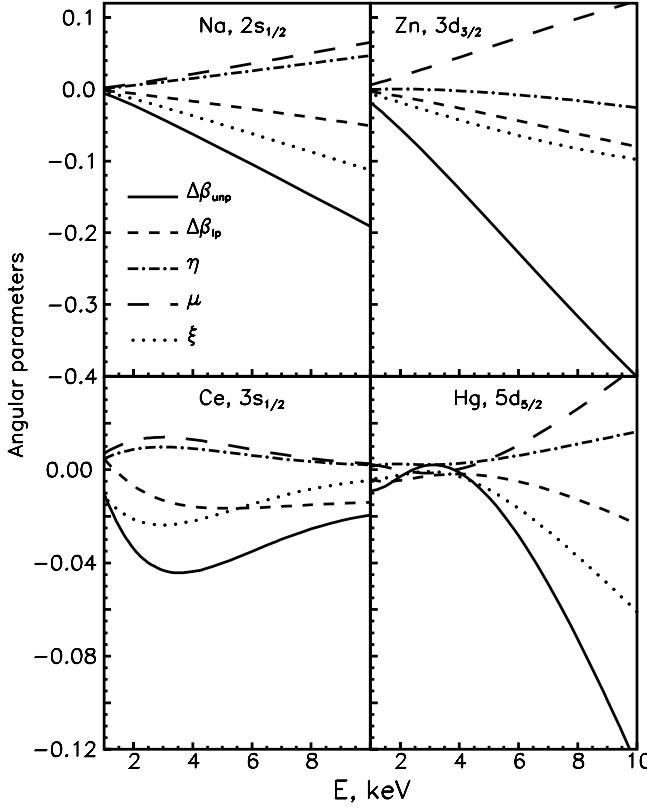


Fig. 2. The dependence of the second order parameters on the photoelectron energy  $E$ :  $\Delta\beta_{unp}$ , solid line;  $\Delta\beta_{lp}$ , short-dashed line;  $\eta$ , dot-dashed line;  $\mu$ , long-dashed line; and  $\xi$ , dot line.

pendence is shown at the top of Fig. 2 for the  $2s_{1/2}$ -shell of Na and the  $3d_{3/2}$ -shell of Zn. However sometimes, the  $E$ -dependence of some parameters may exhibit maxima and minima in the range  $E = 1–5$  keV as for the inner  $3s_{1/2}$ -shell of Ce and the outer  $5d_{5/2}$ -shell of Hg presented at the bottom of Fig. 2. Therefore we present the parameters for three values of the photoelectron energy in this region.

Calculations were performed within the one-electron approximation for a free atom with the standard electron configuration. We used the central Dirac–Fock–Slater potential with the coefficient  $C = 1$  in the approximate expression for the exchange term [16]. The exact consideration of the exchange interaction between electrons as well as the influence of electron correlations on the photoelectron angular distribution parameters were discussed in papers [4,7,10]. These effects were shown to be important at low photoelectron energies near the ionization threshold ( $E \lesssim 100$  eV). For the present calculations of the angular distribution parameters at photoelectron energy  $E \geq 1$  keV, the independent-particle Dirac–Fock–Slater model is quite adequate. The hole in the atomic subshell from which a photoelectron was emitted was taken into consideration in the framework of the frozen orbital approximation. The method of calculations is discussed at great length in paper [1]. Experimental values of the electron binding energies used in calculations are given in [1,2]. Computations were carried out by the use of the computer code package RAIN [17].

### 1.2. Influence of second order terms on the photoelectron angular distribution

Let us consider the total effect of terms of the order  $O[(kr)^2]$  on the photoelectron angular distribution for photoionization of different atomic shells. Fig. 3 demonstrates the differential cross section normalized to a unit solid angle

$$\frac{d\bar{\sigma}_i(\theta)}{d\Omega} = \frac{d\sigma_i(\theta)}{d\Omega} \Big/ \frac{\sigma_i}{4\pi} \quad (35)$$

for the case of unpolarized radiation at the energy  $E = 10$  keV. Calculations were carried out including the  $O[(kr)^2]$  order terms using Eq. (25) (solid curves) and without them using Eq. (1) (dashed curves). As seen in the figure, the solid curves are shifted to the lesser angles with relation to the dashed curves. The difference between corresponding values of  $\frac{d\bar{\sigma}_i(\theta)}{d\Omega}$  reaches 19% for the  $1s_{1/2}$ -shell of Li, 14% for the  $2p_{1/2}$ -shell of Na, 21% for the  $4d_{3/2}$ -shell of Ag, and 33% for the  $4f_{5/2}$ -shell of Sm.

The angular distribution in the case of linearly polarized radiation is shown in Fig. 4 for  $E = 10$  keV. We present the  $\theta$ -dependence of  $\frac{d\bar{\sigma}_i(\theta, \varphi)}{d\Omega}$  for two values of the angle  $\varphi$  ( $\varphi = 0$  and  $\varphi = \pi/2$ ). The comparison of the angular distribution calculated with and without including the second order terms also exhibits the considerable effect of these terms. The difference in corresponding differential sections

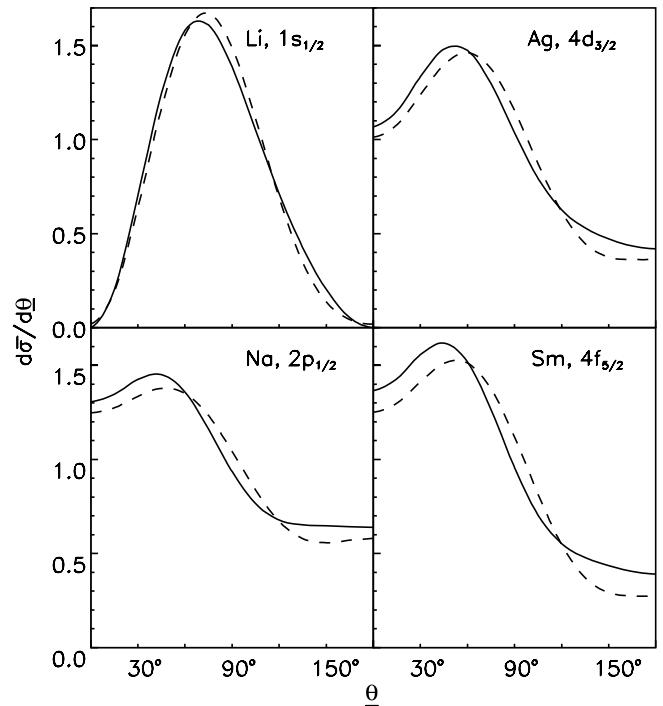


Fig. 3. Photoelectron angular distribution  $d\bar{\sigma}_i/d\Omega(\theta)$  calculated with (solid line) and without (dashed line) regard to the terms of the order  $O[(kr)^2]$  in the case of unpolarized radiation at the photoelectron energy  $E = 10$  keV.

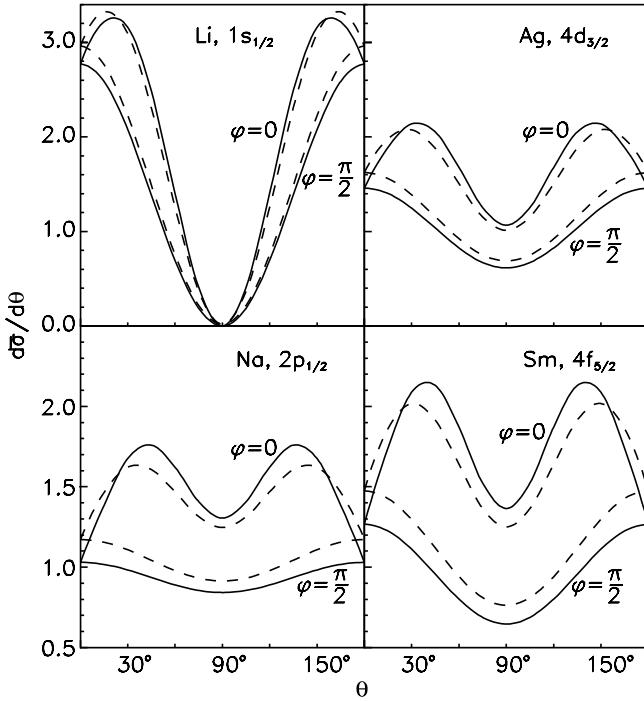


Fig. 4. Photoelectron angular distribution  $d\bar{\sigma}_i/d\Omega(\theta, \varphi)$  calculated with (solid line) and without (dashed line) regard to the terms of the order  $O[(kr)^2]$  at the photoelectron energy  $E = 10$  keV in the case of linearly polarized radiation at two values  $\varphi = 0$  and  $\varphi = \pi/2$ .

reaches  $\sim 20\%$ . In addition, calculations with regard to these terms using Eq. (24) (solid curves) and without regard for these terms using Eq. (2) (dashed curves) differ in the positions of the maxima at  $\varphi = 0$ . Calculations showed that the second-order terms make a noticeable contribution to the angular distributions for lower energies also. For example, the contribution is 6% for the 2p<sub>1/2</sub>-shell of Na and 8% for the 4d<sub>3/2</sub>-shell of Ag at  $E = 5$  keV.

The role of the  $O[(kr)^2]$  terms becomes of particular importance in calculation of the special non-dipole parameter  $\zeta$  which is specified for linearly polarized radiation as follows:

$$\zeta = \sqrt{\frac{27}{2}} \left\{ \left[ \frac{d\sigma_i}{d\Omega}(\theta_m, \varphi = 0) \Big/ \frac{d\sigma_i}{d\Omega}(\theta_m, \varphi = \pi/2) \right] - 1 \right\}. \quad (36)$$

Here  $\theta_m = 54.7^\circ$  is the magic angle for which  $P_2(\cos \theta_m) = 0$ , that is, the dipole term vanishes in the differential cross section. The parameter  $\zeta$  is measured experimentally [9]. The dependence  $\zeta(E)$  obtained with and without regard to the  $O[(kr)^2]$  terms is shown in Fig. 5 for the 2p<sub>1/2</sub>-shell of Na, the 3d<sub>3/2</sub>-shell of Zn, and the 7s-shell of U. As seen, for the 2p<sub>1/2</sub>- and 3d<sub>3/2</sub>-shell, the second order terms increase the value of  $\zeta$  by  $\sim 1.5$  times at  $E = 5$  keV and a factor of two at  $E = 10$  keV. The terms make a noticeable contribution ( $\sim 15\%$ ) even at the lowest energy under consideration  $E = 1$  keV. For the outer 7s-shell, the influence of these terms is even greater. The value of  $\zeta$  increases by  $\sim 2.5$

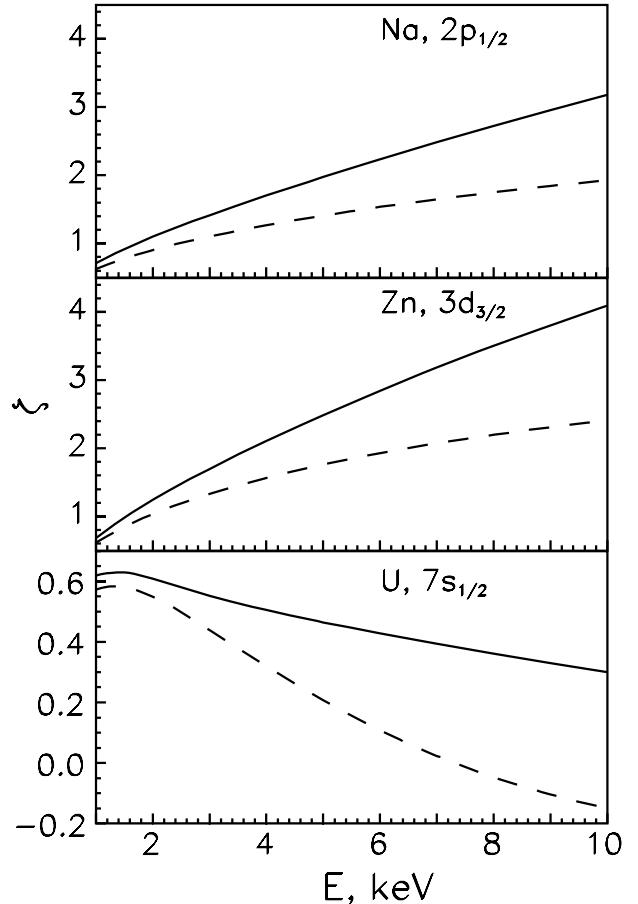


Fig. 5. The non-dipole parameter  $\zeta$  [Eq. (36)] versus the photoelectron energy  $E$  calculated with (solid line) and without (dashed line) regard to the terms of the order  $O[(kr)^2]$ .

times at  $E = 5$  keV and changes from  $-0.15$  to  $+0.32$  at  $E = 10$  keV if the second-order terms are taken into account. Consequently, the proper allowance must be made for terms of the order  $O[(kr)^2]$  in the photoelectron energy range under consideration.

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## Appendix A. Supplementary data

Supplementary data associated with this article can be found, in the online version, at doi:10.1016/j.adt.2005.12.002.

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## Explanation of Tables

**Table 1.** Angular distribution parameters of the second order

$Z$	Atomic number
Shell	Atomic subshell from which a photoelectron is emitted
$E$	Photoelectron energy in keV
$\Delta\beta_{\text{unp}}$	Correction of the second order $O[(kr)^2]$ to the dipole parameter $\beta$ in the case of unpolarized or circularly polarized radiation
$\Delta\beta_{\ell p}$	Correction of the second order $O[(kr)^2]$ to the dipole parameter $\beta$ in the case of linearly polarized radiation
$\eta$ $\mu$ $\xi$	Photoelectron angular distribution parameters of the order $O[(kr)^2]$

The electron configuration of the atom  $Z$  is presented in the form of quantum numbers of the additional electrons with respect to the configuration of the nearest rare gas with the atomic number smaller than  $Z$ .

**Table 2.** Subshell photoionization cross section and angular distribution parameters of the zero and first orders for photoelectron energy  $E = 10$  keV

$\sigma$	Subshell photoionization cross section in kb ( $=10^{-21} \text{ cm}^2$ )
$\beta$	Dipole angular distribution parameter
$\gamma$ $\delta$	Non-dipole angular distribution parameters of the order $O(kr)$

The photoionization cross sections are presented for completely filled atomic subshells. To obtain  $\sigma_i$  for a partially filled subshell  $i$ , the value from the Table should be divided by the factor  $(2j_i + 1)$  and multiplied by the actual occupation number of the  $i$ -th subshell.

Presented for each value to its right is the decimal order. For example, the value  $-1.15-2$  is equal to  $-0.0115$ .

Table 1

Angular distribution parameters of the second order. See page 252 for Explanation of Tables

Shell	$E$	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$	Shell	$E$	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$
$Z = 1, \text{H}: 1s_{1/2}^1$													
$1s_{1/2}$	1	-2.28-2	-6.12-3	5.58-3	7.81-3	-1.34-2	$1s_{1/2}$	1	-2.22-2	-6.02-3	5.41-3	7.57-3	-1.30-2
	3	-6.82-2	-1.83-2	1.67-2	2.33-2	-4.00-2		3	-6.93-2	-1.86-2	1.69-2	2.37-2	-4.06-2
	5	-1.13-1	-3.03-2	2.76-2	3.86-2	-6.62-2		5	-1.07-1	-2.77-2	2.64-2	3.68-2	-6.32-2
	10	-2.21-1	-5.89-2	5.44-2	7.59-2	-1.30-1		10	-2.11-1	-5.40-2	5.25-2	7.33-2	-1.26-1
$Z = 3, \text{Li}: 1s_{1/2}^2 2s_{1/2}^1$													
$1s_{1/2}$	1	-1.97-2	-5.13-3	4.87-3	6.82-3	-1.17-2	$1s_{1/2}$	1	-1.90-2	-4.90-3	4.70-3	6.58-3	-1.13-2
	3	-6.50-2	-1.73-2	1.59-2	2.23-2	-3.82-2		3	-6.31-2	-1.66-2	1.55-2	2.17-2	-3.72-2
	5	-1.10-1	-2.95-2	2.70-2	3.77-2	-6.48-2		5	-1.08-1	-2.86-2	2.65-2	3.70-2	-6.36-2
	10	-2.21-1	-5.93-2	5.42-2	7.56-2	-1.30-1		10	-2.19-1	-5.83-2	5.37-2	7.48-2	-1.29-1
$2s_{1/2}$	1	-1.89-2	-4.93-3	4.65-3	6.51-3	-1.12-2	$2s_{1/2}$	1	-1.86-2	-5.04-3	4.54-3	6.35-3	-1.09-2
	3	-6.52-2	-1.72-2	1.60-2	2.24-2	-3.84-2		3	-6.16-2	-1.62-2	1.52-2	2.12-2	-3.64-2
	5	-1.10-1	-2.91-2	2.70-2	3.78-2	-6.48-2		5	-1.09-1	-2.92-2	2.66-2	3.71-2	-6.36-2
	10	-2.18-1	-5.78-2	5.38-2	7.50-2	-1.29-1		10	-2.19-1	-5.87-2	5.37-2	7.49-2	-1.29-1
$Z = 5, \text{B}: 1s_{1/2}^2 2s_{1/2}^2 2p_{1/2}^1$													
$1s_{1/2}$	1	-1.84-2	-4.63-3	4.58-3	6.41-3	-1.10-2	$1s_{1/2}$	1	-1.74-2	-4.26-3	4.39-3	6.14-3	-1.05-2
	3	-6.15-2	-1.61-2	1.52-2	2.12-2	-3.63-2		3	-6.05-2	-1.57-2	1.49-2	2.09-2	-3.58-2
	5	-1.06-1	-2.80-2	2.61-2	3.64-2	-6.25-2		5	-1.04-1	-2.73-2	2.57-2	3.58-2	-6.15-2
	10	-2.16-1	-5.75-2	5.32-2	7.41-2	-1.27-1		10	-2.14-1	-5.67-2	5.27-2	7.34-2	-1.26-1
$2s_{1/2}$	1	-1.61-2	-4.21-3	3.96-3	5.54-3	-9.50-3	$2s_{1/2}$	1	-1.40-2	-3.63-3	3.46-3	4.84-3	-8.30-3
	3	-6.09-2	-1.64-2	1.49-2	2.08-2	-3.56-2		3	-5.74-2	-1.51-2	1.41-2	1.97-2	-3.38-2
	5	-1.05-1	-2.80-2	2.57-2	3.59-2	-6.16-2		5	-1.02-1	-2.73-2	2.50-2	3.50-2	-6.00-2
	10	-2.15-1	-5.74-2	5.29-2	7.37-2	-1.27-1		10	-2.12-1	-5.64-2	5.20-2	7.25-2	-1.25-1
$2p_{1/2}$	1	-3.08-2	-5.96-3	1.42-4	9.98-3	-1.01-2	$2p_{1/2}$	1	-2.71-2	-4.83-3	1.22-4	8.93-3	-9.06-3
	3	-8.29-2	-1.31-2	-4.41-3	2.70-2	-2.26-2		3	-9.44-2	-1.81-2	-1.65-3	3.02-2	-2.85-2
	5	-1.62-1	-3.20-2	-4.49-3	5.12-2	-4.67-2		5	-1.46-1	-2.49-2	-6.29-3	4.72-2	-4.09-2
	10	-3.01-1	-5.35-2	-1.17-2	9.65-2	-8.49-2		10	-3.05-1	-5.48-2	-1.22-2	9.75-2	-8.53-2
$Z = 7, \text{N}: 1s_{1/2}^2 2s_{1/2}^2 2p_{1/2}^2 2p_{3/2}^1$													
$1s_{1/2}$	1	-1.64-2	-3.90-3	4.18-3	5.85-3	-1.00-2	$1s_{1/2}$	1	-1.55-2	-3.55-3	3.99-3	5.58-3	-9.56-3
	3	-5.92-2	-1.53-2	1.47-2	2.05-2	-3.52-2		3	-5.77-2	-1.47-2	1.44-2	2.01-2	-3.45-2
	5	-1.03-1	-2.68-2	2.54-2	3.54-2	-6.08-2		5	-1.01-1	-2.63-2	2.51-2	3.50-2	-6.00-2
	10	-2.11-1	-5.58-2	5.21-2	7.26-2	-1.25-1		10	-2.09-1	-5.51-2	5.16-2	7.19-2	-1.24-1
$2s_{1/2}$	1	-1.26-2	-3.35-3	3.07-3	4.30-3	-7.37-3	$2s_{1/2}$	1	-1.10-2	-2.96-3	2.67-3	3.73-3	-6.40-3
	3	-5.46-2	-1.45-2	1.34-2	1.87-2	-3.22-2		3	-5.16-2	-1.37-2	1.27-2	1.77-2	-3.04-2
	5	-9.82-2	-2.60-2	2.42-2	3.37-2	-5.79-2		5	-9.56-2	-2.55-2	2.35-2	3.27-2	-5.62-2
	10	-2.08-1	-5.54-2	5.11-2	7.13-2	-1.22-1		10	-2.04-1	-5.43-2	5.02-2	7.00-2	-1.20-1
$2p_{1/2}$	1	-2.53-2	-4.60-3	2.74-4	8.35-3	-8.62-3	$2p_{1/2}$	1	-2.50-2	-4.77-3	6.79-4	8.22-3	-8.90-3
	3	-8.82-2	-1.54-2	-1.66-3	2.88-2	-2.71-2		3	-8.87-2	-1.65-2	-5.28-4	2.88-2	-2.83-2
	5	-1.53-1	-2.85-2	-3.78-3	4.92-2	-4.54-2		5	-1.49-1	-2.67-2	-3.35-3	4.84-2	-4.50-2
	10	-2.98-1	-5.32-2	-1.15-2	9.57-2	-8.42-2		10	-2.96-1	-5.32-2	-1.08-2	9.49-2	-8.41-2
$2p_{3/2}$	1	-2.13-2	-5.13-3	1.81-3	6.81-3	-8.62-3	$2p_{3/2}$	1	-2.12-2	-5.28-3	2.13-3	6.78-3	-8.90-3
	3	-7.42-2	-1.71-2	3.48-3	2.35-2	-2.70-2		3	-7.53-2	-1.83-2	4.46-3	2.37-2	-2.82-2
	5	-1.29-1	-3.15-2	5.03-3	4.00-2	-4.51-2		5	-1.26-1	-2.97-2	5.15-3	3.96-2	-4.47-2
	10	-2.51-1	-5.95-2	5.18-3	7.78-2	-8.30-2		10	-2.49-1	-5.93-2	5.72-3	7.70-2	-8.27-2
$Z = 9, \text{F}: 1s_{1/2}^2 2s_{1/2}^2 2p_{1/2}^2 2p_{3/2}^3$													
$1s_{1/2}$	1	-1.46-2	-3.19-3	3.80-3	5.32-3	-9.12-3	$1s_{1/2}$	1	-1.36-2	-2.80-3	3.61-3	5.05-3	-8.66-3
	3	-5.61-2	-1.41-2	1.41-2	1.96-2	-3.37-2		3	-5.45-2	-1.35-2	1.37-2	1.92-2	-3.29-2
	5	-9.94-2	-2.56-2	2.47-2	3.45-2	-5.92-2		5	-9.75-2	-2.49-2	2.43-2	3.39-2	-5.82-2
	10	-2.07-1	-5.44-2	5.13-2	7.14-2	-1.23-1		10	-2.05-1	-5.37-2	5.09-2	7.08-2	-1.22-1
$2s_{1/2}$	1	-9.12-3	-2.46-3	2.22-3	3.10-3	-5.33-3	$2s_{1/2}$	1	-7.26-3	-1.97-3	1.77-3	2.47-3	-4.24-3
	3	-4.79-2	-1.25-2	1.18-2	1.65-2	-2.83-2		3	-4.50-2	-1.19-2	1.11-2	1.55-2	-2.66-2
	5	-9.12-2	-2.41-2	2.25-2	3.13-2	-5.38-2		5	-8.69-2	-2.29-2	2.14-2	2.99-2	-5.13-2
	10	-2.01-1	-5.34-2	4.94-2	6.87-2	-1.18-1		10	-1.96-1	-5.20-2	4.82-2	6.72-2	-1.15-1
$2p_{1/2}$	1	-2.46-2	-4.76-3	1.03-3	8.13-3	-9.16-3	$2p_{1/2}$	1	-2.37-2	-4.55-3	1.23-3	7.90-3	-9.13-3
	3	-8.55-2	-1.56-2	-1.10-5	2.79-2	-2.79-2		3	-8.23-2	-1.49-2	3.21-4	2.70-2	-2.73-2

(continued on next page)

Table 1 (continued)

Shell	$E$	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$	Shell	$E$	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$
	5	-1.51-1	-2.80-2	-1.76-3	4.88-2	-4.71-2		5	-1.45-1	-2.60-2	-1.37-3	4.73-2	-4.59-2
	10	-2.98-1	-5.42-2	-8.96-3	9.56-2	-8.67-2		10	-2.96-1	-5.38-2	-7.56-3	9.56-2	-8.80-2
2p <sub>3/2</sub>	1	-2.09-2	-5.26-3	2.43-3	6.74-3	-9.17-3	2p <sub>3/2</sub>	1	-2.01-2	-5.03-3	2.59-3	6.56-3	-9.15-3
	3	-7.22-2	-1.74-2	4.95-3	2.29-2	-2.79-2		3	-6.94-2	-1.66-2	5.13-3	2.21-2	-2.73-2
	5	-1.28-1	-3.10-2	6.65-3	4.01-2	-4.68-2		5	-1.22-1	-2.90-2	6.86-3	3.88-2	-4.56-2
	10	-2.52-1	-6.04-2	7.41-3	7.80-2	-8.54-2		10	-2.51-1	-5.98-2	8.51-3	7.81-2	-8.66-2
$Z = 11$ , Na: 3s <sub>1/2</sub>							$Z = 12$ , Mg: 3s <sub>1/2</sub>						
1s <sub>1/2</sub>	1	-1.28-2	-2.42-3	3.46-3	4.83-3	-8.29-3	1s <sub>1/2</sub>	1	-1.20-2	-2.03-3	3.32-3	4.64-3	-7.96-3
	3	-5.30-2	-1.29-2	1.34-2	1.87-2	-3.21-2		3	-5.16-2	-1.23-2	1.31-2	1.83-2	-3.15-2
	5	-9.56-2	-2.42-2	2.39-2	3.34-2	-5.73-2		5	-9.38-2	-2.34-2	2.36-2	3.29-2	-5.64-2
	10	-2.03-1	-5.28-2	5.04-2	7.02-2	-1.21-1		10	-2.01-1	-5.20-2	5.00-2	6.96-2	-1.20-1
2s <sub>1/2</sub>	1	-5.80-3	-1.62-3	1.40-3	1.95-3	-3.35-3	2s <sub>1/2</sub>	1	-4.58-3	-1.33-3	1.09-3	1.52-3	-2.60-3
	3	-4.19-2	-1.11-2	1.03-2	1.44-2	-2.47-2		3	-3.89-2	-1.03-2	9.57-3	1.34-2	-2.29-2
	5	-8.34-2	-2.20-2	2.05-2	2.87-2	-4.92-2		5	-7.96-2	-2.10-2	1.96-2	2.73-2	-4.70-2
	10	-1.91-1	-5.06-2	4.71-2	6.56-2	-1.13-1		10	-1.86-1	-4.92-2	4.59-2	6.39-2	-1.10-1
2p <sub>1/2</sub>	1	-2.24-2	-4.23-3	1.27-3	7.51-3	-8.78-3	2p <sub>1/2</sub>	1	-2.16-2	-4.04-3	1.34-3	7.27-3	-8.61-3
	3	-8.16-2	-1.51-2	1.11-3	2.68-2	-2.79-2		3	-8.06-2	-1.51-2	1.75-3	2.66-2	-2.83-2
	5	-1.43-1	-2.62-2	-5.06-4	4.67-2	-4.62-2		5	-1.41-1	-2.59-2	2.98-4	4.61-2	-4.64-2
	10	-2.95-1	-5.35-2	-6.11-3	9.53-2	-8.92-2		10	-2.92-1	-5.31-2	-4.87-3	9.47-2	-8.98-2
2p <sub>3/2</sub>	1	-1.90-2	-4.69-3	2.57-3	6.24-3	-8.81-3	2p <sub>3/2</sub>	1	-1.83-2	-4.49-3	2.61-3	6.03-3	-8.64-3
	3	-6.90-2	-1.68-2	5.81-3	2.21-2	-2.79-2		3	-6.84-2	-1.67-2	6.36-3	2.20-2	-2.83-2
	5	-1.21-1	-2.91-2	7.58-3	3.84-2	-4.59-2		5	-1.20-1	-2.88-2	8.27-3	3.79-2	-4.62-2
	10	-2.50-1	-5.95-2	9.79-3	7.81-2	-8.79-2		10	-2.48-1	-5.90-2	1.09-2	7.77-2	-8.86-2
3s <sub>1/2</sub>	1	-5.70-3	-1.72-3	1.33-3	1.86-3	-3.18-3	3s <sub>1/2</sub>	1	-4.27-3	-1.33-3	9.82-4	1.37-3	-2.35-3
	3	-4.23-2	-1.14-2	1.03-2	1.44-2	-2.47-2		3	-3.84-2	-1.02-2	9.43-3	1.32-2	-2.26-2
	5	-8.27-2	-2.18-2	2.04-2	2.85-2	-4.89-2		5	-7.91-2	-2.09-2	1.95-2	2.71-2	-4.66-2
	10	-1.91-1	-5.06-2	4.70-2	6.54-2	-1.12-1		10	-1.85-1	-4.91-2	4.57-2	6.36-2	-1.09-1
$Z = 13$ , Al: 3s <sub>1/2</sub> <sup>2</sup> 2p <sub>1/2</sub> <sup>1</sup>							$Z = 14$ , Si: 3s <sub>1/2</sub> <sup>2</sup> 2p <sub>1/2</sub> <sup>2</sup>						
1s <sub>1/2</sub>	1	-1.12-2	-1.63-3	3.19-3	4.45-3	-7.65-3	1s <sub>1/2</sub>	1	-1.03-2	-1.21-3	3.06-3	4.26-3	-7.33-3
	3	-5.02-2	-1.17-2	1.29-2	1.80-2	-3.09-2		3	-4.89-2	-1.12-2	1.26-2	1.76-2	-3.03-2
	5	-9.20-2	-2.28-2	2.32-2	3.24-2	-5.56-2		5	-9.03-2	-2.20-2	2.29-2	3.19-2	-5.47-2
	10	-1.99-1	-5.10-2	4.95-2	6.89-2	-1.18-1		10	-1.96-1	-5.01-2	4.91-2	6.82-2	-1.17-1
2s <sub>1/2</sub>	1	-3.55-3	-1.11-3	8.18-4	1.14-3	-1.96-3	2s <sub>1/2</sub>	1	-2.70-3	-9.41-4	5.90-4	8.22-4	-1.41-3
	3	-3.58-2	-9.44-3	8.81-3	1.23-2	-2.11-2		3	-3.27-2	-8.65-3	8.06-3	1.12-2	-1.93-2
	5	-7.57-2	-2.00-2	1.87-2	2.60-2	-4.47-2		5	-7.17-2	-1.89-2	1.77-2	2.47-2	-4.24-2
	10	-1.81-1	-4.78-2	4.47-2	6.22-2	-1.07-1		10	-1.76-1	-4.65-2	4.34-2	6.04-2	-1.04-1
2p <sub>1/2</sub>	1	-2.07-2	-3.83-3	1.36-3	7.02-3	-8.37-3	2p <sub>1/2</sub>	1	-2.00-2	-3.67-3	1.36-3	6.81-3	-8.17-3
	3	-7.96-2	-1.49-2	2.35-3	2.63-2	-2.87-2		3	-7.84-2	-1.47-2	2.90-3	2.61-2	-2.90-2
	5	-1.39-1	-2.57-2	1.19-3	4.57-2	-4.69-2		5	-1.38-1	-2.56-2	2.07-3	4.54-2	-4.75-2
	10	-2.89-1	-5.26-2	-3.68-3	9.39-2	-9.03-2		10	-2.87-1	-5.22-2	-2.48-3	9.32-2	-9.07-2
2p <sub>3/2</sub>	1	-1.75-2	-4.28-3	2.61-3	5.80-3	-8.41-3	2p <sub>3/2</sub>	1	-1.68-2	-4.11-3	2.61-3	5.61-3	-8.22-3
	3	-6.76-2	-1.65-2	6.88-3	2.18-2	-2.87-2		3	-6.68-2	-1.63-2	7.35-3	2.17-2	-2.90-2
	5	-1.18-1	-2.86-2	9.05-3	3.77-2	-4.67-2		5	-1.17-1	-2.84-2	9.84-3	3.75-2	-4.74-2
	10	-2.45-1	-5.85-2	1.19-2	7.72-2	-8.91-2		10	-2.43-1	-5.81-2	1.30-2	7.67-2	-8.96-2
3s <sub>1/2</sub>	1	-3.15-3	-1.08-3	6.93-4	9.66-4	-1.66-3	3s <sub>1/2</sub>	1	-2.27-3	-8.94-4	4.61-4	6.43-4	-1.10-3
	3	-3.52-2	-9.49-3	8.61-3	1.20-2	-2.06-2		3	-3.15-2	-8.40-3	7.73-3	1.08-2	-1.85-2
	5	-7.51-2	-1.99-2	1.85-2	2.57-2	-4.42-2		5	-7.06-2	-1.87-2	1.74-2	2.42-2	-4.16-2
	10	-1.80-1	-4.77-2	4.44-2	6.18-2	-1.06-1		10	-1.75-1	-4.63-2	4.31-2	6.00-2	-1.03-1
3p <sub>1/2</sub>	1	-1.95-2	-3.73-3	1.40-3	6.59-3	-7.99-3	3p <sub>1/2</sub>	1	-1.80-2	-3.37-3	1.35-3	6.13-3	-7.47-3
	3	-7.94-2	-1.52-2	2.61-3	2.62-2	-2.88-2		3	-7.64-2	-1.44-2	3.01-3	2.54-2	-2.84-2
	5	-1.38-1	-2.54-2	1.26-3	4.53-2	-4.66-2		5	-1.36-1	-2.54-2	2.22-3	4.49-2	-4.71-2
	10	-2.88-1	-5.23-2	-3.57-3	9.36-2	-9.00-2		10	-2.84-1	-5.18-2	-2.31-3	9.26-2	-9.03-2
$Z = 15$ , P: 3s <sub>1/2</sub> <sup>2</sup> 2p <sub>1/2</sub> <sup>2</sup> 2p <sub>3/2</sub> <sup>1</sup>							$Z = 16$ , S: 3s <sub>1/2</sub> <sup>2</sup> 2p <sub>1/2</sub> <sup>2</sup> 2p <sub>3/2</sub> <sup>2</sup>						
2s <sub>1/2</sub>	1	-2.00-3	-8.11-4	3.98-4	5.55-4	-9.53-4	2s <sub>1/2</sub>	1	-1.46-3	-7.24-4	2.46-4	3.42-4	-5.88-4
	3	-2.97-2	-7.88-3	7.32-3	1.02-2	-1.75-2		3	-2.68-2	-7.14-3	6.60-3	9.20-3	-1.58-2
	5	-6.78-2	-1.79-2	1.67-2	2.33-2	-4.01-2		5	-6.38-2	-1.68-2	1.57-2	2.19-2	-3.77-2
	10	-1.71-1	-4.51-2	4.22-2	5.87-2	-1.01-1		10	-1.65-1	-4.37-2	4.09-2	5.69-2	-9.78-2

Table 1 (continued)

Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$	Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$
2p <sub>1/2</sub>	1	-1.94-2	-3.50-3	1.35-3	6.64-3	-7.99-3	2p <sub>1/2</sub>	1	-1.88-2	-3.29-3	1.31-3	6.45-3	-7.76-3
	3	-7.73-2	-1.45-2	3.36-3	2.58-2	-2.92-2		3	-7.59-2	-1.42-2	3.72-3	2.54-2	-2.92-2
	5	-1.37-1	-2.55-2	2.96-3	4.52-2	-4.81-2		5	-1.36-1	-2.53-2	3.78-3	4.49-2	-4.87-2
	10	-2.84-1	-5.20-2	-1.23-3	9.26-2	-9.14-2		10	-2.82-1	-5.18-2	6.42-5	9.21-2	-9.22-2
2p <sub>3/2</sub>	1	-1.62-2	-3.94-3	2.60-3	5.44-3	-8.04-3	2p <sub>3/2</sub>	1	-1.55-2	-3.73-3	2.57-3	5.24-3	-7.80-3
	3	-6.59-2	-1.60-2	7.76-3	2.15-2	-2.92-2		3	-6.47-2	-1.57-2	8.06-3	2.12-2	-2.93-2
	5	-1.16-1	-2.82-2	1.06-2	3.74-2	-4.81-2		5	-1.15-1	-2.80-2	1.14-2	3.73-2	-4.86-2
	10	-2.41-1	-5.78-2	1.41-2	7.62-2	-9.03-2		10	-2.40-1	-5.75-2	1.53-2	7.59-2	-9.12-2
3s <sub>1/2</sub>	1	-1.62-3	-7.95-4	2.78-4	3.86-4	-6.64-4	3s <sub>1/2</sub>	1	-1.20-3	-7.77-4	1.42-4	1.98-4	-3.40-4
	3	-2.86-2	-7.76-3	6.98-3	9.74-3	-1.67-2		3	-2.57-2	-7.10-3	6.23-3	8.69-3	-1.49-2
	5	-6.64-2	-1.77-2	1.63-2	2.28-2	-3.91-2		5	-6.21-2	-1.65-2	1.53-2	2.13-2	-3.65-2
	10	-1.69-1	-4.48-2	4.18-2	5.81-2	-9.99-2		10	-1.64-1	-4.34-2	4.04-2	5.62-2	-9.66-2
3p <sub>1/2</sub>	1	-1.66-2	-3.07-3	1.26-3	5.67-3	-6.92-3	3p <sub>1/2</sub>	1	-1.54-2	-2.89-3	1.21-3	5.25-3	-6.46-3
	3	-7.35-2	-1.37-2	3.25-3	2.46-2	-2.79-2		3	-7.21-2	-1.37-2	3.81-3	2.41-2	-2.80-2
	5	-1.34-1	-2.47-2	2.98-3	4.41-2	-4.71-2		5	-1.32-1	-2.48-2	3.99-3	4.37-2	-4.77-2
	10	-2.81-1	-5.15-2	-1.09-3	9.18-2	-9.07-2		10	-2.78-1	-5.11-2	2.74-4	9.09-2	-9.12-2
3p <sub>3/2</sub>	1	-1.36-2	-3.48-3	2.42-3	4.55-3	-6.97-3	3p <sub>3/2</sub>	1	-1.26-2	-3.29-3	2.34-3	4.18-3	-6.52-3
	3	-6.23-2	-1.52-2	7.58-3	2.04-2	-2.79-2		3	-6.12-2	-1.52-2	8.04-3	2.00-2	-2.81-2
	5	-1.13-1	-2.74-2	1.06-2	3.64-2	-4.70-2		5	-1.12-1	-2.74-2	1.15-2	3.62-2	-4.77-2
	10	-2.38-1	-5.71-2	1.42-2	7.53-2	-8.95-2		10	-2.36-1	-5.67-2	1.54-2	7.48-2	-9.02-2
<i>Z</i> = 17, Cl: 3s <sub>1/2</sub> <sup>2</sup> 2p <sub>1/2</sub> <sup>2</sup> 2p <sub>3/2</sub> <sup>2</sup>							<i>Z</i> = 18, Ar: 3s <sub>1/2</sub> <sup>2</sup> 2p <sub>1/2</sub> <sup>2</sup> 2p <sub>3/2</sub> <sup>4</sup>						
2s <sub>1/2</sub>	1	-1.09-3	-6.89-4	1.37-4	1.90-4	-3.27-4	2s <sub>1/2</sub>	1	-9.56-4	-7.21-4	8.01-5	1.10-4	-1.90-4
	3	-2.41-2	-6.49-3	5.92-3	8.25-3	-1.42-2		3	-2.16-2	-5.88-3	5.28-3	7.35-3	-1.26-2
	5	-5.97-2	-1.57-2	1.48-2	2.06-2	-3.53-2		5	-5.57-2	-1.47-2	1.38-2	1.92-2	-3.29-2
	10	-1.60-1	-4.22-2	3.96-2	5.51-2	-9.47-2		10	-1.55-1	-4.08-2	3.83-2	5.32-2	-9.15-2
2p <sub>1/2</sub>	1	-1.80-2	-3.04-3	1.23-3	6.24-3	-7.48-3	2p <sub>1/2</sub>	1	-1.73-2	-2.78-3	1.13-3	6.04-3	-7.16-3
	3	-7.45-2	-1.39-2	4.03-3	2.51-2	-2.91-2		3	-7.33-2	-1.36-2	4.29-3	2.48-2	-2.90-2
	5	-1.34-1	-2.50-2	4.54-3	4.46-2	-4.91-2		5	-1.33-1	-2.47-2	5.21-3	4.42-2	-4.94-2
	10	-2.80-1	-5.16-2	1.39-3	9.17-2	-9.31-2		10	-2.78-1	-5.14-2	2.73-3	9.14-2	-9.41-2
2p <sub>3/2</sub>	1	-1.48-2	-3.49-3	2.52-3	5.02-3	-7.54-3	2p <sub>3/2</sub>	1	-1.40-2	-3.22-3	2.44-3	4.79-3	-7.23-3
	3	-6.35-2	-1.54-2	8.32-3	2.09-2	-2.92-2		3	-6.25-2	-1.51-2	8.56-3	2.07-2	-2.92-2
	5	-1.15-1	-2.78-2	1.21-2	3.71-2	-4.92-2		5	-1.13-1	-2.74-2	1.27-2	3.69-2	-4.96-2
	10	-2.38-1	-5.73-2	1.65-2	7.57-2	-9.22-2		10	-2.37-1	-5.71-2	1.77-2	7.56-2	-9.33-2
3s <sub>1/2</sub>	1	-9.13-4	-7.66-4	4.98-5	6.88-5	-1.19-4	3s <sub>1/2</sub>	1	-8.14-4	-7.86-4	9.34-6	1.28-5	-2.22-5
	3	-2.28-2	-6.33-3	5.50-3	7.67-3	-1.32-2		3	-2.03-2	-5.84-3	4.84-3	6.75-3	-1.16-2
	5	-5.78-2	-1.55-2	1.42-2	1.98-2	-3.40-2		5	-5.35-2	-1.44-2	1.31-2	1.83-2	-3.14-2
	10	-1.58-1	-4.19-2	3.90-2	5.42-2	-9.32-2		10	-1.52-1	-4.03-2	3.75-2	5.22-2	-8.97-2
3p <sub>1/2</sub>	1	-1.42-2	-2.66-3	1.14-3	4.85-3	-5.99-3	3p <sub>1/2</sub>	1	-1.28-2	-2.31-3	9.90-4	4.39-3	-5.38-3
	3	-6.91-2	-1.29-2	3.95-3	2.33-2	-2.73-2		3	-6.77-2	-1.28-2	4.33-3	2.28-2	-2.72-2
	5	-1.28-1	-2.38-2	4.52-3	4.28-2	-4.73-2		5	-1.26-1	-2.36-2	5.29-3	4.21-2	-4.74-2
	10	-2.75-1	-5.07-2	1.59-3	9.02-2	-9.18-2		10	-2.72-1	-5.03-2	3.00-3	8.94-2	-9.24-2
3p <sub>3/2</sub>	1	-1.14-2	-3.06-3	2.24-3	3.80-3	-6.05-3	3p <sub>3/2</sub>	1	-1.01-2	-2.70-3	2.07-3	3.37-3	-5.44-3
	3	-5.85-2	-1.43-2	8.10-3	1.93-2	-2.74-2		3	-5.74-2	-1.42-2	8.40-3	1.89-2	-2.73-2
	5	-1.09-1	-2.65-2	1.19-2	3.54-2	-4.73-2		5	-1.07-1	-2.62-2	1.25-2	3.50-2	-4.75-2
	10	-2.34-1	-5.62-2	1.66-2	7.43-2	-9.09-2		10	-2.31-1	-5.59-2	1.79-2	7.38-2	-9.17-2
<i>Z</i> = 19, K: 4s <sub>1/2</sub> <sup>1</sup>							<i>Z</i> = 20, Ca: 4s <sub>1/2</sub> <sup>2</sup>						
2s <sub>1/2</sub>	1	-1.03-3	-8.09-4	7.50-5	1.04-4	-1.79-4	2s <sub>1/2</sub>	1	-1.34-3	-9.68-4	1.24-4	1.74-4	-2.98-4
	3	-1.92-2	-5.32-3	4.67-3	6.50-3	-1.12-2		3	-1.70-2	-4.79-3	4.10-3	5.70-3	-9.80-3
	5	-5.18-2	-1.37-2	1.28-2	1.78-2	-3.06-2		5	-4.82-2	-1.28-2	1.19-2	1.65-2	-2.84-2
	10	-1.49-1	-3.93-2	3.70-2	5.13-2	-8.83-2		10	-1.43-1	-3.78-2	3.56-2	4.94-2	-8.50-2
2p <sub>1/2</sub>	1	-1.65-2	-2.50-3	1.01-3	5.82-3	-6.83-3	2p <sub>1/2</sub>	1	-1.58-2	-2.20-3	8.65-4	5.60-3	-6.47-3
	3	-7.21-2	-1.33-2	4.52-3	2.44-2	-2.90-2		3	-7.10-2	-1.30-2	4.71-3	2.41-2	-2.89-2
	5	-1.31-1	-2.44-2	5.76-3	4.38-2	-4.96-2		5	-1.29-1	-2.40-2	6.28-3	4.34-2	-4.97-2
	10	-2.77-1	-5.13-2	4.04-3	9.10-2	-9.51-2		10	-2.75-1	-5.11-2	5.33-3	9.07-2	-9.60-2
2p <sub>3/2</sub>	1	-1.32-2	-2.95-3	2.35-3	4.55-3	-6.90-3	2p <sub>3/2</sub>	1	-1.23-2	-2.66-3	2.25-3	4.30-3	-6.55-3
	3	-6.15-2	-1.49-2	8.76-3	2.04-2	-2.92-2		3	-6.05-2	-1.46-2	8.94-3	2.02-2	-2.91-2
	5	-1.12-1	-2.71-2	1.32-2	3.66-2	-4.98-2		5	-1.11-1	-2.67-2	1.36-2	3.63-2	-4.99-2
	10	-2.36-1	-5.69-2	1.90-2	7.55-2	-9.44-2		10	-2.35-1	-5.67-2	2.02-2	7.54-2	-9.55-2

(continued on next page)

Table 1 (continued)

Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$	Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$
3s <sub>1/2</sub>	1	-9.41-4	-8.94-4	1.54-5	2.21-5	-3.75-5	3s <sub>1/2</sub>	1	-1.21-3	-1.03-3	5.91-5	8.40-5	-1.43-4
	3	-1.76-2	-5.16-3	4.17-3	5.81-3	-9.98-3		3	-1.52-2	-4.58-3	3.55-3	4.94-3	-8.50-3
	5	-4.97-2	-1.35-2	1.21-2	1.69-2	-2.91-2		5	-4.59-2	-1.26-2	1.12-2	1.56-2	-2.68-2
	10	-1.46-1	-3.88-2	3.61-2	5.01-2	-8.62-2		10	-1.40-1	-3.71-2	3.46-2	4.80-2	-8.26-2
3p <sub>1/2</sub>	1	-1.15-2	-2.06-3	8.63-4	3.97-3	-4.83-3	3p <sub>1/2</sub>	1	-1.05-2	-1.85-3	7.59-4	3.62-3	-4.38-3
	3	-6.52-2	-1.23-2	4.54-3	2.21-2	-2.66-2		3	-6.29-2	-1.18-2	4.67-3	2.14-2	-2.61-2
	5	-1.23-1	-2.30-2	5.78-3	4.12-2	-4.70-2		5	-1.21-1	-2.26-2	6.37-3	4.05-2	-4.69-2
	10	-2.69-1	-4.99-2	4.36-3	8.87-2	-9.30-2		10	-2.66-1	-4.94-2	5.66-3	8.79-2	-9.35-2
3p <sub>3/2</sub>	1	-8.95-3	-2.44-3	1.91-3	2.99-3	-4.90-3	3p <sub>3/2</sub>	1	-7.97-3	-2.23-3	1.80-3	2.66-3	-4.45-3
	3	-5.53-2	-1.37-2	8.52-3	1.83-2	-2.69-2		3	-5.32-2	-1.32-2	8.59-3	1.77-2	-2.63-2
	5	-1.05-1	-2.56-2	1.29-2	3.43-2	-4.72-2		5	-1.03-1	-2.52-2	1.34-2	3.37-2	-4.71-2
	10	-2.29-1	-5.54-2	1.91-2	7.33-2	-9.24-2		10	-2.27-1	-5.49-2	2.02-2	7.28-2	-9.31-2
4s <sub>1/2</sub>	1	-1.10-3	-1.04-3	1.96-5	2.82-5	-4.77-5	4s <sub>1/2</sub>	1	-1.25-3	-1.06-3	6.01-5	8.59-5	-1.46-4
	3	-1.73-2	-5.12-3	4.10-3	5.71-3	-9.81-3		3	-1.52-2	-4.71-3	3.54-3	4.92-3	-8.46-3
	5	-4.95-2	-1.35-2	1.21-2	1.68-2	-2.89-2		5	-4.58-2	-1.26-2	1.11-2	1.55-2	-2.66-2
	10	-1.46-1	-3.88-2	3.61-2	5.01-2	-8.61-2		10	-1.40-1	-3.72-2	3.45-2	4.80-2	-8.25-2
<i>Z</i> = 21, Sc: 4s <sub>1/2</sub> <sup>2</sup> 3d <sub>3/2</sub> <sup>1</sup>							<i>Z</i> = 22, Ti: 4s <sub>1/2</sub> <sup>2</sup> 3d <sub>3/2</sub> <sup>2</sup>						
2s <sub>1/2</sub>	1	-1.88-3	-1.20-3	2.27-4	3.19-4	-5.46-4	2s <sub>1/2</sub>	1	-2.65-3	-1.49-3	3.86-4	5.42-4	-9.28-4
	3	-1.48-2	-4.27-3	3.54-3	4.91-3	-8.45-3		3	-1.27-2	-3.79-3	3.00-3	4.16-3	-7.17-3
	5	-4.46-2	-1.19-2	1.10-2	1.53-2	-2.63-2		5	-4.10-2	-1.10-2	1.01-2	1.40-2	-2.41-2
	10	-1.38-1	-3.62-2	3.42-2	4.74-2	-8.16-2		10	-1.32-1	-3.47-2	3.28-2	4.54-2	-7.82-2
2p <sub>1/2</sub>	1	-1.49-2	-1.88-3	6.96-4	5.35-3	-6.05-3	2p <sub>1/2</sub>	1	-1.40-2	-1.55-3	5.09-4	5.08-3	-5.59-3
	3	-6.98-2	-1.27-2	4.86-3	2.38-2	-2.87-2		3	-6.85-2	-1.23-2	4.93-3	2.35-2	-2.84-2
	5	-1.28-1	-2.36-2	6.76-3	4.30-2	-4.98-2		5	-1.26-1	-2.33-2	7.20-3	4.26-2	-4.98-2
	10	-2.73-1	-5.08-2	6.58-3	9.04-2	-9.69-2		10	-2.71-1	-5.04-2	7.75-3	8.99-2	-9.77-2
2p <sub>3/2</sub>	1	-1.13-2	-2.35-3	2.13-3	4.01-3	-6.14-3	2p <sub>3/2</sub>	1	-1.03-2	-2.03-3	1.99-3	3.70-3	-5.69-3
	3	-5.95-2	-1.42-2	9.08-3	1.99-2	-2.90-2		3	-5.82-2	-1.38-2	9.16-3	1.96-2	-2.88-2
	5	-1.09-1	-2.64-2	1.41-2	3.60-2	-5.01-2		5	-1.08-1	-2.60-2	1.45-2	3.58-2	-5.02-2
	10	-2.34-1	-5.64-2	2.13-2	7.53-2	-9.66-2		10	-2.33-1	-5.61-2	2.25-2	7.51-2	-9.76-2
3s <sub>1/2</sub>	1	-1.63-3	-1.20-3	1.41-4	2.00-4	-3.41-4	3s <sub>1/2</sub>	1	-2.18-3	-1.39-3	2.60-4	3.68-4	-6.29-4
	3	-1.30-2	-4.10-3	2.98-3	4.14-3	-7.12-3		3	-1.10-2	-3.68-3	2.46-3	3.41-3	-5.87-3
	5	-4.20-2	-1.16-2	1.02-2	1.42-2	-2.44-2		5	-3.82-2	-1.07-2	9.26-3	1.29-2	-2.21-2
	10	-1.34-1	-3.55-2	3.31-2	4.59-2	-7.90-2		10	-1.28-1	-3.40-2	3.16-2	4.38-2	-7.54-2
3p <sub>1/2</sub>	1	-9.38-3	-1.61-3	6.21-4	3.23-3	-3.85-3	3p <sub>1/2</sub>	1	-8.28-3	-1.37-3	4.76-4	2.86-3	-3.33-3
	3	-6.03-2	-1.12-2	4.71-3	2.06-2	-2.53-2		3	-5.77-2	-1.06-2	4.69-3	1.98-2	-2.44-2
	5	-1.18-1	-2.21-2	6.88-3	3.98-2	-4.66-2		5	-1.15-1	-2.16-2	7.31-3	3.90-2	-4.63-2
	10	-2.63-1	-4.88-2	6.84-3	8.70-2	-9.38-2		10	-2.59-1	-4.81-2	7.95-3	8.60-2	-9.40-2
3p <sub>3/2</sub>	1	-6.89-3	-1.98-3	1.64-3	2.29-3	-3.94-3	3p <sub>3/2</sub>	1	-5.83-3	-1.74-3	1.48-3	1.93-3	-3.41-3
	3	-5.09-2	-1.26-2	8.56-3	1.70-2	-2.56-2		3	-4.85-2	-1.20-2	8.48-3	1.63-2	-2.48-2
	5	-1.01-1	-2.47-2	1.38-2	3.31-2	-4.70-2		5	-9.82-2	-2.41-2	1.42-2	3.25-2	-4.67-2
	10	-2.24-1	-5.42-2	2.13-2	7.22-2	-9.35-2		10	-2.21-1	-5.35-2	2.23-2	7.15-2	-9.38-2
3d <sub>3/2</sub>	1	-2.92-2	-5.54-3	-1.22-4	9.44-3	-9.32-3	3d <sub>3/2</sub>	1	-2.81-2	-5.29-3	-9.61-6	9.12-3	-9.11-3
	3	-1.20-1	-2.35-2	-4.87-3	3.75-2	-3.26-2		3	-1.17-1	-2.29-2	-4.11-3	3.70-2	-3.29-2
	5	-2.06-1	-4.12-2	-1.54-2	6.28-2	-4.73-2		5	-2.05-1	-4.12-2	-1.37-2	6.30-2	-4.93-2
	10	-4.31-1	-8.76-2	-4.70-2	1.28-1	-8.10-2		10	-4.25-1	-8.56-2	-4.45-2	1.27-1	-8.23-2
4s <sub>1/2</sub>	1	-1.81-3	-1.34-3	1.54-4	2.18-4	-3.71-4	4s <sub>1/2</sub>	1	-2.37-3	-1.50-3	2.85-4	4.03-4	-6.88-4
	3	-1.27-2	-4.05-3	2.90-3	4.03-3	-6.93-3		3	-1.09-2	-3.75-3	2.42-3	3.35-3	-5.77-3
	5	-4.19-2	-1.16-2	1.02-2	1.41-2	-2.43-2		5	-3.79-2	-1.07-2	9.17-3	1.27-2	-2.19-2
	10	-1.34-1	-3.55-2	3.30-2	4.58-2	-7.88-2		10	-1.28-1	-3.40-2	3.15-2	4.37-2	-7.52-2
<i>Z</i> = 23, V: 4s <sub>1/2</sub> <sup>2</sup> 3d <sub>3/2</sub> <sup>3</sup>							<i>Z</i> = 24, Cr: 4s <sub>1/2</sub> <sup>1</sup> 3d <sub>3/2</sub> <sup>4</sup> 3d <sub>5/2</sub> <sup>1</sup>						
2s <sub>1/2</sub>	1	-3.65-3	-1.84-3	5.98-4	8.42-4	-1.44-3	2s <sub>1/2</sub>	1	-4.96-3	-2.29-3	8.87-4	1.25-3	-2.13-3
	3	-1.08-2	-3.37-3	2.51-3	3.47-3	-5.97-3		3	-9.03-3	-3.00-3	2.04-3	2.82-3	-4.86-3
	5	-3.75-2	-1.01-2	9.22-3	1.28-2	-2.20-2		5	-3.40-2	-9.29-3	8.35-3	1.16-2	-1.99-2
	10	-1.26-1	-3.31-2	3.13-2	4.34-2	-7.48-2		10	-1.20-1	-3.16-2	2.99-2	4.15-2	-7.14-2
2p <sub>1/2</sub>	1	-1.31-2	-1.21-3	3.09-4	4.80-3	-5.11-3	2p <sub>1/2</sub>	1	-1.22-2	-8.81-4	8.32-5	4.53-3	-4.61-3
	3	-6.70-2	-1.18-2	4.94-3	2.31-2	-2.80-2		3	-6.55-2	-1.13-2	4.89-3	2.27-2	-2.75-2
	5	-1.25-1	-2.29-2	7.59-3	4.22-2	-4.98-2		5	-1.23-1	-2.25-2	7.92-3	4.18-2	-4.98-2
	10	-2.69-1	-5.00-2	8.84-3	8.95-2	-9.83-2		10	-2.67-1	-4.96-2	9.88-3	8.90-2	-9.89-2

Table 1 (continued)

Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$	Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$
2p <sub>3/2</sub>	1	-9.21-3	-1.71-3	1.85-3	3.37-3	-5.22-3	2p <sub>3/2</sub>	1	-8.14-3	-1.39-3	1.68-3	3.04-3	-4.72-3
	3	-5.68-2	-1.34-2	9.19-3	1.92-2	-2.84-2		3	-5.54-2	-1.29-2	9.17-3	1.88-2	-2.80-2
	5	-1.07-1	-2.56-2	1.49-2	3.55-2	-5.03-2		5	-1.06-1	-2.52-2	1.52-2	3.52-2	-5.04-2
	10	-2.31-1	-5.57-2	2.35-2	7.49-2	-9.84-2		10	-2.30-1	-5.53-2	2.45-2	7.46-2	-9.91-2
3s <sub>1/2</sub>	1	-2.85-3	-1.60-3	4.12-4	5.81-4	-9.93-4	3s <sub>1/2</sub>	1	-3.69-3	-1.85-3	6.08-4	8.58-4	-1.47-3
	3	-9.23-3	-3.34-3	1.99-3	2.75-3	-4.74-3		3	-7.69-3	-3.07-3	1.56-3	2.16-3	-3.72-3
	5	-3.45-2	-9.79-3	8.32-3	1.15-2	-1.99-2		5	-3.09-2	-8.94-3	7.40-3	1.03-2	-1.77-2
	10	-1.22-1	-3.25-2	3.01-2	4.17-2	-7.18-2		10	-1.16-1	-3.11-2	2.86-2	3.96-2	-6.82-2
3p <sub>1/2</sub>	1	-7.21-3	-1.15-3	3.25-4	2.49-3	-2.81-3	3p <sub>1/2</sub>	1	-6.18-3	-9.49-4	1.64-4	2.13-3	-2.29-3
	3	-5.50-2	-1.00-2	4.61-3	1.89-2	-2.35-2		3	-5.24-2	-9.46-3	4.50-3	1.81-2	-2.26-2
	5	-1.12-1	-2.09-2	7.63-3	3.80-2	-4.57-2		5	-1.09-1	-2.02-2	7.88-3	3.71-2	-4.50-2
	10	-2.56-1	-4.75-2	9.02-3	8.50-2	-9.40-2		10	-2.52-1	-4.69-2	1.01-2	8.41-2	-9.42-2
3p <sub>3/2</sub>	1	-4.81-3	-1.52-3	1.32-3	1.58-3	-2.90-3	3p <sub>3/2</sub>	1	-3.81-3	-1.31-3	1.15-3	1.23-3	-2.38-3
	3	-4.61-2	-1.14-2	8.35-3	1.55-2	-2.39-2		3	-4.37-2	-1.09-2	8.19-3	1.48-2	-2.30-2
	5	-9.56-2	-2.34-2	1.44-2	3.18-2	-4.62-2		5	-9.29-2	-2.27-2	1.46-2	3.10-2	-4.56-2
	10	-2.18-1	-5.29-2	2.32-2	7.08-2	-9.40-2		10	-2.16-1	-5.23-2	2.42-2	7.02-2	-9.44-2
3d <sub>3/2</sub>	1	-2.70-2	-5.06-3	7.88-5	8.81-3	-8.89-3	3d <sub>3/2</sub>	1	-2.60-2	-4.78-3	1.28-4	8.51-3	-8.64-3
	3	-1.14-1	-2.20-2	-3.49-3	3.62-2	-3.27-2		3	-1.11-1	-2.11-2	-2.96-3	3.54-2	-3.24-2
	5	-2.05-1	-4.09-2	-1.21-2	6.31-2	-5.10-2		5	-2.03-1	-4.03-2	-1.07-2	6.30-2	-5.24-2
	10	-4.19-1	-8.39-2	-4.24-2	1.26-1	-8.32-2		10	-4.15-1	-8.28-2	-4.01-2	1.25-1	-8.45-2
4s <sub>1/2</sub>	1	-2.94-3	-1.61-3	4.37-4	6.17-4	-1.05-3	3d <sub>5/2</sub>	1	-2.31-2	-5.18-3	1.23-3	7.41-3	-8.65-3
	3	-9.17-3	-3.44-3	1.93-3	2.68-3	-4.61-3		3	-1.02-1	-2.26-2	6.40-4	3.19-2	-3.25-2
	5	-3.42-2	-9.78-3	8.22-3	1.14-2	-1.96-2		5	-1.88-1	-4.30-2	-4.60-3	5.72-2	-5.26-2
	10	-1.22-1	-3.26-2	3.00-2	4.16-2	-7.16-2		10	-3.88-1	-8.92-2	-2.83-2	1.14-1	-8.57-2
Z = 25, Mn: 4s <sub>1/2</sub> <sup>2</sup> 3d <sub>3/2</sub> <sup>4</sup> 3d <sub>5/2</sub> <sup>1</sup>													
2s <sub>1/2</sub>	1	-6.25-3	-2.70-3	1.17-3	1.65-3	-2.83-3	2s <sub>1/2</sub>	1	-7.84-3	-3.20-3	1.54-3	2.16-3	-3.70-3
	3	-7.58-3	-2.72-3	1.65-3	2.27-3	-3.93-3		3	-6.33-3	-2.51-3	1.31-3	1.79-3	-3.10-3
	5	-3.07-2	-8.49-3	7.52-3	1.04-2	-1.79-2		5	-2.75-2	-7.72-3	6.70-3	9.26-3	-1.60-2
	10	-1.15-1	-3.02-2	2.85-2	3.95-2	-6.80-2		10	-1.09-1	-2.87-2	2.71-2	3.75-2	-6.46-2
2p <sub>1/2</sub>	1	-1.12-2	-5.36-4	-1.15-4	4.25-3	-4.13-3	2p <sub>1/2</sub>	1	-1.03-2	-1.87-4	-3.38-4	3.97-3	-3.63-3
	3	-6.37-2	-1.07-2	4.80-3	2.22-2	-2.70-2		3	-6.20-2	-1.02-2	4.66-3	2.17-2	-2.63-2
	5	-1.21-1	-2.20-2	8.19-3	4.14-2	-4.96-2		5	-1.19-1	-2.15-2	8.37-3	4.09-2	-4.92-2
	10	-2.65-1	-4.91-2	1.08-2	8.85-2	-9.93-2		10	-2.63-1	-4.87-2	1.17-2	8.79-2	-9.97-2
2p <sub>3/2</sub>	1	-7.04-3	-1.06-3	1.54-3	2.70-3	-4.24-3	2p <sub>3/2</sub>	1	-5.92-3	-7.32-4	1.39-3	2.35-3	-3.74-3
	3	-5.36-2	-1.23-2	9.10-3	1.83-2	-2.74-2		3	-5.19-2	-1.18-2	9.00-3	1.78-2	-2.68-2
	5	-1.04-1	-2.48-2	1.54-2	3.48-2	-5.03-2		5	-1.02-1	-2.43-2	1.56-2	3.44-2	-5.00-2
	10	-2.28-1	-5.48-2	2.54-2	7.43-2	-9.97-2		10	-2.26-1	-5.44-2	2.63-2	7.40-2	-1.00-1
3s <sub>1/2</sub>	1	-4.42-3	-2.04-3	7.86-4	1.11-3	-1.89-3	3s <sub>1/2</sub>	1	-5.28-3	-2.26-3	1.00-3	1.41-3	-2.41-3
	3	-6.44-3	-2.87-3	1.21-3	1.67-3	-2.88-3		3	-5.39-3	-2.74-3	9.07-4	1.24-3	-2.15-3
	5	-2.76-2	-8.17-3	6.55-3	9.06-3	-1.56-2		5	-2.44-2	-7.48-3	5.74-3	7.93-3	-1.37-2
	10	-1.10-1	-2.96-2	2.71-2	3.75-2	-6.47-2		10	-1.04-1	-2.81-2	2.56-2	3.54-2	-6.11-2
3p <sub>1/2</sub>	1	-5.29-3	-7.77-4	3.68-5	1.81-3	-1.85-3	3p <sub>1/2</sub>	1	-4.47-3	-6.27-4	-9.09-5	1.52-3	-1.43-3
	3	-4.97-2	-8.88-3	4.37-3	1.72-2	-2.16-2		3	-4.71-2	-8.32-3	4.19-3	1.63-2	-2.05-2
	5	-1.06-1	-1.95-2	8.01-3	3.60-2	-4.40-2		5	-1.02-1	-1.87-2	8.07-3	3.49-2	-4.30-2
	10	-2.48-1	-4.63-2	1.11-2	8.31-2	-9.41-2		10	-2.45-1	-4.57-2	1.20-2	8.21-2	-9.41-2
3p <sub>3/2</sub>	1	-2.95-3	-1.14-3	1.01-3	9.26-4	-1.93-3	3p <sub>3/2</sub>	1	-2.15-3	-9.85-4	8.69-4	6.38-4	-1.51-3
	3	-4.13-2	-1.03-2	8.00-3	1.40-2	-2.20-2		3	-3.89-2	-9.70-3	7.78-3	1.32-2	-2.10-2
	5	-8.98-2	-2.20-2	1.46-2	3.01-2	-4.47-2		5	-8.68-2	-2.12-2	1.46-2	2.91-2	-4.38-2
	10	-2.13-1	-5.17-2	2.50-2	6.95-2	-9.45-2		10	-2.10-1	-5.10-2	2.59-2	6.88-2	-9.46-2
3d <sub>3/2</sub>	1	-2.47-2	-4.48-3	1.60-4	8.14-3	-8.30-3	3d <sub>3/2</sub>	1	-2.35-2	-4.16-3	1.45-4	7.75-3	-7.89-3
	3	-1.08-1	-2.05-2	-2.45-3	3.46-2	-3.22-2		3	-1.06-1	-1.99-2	-1.96-3	3.39-2	-3.19-2
	5	-2.01-1	-3.95-2	-9.40-3	6.26-2	-5.32-2		5	-1.97-1	-3.85-2	-8.25-3	6.19-2	-5.37-2
	10	-4.11-1	-8.21-2	-3.77-2	1.24-1	-8.61-2		10	-4.09-1	-8.19-2	-3.53-2	1.24-1	-8.83-2

(continued on next page)

Table 1 (continued)

Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$	Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$
3d <sub>5/2</sub>	1	-2.19-2	-4.88-3	1.25-3	7.06-3	-8.31-3	3d <sub>5/2</sub>	1	-2.07-2	-4.54-3	1.22-3	6.69-3	-7.91-3
	3	-9.92-2	-2.20-2	1.11-3	3.11-2	-3.22-2		3	-9.65-2	-2.14-2	1.56-3	3.04-2	-3.19-2
	5	-1.86-1	-4.22-2	-3.36-3	5.69-2	-5.35-2		5	-1.83-1	-4.12-2	-2.28-3	5.62-2	-5.39-2
	10	-3.85-1	-8.86-2	-2.62-2	1.13-1	-8.72-2		10	-3.83-1	-8.83-2	-2.37-2	1.13-1	-8.95-2
4s <sub>1/2</sub>	1	-4.34-3	-1.99-3	7.77-4	1.10-3	-1.87-3	4s <sub>1/2</sub>	1	-5.22-3	-2.25-3	9.80-4	1.38-3	-2.36-3
	3	-6.31-3	-2.90-3	1.16-3	1.60-3	-2.75-3		3	-5.43-3	-2.89-3	8.68-4	1.19-3	-2.06-3
	5	-2.73-2	-8.18-3	6.44-3	8.92-3	-1.54-2		5	-2.42-2	-7.52-3	5.63-3	7.79-3	-1.34-2
	10	-1.09-1	-2.96-2	2.70-2	3.73-2	-6.43-2		10	-1.03-1	-2.81-2	2.55-2	3.52-2	-6.07-2
Z = 27, Co: 4s^2_1/2 3d^4_3/2 3d^3_5/2	1	-9.62-3	-3.74-3	1.95-3	2.74-3	-4.68-3	Z = 28, Ni: 4s^2_1/2 3d^4_3/2 3d^4_5/2	1	-1.16-2	-4.32-3	2.40-3	3.37-3	-5.77-3
	3	-5.35-3	-2.39-3	1.02-3	1.39-3	-2.41-3		3	-4.63-3	-2.34-3	7.97-4	1.08-3	-1.87-3
	5	-2.45-2	-7.01-3	5.93-3	8.17-3	-1.41-2		5	-2.16-2	-6.37-3	5.20-3	7.14-3	-1.23-2
	10	-1.03-1	-2.72-2	2.57-2	3.55-2	-6.12-2		10	-9.75-2	-2.58-2	2.43-2	3.36-2	-5.79-2
2p <sub>1/2</sub>	1	-9.31-3	1.63-4	-5.65-4	3.68-3	-3.11-3	2p <sub>1/2</sub>	1	-8.37-3	5.11-4	-7.94-4	3.39-3	-2.60-3
	3	-6.02-2	-9.57-3	4.46-3	2.11-2	-2.56-2		3	-5.83-2	-8.95-3	4.24-3	2.06-2	-2.48-2
	5	-1.17-1	-2.08-2	8.47-3	4.03-2	-4.88-2		5	-1.15-1	-2.02-2	8.51-3	3.97-2	-4.82-2
	10	-2.60-1	-4.82-2	1.26-2	8.74-2	-1.00-1		10	-2.58-1	-4.77-2	1.34-2	8.68-2	-1.00-1
2p <sub>3/2</sub>	1	-4.78-3	-4.02-4	1.23-3	2.00-3	-3.23-3	2p <sub>3/2</sub>	1	-3.65-3	-7.54-5	1.08-3	1.64-3	-2.73-3
	3	-5.01-2	-1.12-2	8.84-3	1.73-2	-2.62-2		3	-4.82-2	-1.06-2	8.67-3	1.68-2	-2.54-2
	5	-1.01-1	-2.37-2	1.58-2	3.39-2	-4.97-2		5	-9.86-2	-2.30-2	1.58-2	3.34-2	-4.92-2
	10	-2.25-1	-5.39-2	2.71-2	7.37-2	-1.01-1		10	-2.23-1	-5.35-2	2.79-2	7.34-2	-1.01-1
3s <sub>1/2</sub>	1	-6.13-3	-2.45-3	1.22-3	1.72-3	-2.93-3	3s <sub>1/2</sub>	1	-6.98-3	-2.62-3	1.44-3	2.03-3	-3.47-3
	3	-4.58-3	-2.66-3	6.58-4	8.97-4	-1.56-3		3	-4.00-3	-2.65-3	4.68-4	6.33-4	-1.10-3
	5	-2.15-2	-6.86-3	4.97-3	6.86-3	-1.18-2		5	-1.89-2	-6.31-3	4.27-3	5.88-3	-1.01-2
	10	-9.79-2	-2.66-2	2.41-2	3.33-2	-5.74-2		10	-9.19-2	-2.51-2	2.26-2	3.12-2	-5.39-2
3p <sub>1/2</sub>	1	-3.76-3	-5.11-4	-2.02-4	1.26-3	-1.06-3	3p <sub>1/2</sub>	1	-3.17-3	-4.29-4	-2.94-4	1.04-3	-7.42-4
	3	-4.45-2	-7.76-3	3.98-3	1.55-2	-1.95-2		3	-4.19-2	-7.19-3	3.75-3	1.46-2	-1.84-2
	5	-9.85-2	-1.79-2	8.08-3	3.38-2	-4.19-2		5	-9.49-2	-1.72-2	8.03-3	3.27-2	-4.07-2
	10	-2.41-1	-4.49-2	1.29-2	8.10-2	-9.39-2		10	-2.37-1	-4.41-2	1.36-2	7.98-2	-9.35-2
3p <sub>3/2</sub>	1	-1.45-3	-8.66-4	7.53-4	3.83-4	-1.14-3	3p <sub>3/2</sub>	1	-8.58-4	-7.81-4	6.57-4	1.62-4	-8.19-4
	3	-3.65-2	-9.15-3	7.53-3	1.25-2	-2.00-2		3	-3.41-2	-8.58-3	7.26-3	1.17-2	-1.89-2
	5	-8.37-2	-2.04-2	1.46-2	2.82-2	-4.28-2		5	-8.05-2	-1.97-2	1.44-2	2.72-2	-4.17-2
	10	-2.07-1	-5.03-2	2.67-2	6.80-2	-9.47-2		10	-2.04-1	-4.95-2	2.73-2	6.72-2	-9.45-2
3d <sub>3/2</sub>	1	-2.21-2	-3.83-3	1.05-4	7.35-3	-7.45-3	3d <sub>3/2</sub>	1	-2.09-2	-3.52-3	4.66-5	6.95-3	-7.00-3
	3	-1.03-1	-1.93-2	-1.50-3	3.31-2	-3.16-2		3	-1.00-1	-1.88-2	-1.09-3	3.24-2	-3.13-2
	5	-1.94-1	-3.75-2	-7.22-3	6.11-2	-5.39-2		5	-1.90-1	-3.65-2	-6.30-3	6.02-2	-5.39-2
	10	-4.07-1	-8.17-2	-3.29-2	1.24-1	-9.08-2		10	-4.06-1	-8.13-2	-3.04-2	1.24-1	-9.33-2
3d <sub>5/2</sub>	1	-1.94-2	-4.21-3	1.17-3	6.30-3	-7.47-3	3d <sub>5/2</sub>	1	-1.81-2	-3.90-3	1.11-3	5.92-3	-7.02-3
	3	-9.39-2	-2.07-2	1.98-3	2.97-2	-3.16-2		3	-9.15-2	-2.02-2	2.35-3	2.90-2	-3.14-2
	5	-1.79-1	-4.02-2	-1.34-3	5.54-2	-5.41-2		5	-1.76-1	-3.92-2	-4.84-4	5.46-2	-5.41-2
	10	-3.82-1	-8.81-2	-2.14-2	1.13-1	-9.20-2		10	-3.81-1	-8.77-2	-1.90-2	1.13-1	-9.45-2
4s <sub>1/2</sub>	1	-6.10-3	-2.48-3	1.19-3	1.69-3	-2.88-3	4s <sub>1/2</sub>	1	-6.92-3	-2.65-3	1.41-3	1.99-3	-3.40-3
	3	-4.57-3	-2.79-3	6.12-4	8.35-4	-1.45-3		3	-3.85-3	-2.66-3	4.15-4	5.62-4	-9.78-4
	5	-2.12-2	-6.86-3	4.85-3	6.70-3	-1.15-2		5	-1.84-2	-6.24-3	4.13-3	5.69-3	-9.82-3
	10	-9.73-2	-2.66-2	2.40-2	3.31-2	-5.71-2		10	-9.13-2	-2.50-2	2.24-2	3.10-2	-5.34-2
Z = 29, Cu: 4s <sub>1/2</sub> 3d <sub>3/2</sub> 3d <sub>6/2</sub>	1	-1.39-2	-4.99-3	2.95-3	4.15-3	-7.09-3	Z = 30, Zn: 4s <sub>2/2</sub> 3d <sub>3/2</sub> 3d <sub>6/2</sub>	1	-1.59-2	-5.57-3	3.43-3	4.83-3	-8.26-3
	3	-4.19-3	-2.38-3	6.31-4	8.47-4	-1.48-3		3	-4.04-3	-2.50-3	5.41-4	7.24-4	-1.26-3
	5	-1.90-2	-5.79-3	4.50-3	6.17-3	-1.07-2		5	-1.66-2	-5.30-3	3.88-3	5.30-3	-9.18-3
	10	-9.19-2	-2.44-2	2.29-2	3.16-2	-5.45-2		10	-8.64-2	-2.30-2	2.16-2	2.97-2	-5.12-2
2p <sub>1/2</sub>	1	-7.38-3	8.81-4	-1.05-3	3.09-3	-2.05-3	2p <sub>1/2</sub>	1	-6.62-3	1.19-3	-1.26-3	2.87-3	-1.61-3
	3	-5.64-2	-8.30-3	3.97-3	2.00-2	-2.40-2		3	-5.45-2	-7.67-3	3.70-3	1.95-2	-2.32-2
	5	-1.13-1	-1.95-2	8.49-3	3.91-2	-4.76-2		5	-1.11-1	-1.88-2	8.41-3	3.85-2	-4.69-2
	10	-2.56-1	-4.71-2	1.41-2	8.63-2	-1.00-1		10	-2.53-1	-4.65-2	1.48-2	8.57-2	-1.00-1
2p <sub>3/2</sub>	1	-2.42-3	2.69-4	9.15-4	1.26-3	-2.17-3	2p <sub>3/2</sub>	1	-1.44-3	5.51-4	7.91-4	9.53-4	-1.74-3
	3	-4.62-2	-1.00-2	8.46-3	1.62-2	-2.47-2		3	-4.43-2	-9.41-3	8.26-3	1.56-2	-2.39-2
	5	-9.66-2	-2.24-2	1.59-2	3.29-2	-4.87-2		5	-9.45-2	-2.17-2	1.58-2	3.23-2	-4.81-2
	10	-2.21-1	-5.30-2	2.87-2	7.31-2	-1.02-1		10	-2.20-1	-5.24-2	2.93-2	7.28-2	-1.02-1

Table 1 (continued)

Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$	Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$
3s <sub>1/2</sub>	1	-7.91–3	-2.78–3	1.69–3	2.39–3	-4.08–3	3s <sub>1/2</sub>	1	-8.60–3	-2.89–3	1.89–3	2.66–3	-4.55–3
	3	-3.65–3	-2.70–3	3.31–4	4.46–4	-7.77–4		3	-3.56–3	-2.81–3	2.62–4	3.52–4	-6.14–4
	5	-1.64–2	-5.84–3	3.61–3	4.95–3	-8.56–3		5	-1.43–2	-5.45–3	3.03–3	4.14–3	-7.17–3
	10	-8.59–2	-2.36–2	2.11–2	2.92–2	-5.03–2		10	-8.02–2	-2.22–2	1.97–2	2.71–2	-4.68–2
3p <sub>1/2</sub>	1	-2.67–3	-3.75–4	-3.76–4	8.42–4	-4.66–4	3p <sub>1/2</sub>	1	-2.38–3	-3.67–4	-4.20–4	7.20–4	-3.00–4
	3	-3.93–2	-6.62–3	3.48–3	1.38–2	-1.72–2		3	-3.68–2	-6.07–3	3.21–3	1.29–2	-1.61–2
	5	-9.14–2	-1.64–2	7.93–3	3.16–2	-3.95–2		5	-8.79–2	-1.56–2	7.80–3	3.05–2	-3.83–2
	10	-2.33–1	-4.33–2	1.43–2	7.86–2	-9.29–2		10	-2.28–1	-4.23–2	1.48–2	7.74–2	-9.22–2
3p <sub>3/2</sub>	1	-3.40–4	-7.26–4	5.77–4	-3.90–5	-5.38–4	3p <sub>3/2</sub>	1	-3.11–5	-7.15–4	5.33–4	-1.67–4	-3.66–4
	3	-3.17–2	-8.01–3	6.96–3	1.09–2	-1.78–2		3	-2.94–2	-7.46–3	6.64–3	1.01–2	-1.67–2
	5	-7.74–2	-1.89–2	1.43–2	2.62–2	-4.05–2		5	-7.43–2	-1.82–2	1.41–2	2.53–2	-3.94–2
	10	-2.00–1	-4.87–2	2.79–2	6.63–2	-9.42–2		10	-1.97–1	-4.77–2	2.84–2	6.53–2	-9.37–2
3d <sub>3/2</sub>	1	-1.98–2	-3.30–3	-3.80–5	6.61–3	-6.57–3	3d <sub>3/2</sub>	1	-1.84–2	-2.97–3	-9.87–5	6.17–3	-6.07–3
	3	-9.83–2	-1.83–2	-7.03–4	3.18–2	-3.11–2		3	-9.58–2	-1.78–2	-3.52–4	3.12–2	-3.08–2
	5	-1.87–1	-3.57–2	-5.45–3	5.94–2	-5.39–2		5	-1.83–1	-3.48–2	-4.62–3	5.84–2	-5.38–2
	10	-4.04–1	-8.07–2	-2.80–2	1.24–1	-9.57–2		10	-4.01–1	-7.98–2	-2.57–2	1.23–1	-9.77–2
3d <sub>5/2</sub>	1	-1.71–2	-3.67–3	1.02–3	5.57–3	-6.59–3	3d <sub>5/2</sub>	1	-1.57–2	-3.33–3	9.52–4	5.14–3	-6.09–3
	3	-8.94–2	-1.97–2	2.71–3	2.84–2	-3.11–2		3	-8.71–2	-1.91–2	3.01–3	2.78–2	-3.08–2
	5	-1.73–1	-3.83–2	3.33–4	5.38–2	-5.41–2		5	-1.69–1	-3.74–2	1.09–3	5.28–2	-5.39–2
	10	-3.79–1	-8.71–2	-1.68–2	1.14–1	-9.68–2		10	-3.77–1	-8.61–2	-1.46–2	1.13–1	-9.87–2
4s <sub>1/2</sub>	1	-7.21–3	-2.46–3	1.57–3	2.21–3	-3.78–3	4s <sub>1/2</sub>	1	-8.10–3	-2.72–3	1.78–3	2.51–3	-4.29–3
	3	-3.58–3	-2.75–3	2.91–4	3.91–4	-6.81–4		3	-3.52–3	-2.84–3	2.37–4	3.19–4	-5.56–4
	5	-1.60–2	-5.81–3	3.49–3	4.79–3	-8.27–3		5	-1.41–2	-5.52–3	2.92–3	4.00–3	-6.92–3
	10	-8.53–2	-2.36–2	2.09–2	2.89–2	-4.98–2		10	-7.95–2	-2.22–2	1.95–2	2.68–2	-4.63–2
$Z = 31$ , Ga: $4s^2_{1/2}3d^4_{3/2}3d^6_{5/2}4p^1_{1/2}$							$Z = 32$ , Ge: $4s^2_{1/2}3d^4_{3/2}3d^6_{5/2}4p^2_{1/2}$						
2s <sub>1/2</sub>	1	-1.81–2	-6.17–3	3.94–3	5.55–3	-9.49–3	2s <sub>1/2</sub>	1	-2.03–2	-6.80–3	4.48–3	6.31–3	-1.08–2
	3	-4.16–3	-2.70–3	5.13–4	6.86–4	-1.20–3		3	-4.57–3	-2.99–3	5.52–4	7.44–4	-1.30–3
	5	-1.45–2	-4.90–3	3.32–3	4.52–3	-7.85–3		5	-1.27–2	-4.58–3	2.83–3	3.83–3	-6.66–3
	10	-8.10–2	-2.16–2	2.02–2	2.78–2	-4.80–2		10	-7.58–2	-2.03–2	1.89–2	2.60–2	-4.49–2
2p <sub>1/2</sub>	1	-5.88–3	1.51–3	-1.48–3	2.66–3	-1.19–3	2p <sub>1/2</sub>	1	-5.17–3	1.84–3	-1.69–3	2.46–3	-7.72–4
	3	-5.27–2	-7.01–3	3.41–3	1.90–2	-2.24–2		3	-5.09–2	-6.36–3	3.11–3	1.84–2	-2.15–2
	5	-1.09–1	-1.80–2	8.30–3	3.79–2	-4.62–2		5	-1.06–1	-1.73–2	8.11–3	3.73–2	-4.54–2
	10	-2.51–1	-4.59–2	1.53–2	8.51–2	-1.00–1		10	-2.49–1	-4.52–2	1.58–2	8.45–2	-1.00–1
2p <sub>3/2</sub>	1	-4.46–4	8.42–4	6.75–4	6.50–4	-1.33–3	2p <sub>3/2</sub>	1	5.46–4	1.14–3	5.66–4	3.49–4	-9.15–4
	3	-4.24–2	-8.79–3	8.05–3	1.51–2	-2.31–2		3	-4.05–2	-8.17–3	7.83–3	1.45–2	-2.23–2
	5	-9.24–2	-2.10–2	1.58–2	3.17–2	-4.75–2		5	-9.03–2	-2.04–2	1.57–2	3.11–2	-4.68–2
	10	-2.18–1	-5.19–2	3.00–2	7.24–2	-1.02–1		10	-2.16–1	-5.13–2	3.05–2	7.20–2	-1.02–1
3s <sub>1/2</sub>	1	-9.29–3	-2.99–3	2.08–3	2.94–3	-5.02–3	3s <sub>1/2</sub>	1	-9.95–3	-3.07–3	2.27–3	3.20–3	-5.47–3
	3	-3.68–3	-2.98–3	2.45–4	3.31–4	-5.76–4		3	-4.03–3	-3.20–3	2.84–4	3.89–4	-6.73–4
	5	-1.24–2	-5.14–3	2.51–3	3.43–3	-5.94–3		5	-1.09–2	-4.90–3	2.06–3	2.80–3	-4.86–3
	10	-7.47–2	-2.09–2	1.83–2	2.52–2	-4.35–2		10	-6.94–2	-1.97–2	1.69–2	2.33–2	-4.02–2
3p <sub>1/2</sub>	1	-2.22–3	-3.92–4	-4.47–4	6.43–4	-1.96–4	3p <sub>1/2</sub>	1	-2.18–3	-4.49–4	-4.58–4	6.03–4	-1.45–4
	3	-3.44–2	-5.53–3	2.93–3	1.21–2	-1.51–2		3	-3.20–2	-5.01–3	2.63–3	1.13–2	-1.40–2
	5	-8.45–2	-1.49–2	7.63–3	2.94–2	-3.70–2		5	-8.12–2	-1.42–2	7.41–3	2.83–2	-3.57–2
	10	-2.24–1	-4.14–2	1.53–2	7.60–2	-9.13–2		10	-2.19–1	-4.04–2	1.57–2	7.47–2	-9.03–2
3p <sub>3/2</sub>	1	1.59–4	-7.39–4	5.13–4	-2.57–4	-2.57–4	3p <sub>3/2</sub>	1	2.46–4	-7.95–4	5.13–4	-3.14–4	-1.99–4
	3	-2.71–2	-6.93–3	6.34–3	9.34–3	-1.57–2		3	-2.49–2	-6.41–3	6.02–3	8.59–3	-1.46–2
	5	-7.12–2	-1.74–2	1.39–2	2.43–2	-3.82–2		5	-6.82–2	-1.67–2	1.36–2	2.33–2	-3.69–2
	10	-1.93–1	-4.68–2	2.88–2	6.42–2	-9.31–2		10	-1.89–1	-4.59–2	2.91–2	6.32–2	-9.23–2
3d <sub>3/2</sub>	1	-1.74–2	-2.72–3	-1.57–4	5.84–3	-5.69–3	3d <sub>3/2</sub>	1	-1.65–2	-2.50–3	-2.15–4	5.56–3	-5.34–3
	3	-9.37–2	-1.72–2	-5.71–5	3.06–2	-3.05–2		3	-9.17–2	-1.67–2	2.01–4	3.00–2	-3.02–2
	5	-1.80–1	-3.41–2	-3.86–3	5.76–2	-5.37–2		5	-1.77–1	-3.34–2	-3.12–3	5.68–2	-5.37–2
	10	-3.98–1	-7.88–2	-2.35–2	1.23–1	-9.94–2		10	-3.95–1	-7.77–2	-2.15–2	1.22–1	-1.01–1
3d <sub>5/2</sub>	1	-1.47–2	-3.08–3	8.98–4	4.82–3	-5.72–3	3d <sub>5/2</sub>	1	-1.38–2	-2.87–3	8.51–4	4.53–3	-5.38–3
	3	-8.50–2	-1.86–2	3.28–3	2.72–2	-3.05–2		3	-8.31–2	-1.81–2	3.52–3	2.67–2	-3.02–2
	5	-1.66–1	-3.66–2	1.78–3	5.20–2	-5.38–2		5	-1.63–1	-3.60–2	2.47–3	5.13–2	-5.38–2
	10	-3.74–1	-8.51–2	-1.25–2	1.13–1	-1.00–1		10	-3.71–1	-8.40–2	-1.06–2	1.12–1	-1.02–1

(continued on next page)

Table 1 (continued)

Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$	Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$
4s <sub>1/2</sub>	1	-8.39-3	-2.71-3	1.88-3	2.65-3	-4.53-3	4s <sub>1/2</sub>	1	-8.77-3	-2.70-3	2.00-3	2.83-3	-4.84-3
	3	-3.72-3	-3.07-3	2.24-4	3.05-4	-5.29-4		3	-3.99-3	-3.22-3	2.61-4	3.60-4	-6.21-4
	5	-1.22-2	-5.19-3	2.40-3	3.28-3	-5.68-3		5	-1.06-2	-4.94-3	1.95-3	2.65-3	-4.60-3
	10	-7.39-2	-2.09-2	1.81-2	2.48-2	-4.29-2		10	-6.86-2	-1.96-2	1.67-2	2.29-2	-3.96-2
4p <sub>1/2</sub>	1	-2.00-3	-5.05-4	-3.64-4	5.24-4	-1.60-4	4p <sub>1/2</sub>	1	-1.93-3	-5.29-4	-3.66-4	4.89-4	-1.22-4
	3	-3.29-2	-5.43-3	2.85-3	1.16-2	-1.44-2		3	-3.02-2	-4.80-3	2.51-3	1.07-2	-1.32-2
	5	-8.26-2	-1.47-2	7.57-3	2.87-2	-3.63-2		5	-7.89-2	-1.39-2	7.38-3	2.75-2	-3.49-2
	10	-2.22-1	-4.10-2	1.54-2	7.53-2	-9.07-2		10	-2.17-1	-4.00-2	1.57-2	7.38-2	-8.95-2
<i>Z</i> = 33, As: 4s <sub>1/2</sub> <sup>2</sup> 3d <sub>3/2</sub> <sup>4</sup> 3d <sub>5/2</sub> <sup>6</sup> 4p <sub>1/2</sub> <sup>2</sup> 4p <sub>3/2</sub> <sup>1</sup>							<i>Z</i> = 34, Se: 4s <sub>1/2</sub> <sup>2</sup> 3d <sub>3/2</sub> <sup>4</sup> 3d <sub>5/2</sub> <sup>6</sup> 4p <sub>1/2</sub> <sup>2</sup> 4p <sub>3/2</sub> <sup>2</sup>						
2s <sub>1/2</sub>	1	-2.27-2	-7.44-3	5.05-3	7.11-3	-1.22-2	2s <sub>1/2</sub>	1	-2.52-2	-8.11-3	5.64-3	7.95-3	-1.36-2
	3	-5.25-3	-3.35-3	6.54-4	8.90-4	-1.54-3		3	-6.19-3	-3.79-3	8.18-4	1.12-3	-1.94-3
	5	-1.12-2	-4.35-3	2.40-3	3.22-3	-5.62-3		5	-9.94-3	-4.20-3	2.02-3	2.70-3	-4.72-3
	10	-7.07-2	-1.91-2	1.76-2	2.42-2	-4.18-2		10	-6.58-2	-1.79-2	1.64-2	2.24-2	-3.89-2
2p <sub>1/2</sub>	1	-4.43-3	2.19-3	-1.91-3	2.26-3	-3.51-4	2p <sub>1/2</sub>	1	-3.79-3	2.51-3	-2.13-3	2.09-3	3.98-5
	3	-4.92-2	-5.71-3	2.78-3	1.79-2	-2.07-2		3	-4.75-2	-5.07-3	2.44-3	1.74-2	-1.99-2
	5	-1.04-1	-1.66-2	7.92-3	3.66-2	-4.46-2		5	-1.02-1	-1.58-2	7.71-3	3.60-2	-4.38-2
	10	-2.46-1	-4.45-2	1.63-2	8.39-2	-1.00-1		10	-2.44-1	-4.38-2	1.66-2	8.33-2	-9.99-2
2p <sub>3/2</sub>	1	1.58-3	1.45-3	4.62-4	3.89-5	-5.01-4	2p <sub>3/2</sub>	1	2.51-3	1.72-3	3.62-4	-2.46-4	-1.16-4
	3	-3.86-2	-7.57-3	7.60-3	1.39-2	-2.15-2		3	-3.67-2	-6.95-3	7.34-3	1.34-2	-2.07-2
	5	-8.82-2	-1.97-2	1.56-2	3.05-2	-4.61-2		5	-8.59-2	-1.89-2	1.54-2	2.99-2	-4.53-2
	10	-2.14-1	-5.07-2	3.10-2	7.16-2	-1.03-1		10	-2.12-1	-4.99-2	3.14-2	7.10-2	-1.02-1
3s <sub>1/2</sub>	1	-1.06-2	-3.14-3	2.45-3	3.46-3	-5.91-3	3s <sub>1/2</sub>	1	-1.12-2	-3.18-3	2.63-3	3.72-3	-6.35-3
	3	-4.58-3	-3.47-3	3.71-4	5.16-4	-8.87-4		3	-5.30-3	-3.79-3	5.04-4	7.07-4	-1.21-3
	5	-9.54-3	-4.74-3	1.67-3	2.25-3	-3.92-3		5	-8.44-3	-4.64-3	1.33-3	1.78-3	-3.12-3
	10	-6.43-2	-1.85-2	1.56-2	2.14-2	-3.71-2		10	-5.94-2	-1.74-2	1.44-2	1.97-2	-3.41-2
3p <sub>1/2</sub>	1	-2.27-3	-5.39-4	-4.54-4	6.00-4	-1.46-4	3p <sub>1/2</sub>	1	-2.43-3	-6.48-4	-4.37-4	6.24-4	-1.88-4
	3	-2.98-2	-4.52-3	2.33-3	1.06-2	-1.29-2		3	-2.76-2	-4.06-3	2.02-3	9.84-3	-1.19-2
	5	-7.78-2	-1.34-2	7.17-3	2.72-2	-3.44-2		5	-7.45-2	-1.27-2	6.92-3	2.61-2	-3.30-2
	10	-2.15-1	-3.94-2	1.60-2	7.33-2	-8.93-2		10	-2.10-1	-3.84-2	1.62-2	7.18-2	-8.81-2
3p <sub>3/2</sub>	1	2.24-4	-8.84-4	5.30-4	-3.38-4	-1.92-4	3p <sub>3/2</sub>	1	1.28-4	-9.93-4	5.61-4	-3.36-4	-2.25-4
	3	-2.28-2	-5.93-3	5.70-3	7.87-3	-1.36-2		3	-2.07-2	-5.47-3	5.37-3	7.17-3	-1.25-2
	5	-6.52-2	-1.60-2	1.34-2	2.23-2	-3.57-2		5	-6.22-2	-1.53-2	1.31-2	2.14-2	-3.44-2
	10	-1.85-1	-4.49-2	2.94-2	6.21-2	-9.14-2		10	-1.81-1	-4.40-2	2.96-2	6.09-2	-9.05-2
3d <sub>3/2</sub>	1	-1.56-2	-2.29-3	-2.71-4	5.28-3	-5.01-3	3d <sub>3/2</sub>	1	-1.49-2	-2.10-3	-3.25-4	5.04-3	-4.71-3
	3	-8.96-2	-1.62-2	4.29-4	2.95-2	-2.99-2		3	-8.76-2	-1.57-2	6.17-4	2.89-2	-2.95-2
	5	-1.74-1	-3.27-2	-2.43-3	5.61-2	-5.37-2		5	-1.71-1	-3.20-2	-1.80-3	5.54-2	-5.36-2
	10	-3.91-1	-7.66-2	-1.96-2	1.22-1	-1.02-1		10	-3.87-1	-7.55-2	-1.78-2	1.21-1	-1.03-1
3d <sub>5/2</sub>	1	-1.29-2	-2.65-3	8.06-4	4.25-3	-5.05-3	3d <sub>5/2</sub>	1	-1.21-2	-2.47-3	7.69-4	4.00-3	-4.77-3
	3	-8.11-2	-1.76-2	3.73-3	2.62-2	-2.99-2		3	-7.91-2	-1.70-2	3.90-3	2.56-2	-2.95-2
	5	-1.60-1	-3.53-2	3.10-3	5.06-2	-5.37-2		5	-1.58-1	-3.46-2	3.70-3	4.99-2	-5.36-2
	10	-3.67-1	-8.29-2	-8.82-3	1.12-1	-1.03-1		10	-3.63-1	-8.17-2	-7.14-3	1.11-1	-1.04-1
4s <sub>1/2</sub>	1	-9.13-3	-2.70-3	2.12-3	3.00-3	-5.12-3	4s <sub>1/2</sub>	1	-9.44-3	-2.69-3	2.22-3	3.15-3	-5.37-3
	3	-4.53-3	-3.49-3	3.48-4	4.86-4	-8.34-4		3	-5.28-3	-3.83-3	4.80-4	6.76-4	-1.16-3
	5	-9.29-3	-4.79-3	1.56-3	2.11-3	-3.68-3		5	-8.26-3	-4.73-3	1.24-3	1.66-3	-2.90-3
	10	-6.34-2	-1.84-2	1.54-2	2.11-2	-3.64-2		10	-5.85-2	-1.73-2	1.41-2	1.93-2	-3.34-2
4p <sub>1/2</sub>	1	-2.03-3	-6.32-4	-3.28-4	4.95-4	-1.67-4	4p <sub>1/2</sub>	1	-2.26-3	-7.77-4	-2.70-4	5.39-4	-2.69-4
	3	-2.78-2	-4.34-3	2.21-3	9.83-3	-1.20-2		3	-2.57-2	-3.98-3	1.94-3	9.06-3	-1.10-2
	5	-7.52-2	-1.31-2	7.10-3	2.63-2	-3.34-2		5	-7.16-2	-1.24-2	6.82-3	2.51-2	-3.19-2
	10	-2.11-1	-3.89-2	1.60-2	7.22-2	-8.82-2		10	-2.06-1	-3.78-2	1.62-2	7.06-2	-8.68-2
4p <sub>3/2</sub>	1	1.01-4	-9.48-4	5.15-4	-3.17-4	-1.99-4	4p <sub>3/2</sub>	1	-1.29-4	-1.09-3	5.63-4	-2.72-4	-2.91-4
	3	-2.12-2	-5.71-3	5.44-3	7.27-3	-1.27-2		3	-1.92-2	-5.35-3	5.13-3	6.55-3	-1.17-2
	5	-6.29-2	-1.56-2	1.31-2	2.15-2	-3.47-2		5	-5.97-2	-1.49-2	1.28-2	2.05-2	-3.33-2
	10	-1.83-1	-4.44-2	2.93-2	6.11-2	-9.04-2		10	-1.78-1	-4.33-2	2.94-2	5.98-2	-8.92-2
<i>Z</i> = 35, Br: 4s <sub>1/2</sub> <sup>2</sup> 3d <sub>3/2</sub> <sup>3</sup> 3d <sub>5/2</sub> <sup>6</sup> 4p <sub>1/2</sub> <sup>2</sup> 4p <sub>3/2</sub> <sup>1</sup>							<i>Z</i> = 36, Kr: 4s <sub>1/2</sub> <sup>2</sup> 3d <sub>3/2</sub> <sup>3</sup> 3d <sub>5/2</sub> <sup>6</sup> 4p <sub>1/2</sub> <sup>2</sup> 4p <sub>3/2</sub> <sup>4</sup>						
2s <sub>1/2</sub>	1	-2.77-2	-8.78-3	6.25-3	8.81-3	-1.51-2	2s <sub>1/2</sub>	1	-3.03-2	-9.48-3	6.90-3	9.73-3	-1.66-2
	3	-7.40-3	-4.31-3	1.04-3	1.44-3	-2.49-3		3	-8.88-3	-4.91-3	1.33-3	1.85-3	-3.18-3
	5	-8.94-3	-4.14-3	1.71-3	2.26-3	-3.97-3		5	-8.23-3	-4.16-3	1.46-3	1.92-3	-3.38-3
	10	-6.11-2	-1.68-2	1.52-2	2.08-2	-3.60-2		10	-5.65-2	-1.57-2	1.41-2	1.91-2	-3.32-2

Table 1 (continued)

Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$	Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$
2p <sub>1/2</sub>	1	-3.13–3	2.85–3	-2.36–3	1.92–3	4.38–4	2p <sub>1/2</sub>	1	-2.48–3	3.19–3	-2.58–3	1.75–3	8.31–4
	3	-4.57–2	-4.41–3	2.09–3	1.70–2	-1.90–2		3	-4.40–2	-3.74–3	1.72–3	1.65–2	-1.82–2
	5	-9.98–2	-1.50–2	7.45–3	3.54–2	-4.29–2		5	-9.76–2	-1.42–2	7.15–3	3.48–2	-4.19–2
	10	-2.41–1	-4.30–2	1.69–2	8.26–2	-9.95–2		10	-2.38–1	-4.22–2	1.71–2	8.19–2	-9.90–2
2p <sub>3/2</sub>	1	3.52–3	2.02–3	2.71–4	-5.46–4	2.74–4	2p <sub>3/2</sub>	1	4.52–3	2.32–3	1.84–4	-8.43–4	6.59–4
	3	-3.49–2	-6.36–3	7.11–3	1.28–2	-1.99–2		3	-3.30–2	-5.74–3	6.85–3	1.23–2	-1.91–2
	5	-8.39–2	-1.82–2	1.53–2	2.93–2	-4.46–2		5	-8.16–2	-1.75–2	1.51–2	2.87–2	-4.37–2
	10	-2.10–1	-4.93–2	3.18–2	7.06–2	-1.02–1		10	-2.08–1	-4.85–2	3.22–2	7.01–2	-1.02–1
3s <sub>1/2</sub>	1	-1.17–2	-3.19–3	2.80–3	3.96–3	-6.76–3	3s <sub>1/2</sub>	1	-1.22–2	-3.17–3	2.97–3	4.20–3	-7.17–3
	3	-6.20–3	-4.14–3	6.80–4	9.58–4	-1.64–3		3	-7.25–3	-4.53–3	8.94–4	1.26–3	-2.16–3
	5	-7.60–3	-4.62–3	1.06–3	1.41–3	-2.47–3		5	-7.02–3	-4.66–3	8.47–4	1.11–3	-1.96–3
	10	-5.47–2	-1.64–2	1.32–2	1.80–2	-3.12–2		10	-5.03–2	-1.54–2	1.20–2	1.64–2	-2.84–2
3p <sub>1/2</sub>	1	-2.70–3	-7.86–4	-4.08–4	6.84–4	-2.77–4	3p <sub>1/2</sub>	1	-3.07–3	-9.46–4	-3.67–4	7.76–4	-4.09–4
	3	-2.56–2	-3.62–3	1.71–3	9.13–3	-1.08–2		3	-2.36–2	-3.22–3	1.40–3	8.44–3	-9.84–3
	5	-7.12–2	-1.19–2	6.62–3	2.50–2	-3.17–2		5	-6.79–2	-1.12–2	6.29–3	2.39–2	-3.02–2
	10	-2.05–1	-3.73–2	1.64–2	7.04–2	-8.68–2		10	-2.00–1	-3.63–2	1.65–2	6.89–2	-8.54–2
3p <sub>3/2</sub>	1	-6.72–5	-1.13–3	6.07–4	-3.04–4	-3.03–4	3p <sub>3/2</sub>	1	-3.49–4	-1.29–3	6.66–4	-2.44–4	-4.22–4
	3	-1.87–2	-5.04–3	5.04–3	6.49–3	-1.15–2		3	-1.69–2	-4.65–3	4.73–3	5.83–3	-1.06–2
	5	-5.92–2	-1.46–2	1.27–2	2.04–2	-3.31–2		5	-5.62–2	-1.39–2	1.24–2	1.94–2	-3.18–2
	10	-1.77–1	-4.30–2	2.97–2	5.97–2	-8.94–2		10	-1.73–1	-4.20–2	2.98–2	5.85–2	-8.83–2
3d <sub>3/2</sub>	1	-1.41–2	-1.90–3	-3.80–4	4.80–3	-4.42–3	3d <sub>3/2</sub>	1	-1.34–2	-1.71–3	-4.37–4	4.58–3	-4.14–3
	3	-8.55–2	-1.51–2	7.63–4	2.83–2	-2.91–2		3	-8.34–2	-1.45–2	8.70–4	2.77–2	-2.86–2
	5	-1.69–1	-3.13–2	-1.20–3	5.47–2	-5.35–2		5	-1.66–1	-3.07–2	-6.38–4	5.40–2	-5.34–2
	10	-3.83–1	-7.43–2	-1.61–2	1.20–1	-1.04–1		10	-3.79–1	-7.32–2	-1.45–2	1.19–1	-1.05–1
3d <sub>5/2</sub>	1	-1.13–2	-2.27–3	7.32–4	3.75–3	-4.48–3	3d <sub>5/2</sub>	1	-1.05–2	-2.08–3	6.97–4	3.51–3	-4.21–3
	3	-7.71–2	-1.65–2	4.04–3	2.50–2	-2.91–2		3	-7.50–2	-1.59–2	4.14–3	2.45–2	-2.86–2
	5	-1.55–1	-3.39–2	4.26–3	4.93–2	-5.35–2		5	-1.52–1	-3.32–2	4.78–3	4.86–2	-5.34–2
	10	-3.59–1	-8.05–2	-5.54–3	1.10–1	-1.05–1		10	-3.55–1	-7.94–2	-4.02–3	1.10–1	-1.06–1
4s <sub>1/2</sub>	1	-9.70–3	-2.65–3	2.32–3	3.28–3	-5.60–3	4s <sub>1/2</sub>	1	-9.83–3	-2.56–3	2.39–3	3.39–3	-5.78–3
	3	-6.16–3	-4.18–3	6.52–4	9.22–4	-1.57–3		3	-7.13–3	-4.53–3	8.56–4	1.21–3	-2.07–3
	5	-7.45–3	-4.70–3	9.73–4	1.29–3	-2.26–3		5	-6.82–3	-4.71–3	7.58–4	9.96–4	-1.75–3
	10	-5.38–2	-1.63–2	1.29–2	1.76–2	-3.04–2		10	-4.93–2	-1.54–2	1.17–2	1.59–2	-2.76–2
4p <sub>1/2</sub>	1	-2.59–3	-9.47–4	-1.99–4	6.16–4	-4.17–4	4p <sub>1/2</sub>	1	-2.97–3	-1.11–3	-1.24–4	7.17–4	-5.93–4
	3	-2.35–2	-3.60–3	1.66–3	8.30–3	-9.96–3		3	-2.14–2	-3.19–3	1.35–3	7.57–3	-8.92–3
	5	-6.80–2	-1.16–2	6.52–3	2.39–2	-3.04–2		5	-6.44–2	-1.08–2	6.15–3	2.27–2	-2.88–2
	10	-2.01–1	-3.67–2	1.63–2	6.90–2	-8.53–2		10	-1.96–1	-3.56–2	1.64–2	6.73–2	-8.38–2
4p <sub>3/2</sub>	1	-4.47–4	-1.26–3	6.27–4	-1.99–4	-4.29–4	4p <sub>3/2</sub>	1	-8.06–4	-1.42–3	6.97–4	-1.05–4	-5.91–4
	3	-1.72–2	-4.96–3	4.81–3	5.85–3	-1.07–2		3	-1.52–2	-4.55–3	4.45–3	5.15–3	-9.61–3
	5	-5.65–2	-1.42–2	1.24–2	1.94–2	-3.19–2		5	-5.32–2	-1.34–2	1.20–2	1.83–2	-3.03–2
	10	-1.74–1	-4.23–2	2.95–2	5.85–2	-8.80–2		10	-1.69–1	-4.13–2	2.95–2	5.72–2	-8.67–2
<i>Z = 37, Rb: 5s<sub>1/2</sub></i>							<i>Z = 38, Sr: 5s<sub>1/2</sub></i>						
2p <sub>1/2</sub>	1	-1.83–3	3.55–3	-2.80–3	1.59–3	1.21–3	2p <sub>3/2</sub>	1	6.41–3	2.91–3	3.93–5	-1.39–3	1.35–3
	3	-4.24–2	-3.08–3	1.34–3	1.60–2	-1.73–2		3	-2.92–2	-4.51–3	6.34–3	1.12–2	-1.75–2
	5	-9.53–2	-1.34–2	6.82–3	3.41–2	-4.10–2		5	-7.71–2	-1.60–2	1.46–2	2.74–2	-4.20–2
	10	-2.36–1	-4.13–2	1.72–2	8.11–2	-9.84–2		10	-2.03–1	-4.70–2	3.26–2	6.89–2	-1.02–1
2p <sub>3/2</sub>	1	5.52–3	2.63–3	1.06–4	-1.13–3	1.03–3	3s <sub>1/2</sub>	1	-1.29–2	-3.07–3	3.25–3	4.60–3	-7.85–3
	3	-3.11–2	-5.14–3	6.59–3	1.17–2	-1.83–2		3	-9.65–3	-5.38–3	1.40–3	1.99–3	-3.39–3
	5	-7.93–2	-1.67–2	1.49–2	2.80–2	-4.29–2		5	-6.57–3	-4.92–3	6.01–4	7.79–4	-1.38–3
	10	-2.05–1	-4.78–2	3.24–2	6.95–2	-1.02–1		10	-4.22–2	-1.37–2	9.88–3	1.34–2	-2.33–2
3s <sub>1/2</sub>	1	-1.26–2	-3.14–3	3.11–3	4.40–3	-7.51–3	3p <sub>1/2</sub>	1	-4.02–3	-1.31–3	-2.71–4	1.03–3	-7.61–4
	3	-8.42–3	-4.95–3	1.14–3	1.62–3	-2.76–3		3	-2.02–2	-2.55–3	8.41–4	7.22–3	-8.06–3
	5	-6.73–3	-4.78–3	7.06–4	9.21–4	-1.63–3		5	-6.15–2	-9.75–3	5.58–3	2.18–2	-2.74–2
	10	-4.61–2	-1.45–2	1.09–2	1.48–2	-2.58–2		10	-1.91–1	-3.42–2	1.65–2	6.59–2	-8.24–2
3p <sub>1/2</sub>	1	-3.53–3	-1.13–3	-3.21–4	8.97–4	-5.77–4	3p <sub>3/2</sub>	1	-1.11–3	-1.65–3	8.04–4	-5.74–5	-7.47–4
	3	-2.18–2	-2.86–3	1.11–3	7.81–3	-8.92–3		3	-1.35–2	-3.99–3	4.15–3	4.65–3	-8.80–3
	5	-6.46–2	-1.05–2	5.93–3	2.29–2	-2.88–2		5	-5.03–2	-1.25–2	1.16–2	1.75–2	-2.91–2
	10	-1.96–1	-3.53–2	1.65–2	6.74–2	-8.39–2		10	-1.65–1	-4.01–2	2.98–2	5.61–2	-8.59–2

(continued on next page)

Table 1 (continued)

Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$	Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$
3p <sub>3/2</sub>	1	-7.19–4	-1.47–3	7.31–4	-1.55–4	-5.76–4	3d <sub>3/2</sub>	1	-1.20–2	-1.33–3	-5.51–4	4.18–3	-3.63–3
	3	-1.51–2	-4.30–3	4.43–3	5.22–3	-9.65–3		3	-7.92–2	-1.34–2	9.82–4	2.65–2	-2.75–2
	5	-5.32–2	-1.31–2	1.20–2	1.84–2	-3.04–2		5	-1.61–1	-2.93–2	3.30–4	5.26–2	-5.30–2
	10	-1.69–1	-4.10–2	2.98–2	5.73–2	-8.71–2		10	-3.70–1	-7.10–2	-1.14–2	1.17–1	-1.06–1
3d <sub>5/2</sub>	1	-1.27–2	-1.53–3	-4.98–4	4.38–3	-3.88–3	3d <sub>5/2</sub>	1	-9.10–3	-1.70–3	6.26–4	3.08–3	-3.71–3
	3	-8.13–2	-1.40–2	9.39–4	2.71–2	-2.81–2		3	-7.08–2	-1.47–2	4.25–3	2.33–2	-2.75–2
	5	-1.64–1	-3.00–2	-1.30–4	5.34–2	-5.32–2		5	-1.47–1	-3.18–2	5.68–3	4.73–2	-5.30–2
	10	-3.75–1	-7.21–2	-1.29–2	1.18–1	-1.05–1		10	-3.47–1	-7.72–2	-1.20–3	1.08–1	-1.07–1
3d <sub>5/2</sub>	1	-9.81–3	-1.90–3	6.56–4	3.30–3	-3.95–3	4s <sub>1/2</sub>	1	-9.81–3	-2.29–3	2.47–3	3.50–3	-5.96–3
	3	-7.29–2	-1.53–2	4.20–3	2.39–2	-2.81–2		3	-9.35–3	-5.32–3	1.32–3	1.88–3	-3.20–3
	5	-1.50–1	-3.26–2	5.25–3	4.80–2	-5.33–2		5	-6.45–3	-5.00–3	5.30–4	6.88–4	-1.22–3
	10	-3.51–1	-7.83–2	-2.58–3	1.09–1	-1.06–1		10	-4.13–2	-1.37–2	9.54–3	1.29–2	-2.25–2
4s <sub>1/2</sub>	1	-9.77–3	-2.40–3	2.42–3	3.43–3	-5.86–3	4p <sub>1/2</sub>	1	-3.69–3	-1.34–3	7.96–6	9.38–4	-9.46–4
	3	-8.23–3	-4.93–3	1.08–3	1.53–3	-2.61–3		3	-1.80–2	-2.64–3	8.33–4	6.29–3	-7.13–3
	5	-6.57–3	-4.84–3	6.26–4	8.17–4	-1.44–3		5	-5.74–2	-9.35–3	5.41–3	2.03–2	-2.57–2
	10	-4.52–2	-1.45–2	1.06–2	1.44–2	-2.50–2		10	-1.85–1	-3.34–2	1.64–2	6.40–2	-8.04–2
p <sub>1/2</sub>	1	-3.27–3	-1.19–3	-7.17–5	8.16–4	-7.44–4	4p <sub>3/2</sub>	1	-1.50–3	-1.64–3	8.08–4	1.05–4	-9.14–4
	3	-1.96–2	-2.90–3	1.09–3	6.90–3	-7.98–3		3	-1.20–2	-3.98–3	3.86–3	3.97–3	-7.83–3
	5	-6.08–2	-1.01–2	5.78–3	2.14–2	-2.72–2		5	-4.69–2	-1.20–2	1.12–2	1.62–2	-2.74–2
	10	-1.90–1	-3.45–2	1.64–2	6.56–2	-8.21–2		10	-1.60–1	-3.91–2	2.94–2	5.44–2	-8.38–2
4p <sub>3/2</sub>	1	-1.10–3	-1.49–3	7.34–4	-7.99–6	-7.26–4	5s <sub>1/2</sub>	1	-9.49–3	-2.12–3	2.42–3	3.43–3	-5.85–3
	3	-1.35–2	-4.25–3	4.14–3	4.54–3	-8.68–3		3	-9.44–3	-5.36–3	1.34–3	1.90–3	-3.24–3
	5	-4.99–2	-1.27–2	1.16–2	1.72–2	-2.88–2		5	-6.49–3	-5.05–3	5.22–4	6.77–4	-1.20–3
	10	-1.65–1	-4.02–2	2.95–2	5.58–2	-8.52–2		10	-4.12–2	-1.37–2	9.51–3	1.29–2	-2.24–2
5s <sub>1/2</sub>	1	-9.59–3	-2.33–3	2.38–3	3.38–3	-5.76–3							
	3	-8.09–3	-4.80–3	1.08–3	1.53–3	-2.61–3							
	5	-6.53–3	-4.84–3	6.13–4	8.00–4	-1.41–3							
	10	-4.51–2	-1.45–2	1.06–2	1.43–2	-2.49–2							
<i>Z</i> = 39, Y: 5s <sub>1/2</sub> <sup>2</sup> 4d <sub>3/2</sub> <sup>1</sup>							<i>Z</i> = 40, Zr: 5s <sub>1/2</sub> <sup>2</sup> 4d <sub>3/2</sub> <sup>2</sup>						
3s <sub>1/2</sub>	1	-1.33–2	-2.96–3	3.38–3	4.79–3	-8.17–3	3s <sub>1/2</sub>	1	-1.35–2	-2.82–3	3.50–3	4.97–3	-8.47–3
	3	-1.10–2	-5.85–3	1.71–3	2.42–3	-4.13–3		3	-1.26–2	-6.35–3	2.04–3	2.90–3	-4.94–3
	5	-6.69–3	-5.15–3	5.62–4	7.29–4	-1.29–3		5	-7.04–3	-5.44–3	5.76–4	7.57–4	-1.33–3
	10	-3.85–2	-1.30–2	8.89–3	1.20–2	-2.09–2		10	-3.51–2	-1.23–2	7.96–3	1.07–2	-1.86–2
3p <sub>1/2</sub>	1	-4.62–3	-1.52–3	-2.08–4	1.20–3	-9.92–4	3p <sub>1/2</sub>	1	-5.34–3	-1.76–3	-1.34–4	1.40–3	-1.27–3
	3	-1.86–2	-2.27–3	5.75–4	6.66–3	-7.23–3		3	-1.72–2	-2.03–3	3.16–4	6.13–3	-6.44–3
	5	-5.84–2	-9.04–3	5.20–3	2.08–2	-2.60–2		5	-5.53–2	-8.36–3	4.79–3	1.97–2	-2.45–2
	10	-1.86–1	-3.31–2	1.64–2	6.44–2	-8.08–2		10	-1.81–1	-3.21–2	1.63–2	6.28–2	-7.91–2
3p <sub>3/2</sub>	1	-1.59–3	-1.86–3	8.92–4	6.71–5	-9.59–4	3p <sub>3/2</sub>	1	-2.18–3	-2.11–3	9.90–4	2.26–4	-1.22–3
	3	-1.20–2	-3.72–3	3.88–3	4.10–3	-7.98–3		3	-1.06–2	-3.49–3	3.62–3	3.58–3	-7.20–3
	5	-4.74–2	-1.18–2	1.12–2	1.65–2	-2.77–2		5	-4.45–2	-1.11–2	1.08–2	1.55–2	-2.63–2
	10	-1.61–1	-3.91–2	2.97–2	5.48–2	-8.45–2		10	-1.57–1	-3.81–2	2.95–2	5.35–2	-8.31–2
3d <sub>5/2</sub>	1	-1.13–2	-1.10–3	-6.07–4	3.96–3	-3.36–3	3d <sub>3/2</sub>	1	-1.06–2	-8.95–4	-6.74–4	3.76–3	-3.09–3
	3	-7.71–2	-1.28–2	1.00–3	2.59–2	-2.69–2		3	-7.51–2	-1.23–2	1.01–3	2.53–2	-2.63–2
	5	-1.58–1	-2.85–2	7.45–4	5.19–2	-5.27–2		5	-1.55–1	-2.78–2	1.11–3	5.12–2	-5.23–2
	10	-3.67–1	-7.00–2	-1.00–2	1.17–1	-1.07–1		10	-3.63–1	-6.90–2	-8.63–3	1.16–1	-1.07–1
3d <sub>5/2</sub>	1	-8.31–3	-1.48–3	5.99–4	2.85–3	-3.45–3	3d <sub>5/2</sub>	1	-7.56–3	-1.28–3	5.60–4	2.63–3	-3.19–3
	3	-6.88–2	-1.42–2	4.28–3	2.27–2	-2.70–2		3	-6.68–2	-1.37–2	4.29–3	2.21–2	-2.64–2
	5	-1.45–1	-3.11–2	6.06–3	4.67–2	-5.27–2		5	-1.42–1	-3.03–2	6.40–3	4.59–2	-5.23–2
	10	-3.44–1	-7.62–2	1.26–4	1.07–1	-1.07–1		10	-3.40–1	-7.51–2	1.40–3	1.06–1	-1.08–1
4s <sub>1/2</sub>	1	-9.83–3	-2.17–3	2.51–3	3.57–3	-6.08–3	4s <sub>1/2</sub>	1	-9.77–3	-2.01–3	2.54–3	3.61–3	-6.16–3
	3	-1.06–2	-5.75–3	1.60–3	2.27–3	-3.87–3		3	-1.20–2	-6.18–3	1.90–3	2.70–3	-4.60–3
	5	-6.61–3	-5.24–3	4.97–4	6.48–4	-1.14–3		5	-6.99–3	-5.54–3	5.16–4	6.82–4	-1.20–3
	10	-3.76–2	-1.30–2	8.56–3	1.16–2	-2.01–2		10	-3.42–2	-1.24–2	7.62–3	1.03–2	-1.79–2
4p <sub>1/2</sub>	1	-4.18–3	-1.51–3	9.74–5	1.09–3	-1.18–3	4p <sub>1/2</sub>	1	-4.74–3	-1.69–3	1.95–4	1.26–3	-1.46–3
	3	-1.64–2	-2.42–3	5.94–4	5.73–3	-6.32–3		3	-1.50–2	-2.22–3	3.57–4	5.19–3	-5.55–3
	5	-5.41–2	-8.68–3	5.02–3	1.92–2	-2.42–2		5	-5.08–2	-8.04–3	4.62–3	1.80–2	-2.27–2
	10	-1.80–1	-3.23–2	1.63–2	6.23–2	-7.86–2		10	-1.75–1	-3.12–2	1.62–2	6.06–2	-7.68–2

Table 1 (continued)

Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$	Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$
4p <sub>3/2</sub>	1	-1.96–3	-1.81–3	8.96–4	2.40–4	-1.14–3	4p <sub>3/2</sub>	1	-2.49–3	-1.99–3	9.86–4	4.00–4	-1.39–3
	3	-1.06–2	-3.76–3	3.59–3	3.44–3	-7.03–3		3	-9.24–3	-3.56–3	3.32–3	2.94–3	-6.25–3
	5	-4.39–2	-1.13–2	1.07–2	1.52–2	-2.59–2		5	-4.09–2	-1.07–2	1.03–2	1.41–2	-2.44–2
	10	-1.56–1	-3.81–2	2.92–2	5.30–2	-8.22–2		10	-1.52–1	-3.71–2	2.90–2	5.16–2	-8.06–2
4d <sub>3/2</sub>	1	-8.62–3	-1.23–3	-3.17–4	2.89–3	-2.57–3	4d <sub>3/2</sub>	1	-7.71–3	-1.05–3	-3.44–4	2.60–3	-2.25–3
	3	-7.16–2	-1.22–2	1.31–3	2.40–2	-2.53–2		3	-6.89–2	-1.16–2	1.34–3	2.32–2	-2.45–2
	5	-1.52–1	-2.75–2	1.18–3	4.99–2	-5.11–2		5	-1.48–1	-2.66–2	1.55–3	4.88–2	-5.03–2
	10	-3.60–1	-6.89–2	-9.38–3	1.15–1	-1.05–1		10	-3.55–1	-6.77–2	-7.93–3	1.13–1	-1.06–1
5s <sub>1/2</sub>	1	-9.36–3	-1.96–3	2.43–3	3.45–3	-5.87–3	5s <sub>1/2</sub>	1	-9.55–3	-1.98–3	2.48–3	3.52–3	-6.00–3
	3	-1.06–2	-5.72–3	1.60–3	2.27–3	-3.87–3		3	-1.21–2	-6.28–3	1.90–3	2.70–3	-4.60–3
	5	-6.66–3	-5.31–3	4.90–4	6.41–4	-1.13–3		5	-7.05–3	-5.61–3	5.12–4	6.78–4	-1.19–3
	10	-3.75–2	-1.30–2	8.51–3	1.15–2	-2.00–2		10	-3.41–2	-1.24–2	7.57–3	1.02–2	-1.78–2
<i>Z</i> = 41, Nb: 5s <sub>1/2</sub> <sup>1</sup> 4d <sub>3/2</sub> <sup>4</sup>							<i>Z</i> = 42, Mo: 5s <sub>1/2</sub> <sup>1</sup> 4d <sub>3/2</sub> <sup>4</sup> 4d <sub>5/2</sub> <sup>1</sup>						
3s <sub>1/2</sub>	1	-1.37–2	-2.62–3	3.62–3	5.14–3	-8.76–3	3s <sub>1/2</sub>	1	-1.37–2	-2.39–3	3.71–3	5.28–3	-8.99–3
	3	-1.42–2	-6.84–3	2.40–3	3.40–3	-5.80–3		3	-1.58–2	-7.35–3	2.77–3	3.93–3	-6.70–3
	5	-7.63–3	-5.79–3	6.46–4	8.62–4	-1.51–3		5	-8.41–3	-6.20–3	7.65–4	1.04–3	-1.80–3
	10	-3.19–2	-1.18–2	7.07–3	9.46–3	-1.65–2		10	-2.89–2	-1.13–2	6.25–3	8.31–3	-1.46–2
3p <sub>1/2</sub>	1	-6.21–3	-2.05–3	-4.63–5	1.66–3	-1.61–3	3p <sub>1/2</sub>	1	-7.06–3	-2.32–3	4.31–5	1.91–3	-1.95–3
	3	-1.58–2	-1.81–3	7.33–5	5.63–3	-5.70–3		3	-1.46–2	-1.63–3	-1.56–4	5.16–3	-5.00–3
	5	-5.23–2	-7.70–3	4.38–3	1.87–2	-2.31–2		5	-4.93–2	-7.07–3	3.96–3	1.77–2	-2.16–2
	10	-1.76–1	-3.10–2	1.61–2	6.13–2	-7.74–2		10	-1.71–1	-2.98–2	1.59–2	5.96–2	-7.55–2
3p <sub>3/2</sub>	1	-2.89–3	-2.39–3	1.11–3	4.20–4	-1.53–3	3p <sub>3/2</sub>	1	-3.61–3	-2.67–3	1.22–3	6.24–4	-1.85–3
	3	-9.29–3	-3.27–3	3.38–3	3.08–3	-6.46–3		3	-8.09–3	-3.10–3	3.15–3	2.63–3	-5.77–3
	5	-4.17–2	-1.05–2	1.04–2	1.46–2	-2.49–2		5	-3.89–2	-9.87–3	9.91–3	1.36–2	-2.35–2
	10	-1.53–1	-3.70–2	2.93–2	5.22–2	-8.16–2		10	-1.49–1	-3.60–2	2.91–2	5.09–2	-8.00–2
3d <sub>3/2</sub>	1	-9.87–3	-6.56–4	-7.42–4	3.54–3	-2.80–3	3d <sub>3/2</sub>	1	-9.11–3	-4.26–4	-8.05–4	3.31–3	-2.51–3
	3	-7.31–2	-1.18–2	9.92–4	2.47–2	-2.57–2		3	-7.11–2	-1.12–2	9.63–4	2.41–2	-2.51–2
	5	-1.52–1	-2.70–2	1.42–3	5.05–2	-5.19–2		5	-1.49–1	-2.62–2	1.68–3	4.96–2	-5.13–2
	10	-3.59–1	-6.80–2	-7.30–3	1.15–1	-1.08–1		10	-3.55–1	-6.70–2	-6.02–3	1.14–1	-1.08–1
3d <sub>5/2</sub>	1	-6.73–3	-1.04–3	5.27–4	2.38–3	-2.91–3	3d <sub>5/2</sub>	1	-5.92–3	-8.15–4	4.93–4	2.14–3	-2.63–3
	3	-6.48–2	-1.31–2	4.30–3	2.15–2	-2.58–2		3	-6.28–2	-1.26–2	4.28–3	2.09–2	-2.52–2
	5	-1.39–1	-2.95–2	6.70–3	4.52–2	-5.19–2		5	-1.36–1	-2.87–2	6.94–3	4.44–2	-5.14–2
	10	-3.36–1	-7.41–2	2.63–3	1.05–1	-1.08–1		10	-3.32–1	-7.31–2	3.80–3	1.04–1	-1.08–1
4s <sub>1/2</sub>	1	-9.65–3	-1.81–3	2.56–3	3.65–3	-6.21–3	4s <sub>1/2</sub>	1	-9.44–3	-1.58–3	2.57–3	3.66–3	-6.22–3
	3	-1.33–2	-6.58–3	2.21–3	3.14–3	-5.36–3		3	-1.47–2	-6.98–3	2.53–3	3.60–3	-6.14–3
	5	-7.59–3	-5.91–3	5.86–4	7.88–4	-1.37–3		5	-8.36–3	-6.31–3	7.02–4	9.59–4	-1.66–3
	10	-3.10–2	-1.18–2	6.74–3	9.02–3	-1.58–2		10	-2.81–2	-1.13–2	5.93–3	7.88–3	-1.38–2
4p <sub>1/2</sub>	1	-5.39–3	-1.89–3	3.06–4	1.46–3	-1.77–3	4p <sub>1/2</sub>	1	-6.00–3	-2.05–3	4.11–4	1.66–3	-2.07–3
	3	-1.37–2	-2.05–3	1.35–4	4.68–3	-4.82–3		3	-1.25–2	-1.91–3	-7.22–5	4.22–3	-4.15–3
	5	-4.77–2	-7.45–3	4.22–3	1.70–2	-2.12–2		5	-4.47–2	-6.90–3	3.83–3	1.59–2	-1.97–2
	10	-1.69–1	-3.00–2	1.60–2	5.88–2	-7.48–2		10	-1.64–1	-2.89–2	1.57–2	5.71–2	-7.28–2
4p <sub>3/2</sub>	1	-3.11–3	-2.19–3	1.09–3	5.86–4	-1.68–3	4p <sub>3/2</sub>	1	-3.69–3	-2.36–3	1.19–3	7.69–4	-1.96–3
	3	-7.99–3	-3.38–3	3.07–3	2.46–3	-5.52–3		3	-6.87–3	-3.23–3	2.82–3	2.02–3	-4.84–3
	5	-3.81–2	-1.01–2	9.80–3	1.32–2	-2.29–2		5	-3.53–2	-9.54–3	9.34–3	1.22–2	-2.15–2
	10	-1.47–1	-3.60–2	2.88–2	5.01–2	-7.89–2		10	-1.42–1	-3.49–2	2.85–2	4.86–2	-7.71–2
4d <sub>3/2</sub>	1	-6.91–3	-9.42–4	-3.39–4	2.32–3	-1.98–3	4d <sub>3/2</sub>	1	-6.12–3	-8.00–4	-3.56–4	2.06–3	-1.70–3
	3	-6.61–2	-1.10–2	1.35–3	2.23–2	-2.37–2		3	-6.36–2	-1.04–2	1.37–3	2.15–2	-2.29–2
	5	-1.44–1	-2.57–2	1.88–3	4.76–2	-4.95–2		5	-1.40–1	-2.48–2	2.15–3	4.65–2	-4.87–2
	10	-3.50–1	-6.66–2	-6.52–3	1.12–1	-1.06–1		10	-3.46–1	-6.54–2	-5.13–3	1.11–1	-1.06–1
5s <sub>1/2</sub>	1	-8.94–3	-1.48–3	2.44–3	3.47–3	-5.91–3	4d <sub>5/2</sub>	1	-3.52–3	-1.14–3	7.09–4	1.09–3	-1.80–3
	3	-1.36–2	-6.78–3	2.24–3	3.19–3	-5.43–3		3	-5.57–2	-1.17–2	4.54–3	1.85–2	-2.30–2
	5	-7.75–3	-6.01–3	6.05–4	8.16–4	-1.42–3		5	-1.27–1	-2.72–2	7.29–3	4.15–2	-4.87–2
	10	-3.09–2	-1.18–2	6.69–3	8.95–3	-1.56–2		10	-3.23–1	-7.14–2	4.59–3	1.02–1	-1.06–1
							5s <sub>1/2</sub>	1	-8.71–3	-1.29–3	2.42–3	3.45–3	-5.87–3
								3	-1.47–2	-6.91–3	2.54–3	3.61–3	-6.16–3
								5	-8.57–3	-6.45–3	7.25–4	9.94–4	-1.72–3
								10	-2.79–2	-1.13–2	5.87–3	7.81–3	-1.37–2

(continued on next page)

Table 1 (continued)

Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$	Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$
<i>Z</i> = 43, Tc: $5s_{1/2}^2 4d_{3/2}^4 4d_{5/2}^1$													
3s <sub>1/2</sub>	1	-1.37-2	-2.15-3	3.79-3	5.39-3	-9.18-3	3s <sub>1/2</sub>	1	-1.37-2	-1.81-3	3.87-3	5.52-3	-9.38-3
	3	-1.75-2	-7.84-3	3.16-3	4.48-3	-7.64-3		3	-1.93-2	-8.35-3	3.57-3	5.08-3	-8.65-3
	5	-9.37-3	-6.64-3	9.30-4	1.28-3	-2.21-3		5	-1.06-2	-7.16-3	1.15-3	1.59-3	-2.74-3
	10	-2.62-2	-1.08-2	5.50-3	7.26-3	-1.28-2		10	-2.38-2	-1.05-2	4.80-3	6.28-3	-1.11-2
3p <sub>1/2</sub>	1	-7.91-3	-2.58-3	1.29-4	2.16-3	-2.29-3	3p <sub>1/2</sub>	1	-9.02-3	-2.91-3	2.37-4	2.49-3	-2.73-3
	3	-1.35-2	-1.49-3	-3.68-4	4.74-3	-4.37-3		3	-1.25-2	-1.37-3	-5.74-4	4.35-3	-3.77-3
	5	-4.64-2	-6.48-3	3.54-3	1.67-2	-2.02-2		5	-4.37-2	-5.92-3	3.13-3	1.57-2	-1.88-2
	10	-1.66-1	-2.87-2	1.56-2	5.80-2	-7.36-2		10	-1.61-1	-2.76-2	1.53-2	5.64-2	-7.17-2
3p <sub>3/2</sub>	1	-4.33-3	-2.93-3	1.33-3	8.27-4	-2.16-3	3p <sub>3/2</sub>	1	-5.25-3	-3.26-3	1.47-3	1.09-3	-2.57-3
	3	-7.02-3	-2.96-3	2.93-3	2.21-3	-5.14-3		3	-5.99-3	-2.84-3	2.73-3	1.81-3	-4.54-3
	5	-3.63-2	-9.31-3	9.47-3	1.27-2	-2.22-2		5	-3.37-2	-8.77-3	9.04-3	1.18-2	-2.08-2
	10	-1.44-1	-3.50-2	2.88-2	4.95-2	-7.83-2		10	-1.40-1	-3.39-2	2.84-2	4.81-2	-7.66-2
3d <sub>3/2</sub>	1	-8.41-3	-2.08-4	-8.64-4	3.11-3	-2.25-3	3d <sub>3/2</sub>	1	-7.58-3	5.59-5	-9.30-4	2.87-3	-1.94-3
	3	-6.92-2	-1.07-2	9.27-4	2.36-2	-2.45-2		3	-6.72-2	-1.02-2	8.66-4	2.30-2	-2.39-2
	5	-1.46-1	-2.54-2	1.89-3	4.88-2	-5.07-2		5	-1.44-1	-2.46-2	2.08-3	4.80-2	-5.01-2
	10	-3.51-1	-6.60-2	-4.79-3	1.13-1	-1.08-1		10	-3.47-1	-6.50-2	-3.60-3	1.12-1	-1.09-1
3d <sub>5/2</sub>	1	-5.14-3	-5.98-4	4.62-4	1.91-3	-2.37-3	3d <sub>5/2</sub>	1	-4.22-3	-3.38-4	4.35-4	1.64-3	-2.08-3
	3	-6.08-2	-1.20-2	4.26-3	2.04-2	-2.46-2		3	-5.89-2	-1.15-2	4.23-3	1.98-2	-2.40-2
	5	-1.33-1	-2.79-2	7.13-3	4.36-2	-5.07-2		5	-1.30-1	-2.71-2	7.31-3	4.28-2	-5.01-2
	10	-3.29-1	-7.21-2	4.92-3	1.04-1	-1.09-1		10	-3.25-1	-7.11-2	6.01-3	1.03-1	-1.09-1
4s <sub>1/2</sub>	1	-9.17-3	-1.34-3	2.55-3	3.64-3	-6.19-3	4s <sub>1/2</sub>	1	-8.83-3	-1.02-3	2.54-3	3.63-3	-6.17-3
	3	-1.61-2	-7.35-3	2.86-3	4.06-3	-6.92-3		3	-1.75-2	-7.72-3	3.20-3	4.55-3	-7.75-3
	5	-9.29-3	-6.75-3	8.60-4	1.19-3	-2.05-3		5	-1.04-2	-7.24-3	1.07-3	1.49-3	-2.56-3
	10	-2.54-2	-1.09-2	5.18-3	6.84-3	-1.20-2		10	-2.30-2	-1.06-2	4.49-3	5.88-3	-1.04-2
4p <sub>1/2</sub>	1	-6.57-3	-2.20-3	5.09-4	1.85-3	-2.36-3	4p <sub>1/2</sub>	1	-7.25-3	-2.35-3	6.23-4	2.08-3	-2.71-3
	3	-1.14-2	-1.81-3	-2.63-4	3.80-3	-3.54-3		3	-1.05-2	-1.74-3	-4.39-4	3.42-3	-2.98-3
	5	-4.19-2	-6.39-3	3.44-3	1.49-2	-1.83-2		5	-3.91-2	-5.90-3	3.05-3	1.39-2	-1.69-2
	10	-1.58-1	-2.77-2	1.54-2	5.53-2	-7.07-2		10	-1.53-1	-2.65-2	1.50-2	5.34-2	-6.85-2
4p <sub>3/2</sub>	1	-4.22-3	-2.51-3	1.28-3	9.42-4	-2.22-3	4p <sub>3/2</sub>	1	-4.88-3	-2.68-3	1.39-3	1.16-3	-2.55-3
	3	-5.89-3	-3.11-3	2.60-3	1.63-3	-4.23-3		3	-4.99-3	-3.03-3	2.39-3	1.26-3	-3.65-3
	5	-3.28-2	-9.04-3	8.90-3	1.13-2	-2.02-2		5	-3.02-2	-8.56-3	8.45-3	1.04-2	-1.88-2
	10	-1.38-1	-3.38-2	2.81-2	4.71-2	-7.52-2		10	-1.33-1	-3.27-2	2.77-2	4.56-2	-7.33-2
4d <sub>3/2</sub>	1	-5.39-3	-6.82-4	-3.65-4	1.81-3	-1.45-3	4d <sub>3/2</sub>	1	-4.60-3	-5.32-4	-3.88-4	1.55-3	-1.16-3
	3	-6.08-2	-9.80-3	1.35-3	2.07-2	-2.20-2		3	-5.81-2	-9.19-3	1.30-3	1.98-2	-2.11-2
	5	-1.36-1	-2.40-2	2.41-3	4.54-2	-4.78-2		5	-1.33-1	-2.31-2	2.64-3	4.43-2	-4.69-2
	10	-3.41-1	-6.42-2	-3.81-3	1.10-1	-1.06-1		10	-3.36-1	-6.30-2	-2.56-3	1.08-1	-1.06-1
4d <sub>5/2</sub>	1	-2.83-3	-1.02-3	6.89-4	8.61-4	-1.55-3	4d <sub>5/2</sub>	1	-2.03-3	-8.65-4	6.65-4	6.01-4	-1.27-3
	3	-5.30-2	-1.11-2	4.51-3	1.77-2	-2.22-2		3	-5.04-2	-1.04-2	4.46-3	1.69-2	-2.13-2
	5	-1.24-1	-2.64-2	7.51-3	4.04-2	-4.79-2		5	-1.20-1	-2.55-2	7.71-3	3.93-2	-4.70-2
	10	-3.19-1	-7.02-2	5.78-3	1.00-1	-1.06-1		10	-3.14-1	-6.90-2	6.91-3	9.93-2	-1.06-1
5s <sub>1/2</sub>	1	-8.54-3	-1.11-3	2.42-3	3.46-3	-5.88-3	5s <sub>1/2</sub>	1	-8.60-3	-1.10-3	2.44-3	3.49-3	-5.93-3
	3	-1.62-2	-7.49-3	2.86-3	4.06-3	-6.92-3		3	-1.77-2	-7.89-3	3.20-3	4.56-3	-7.76-3
	5	-9.46-3	-6.83-3	8.85-4	1.23-3	-2.11-3		5	-1.07-2	-7.42-3	1.09-3	1.53-3	-2.62-3
	10	-2.53-2	-1.09-2	5.12-3	6.77-3	-1.19-2		10	-2.29-2	-1.06-2	4.43-3	5.81-3	-1.02-2
<i>Z</i> = 45, Rh: $5s_{1/2}^1 4d_{3/2}^4 4d_{5/2}^4$													
3s <sub>1/2</sub>	1	-1.35-2	-1.47-3	3.93-3	5.61-3	-9.54-3	3s <sub>1/2</sub>	1	-1.33-2	-1.05-3	3.98-3	5.70-3	-9.68-3
	3	-2.10-2	-8.84-3	3.99-3	5.68-3	-9.67-3		3	-2.29-2	-9.32-3	4.43-3	6.30-3	-1.07-2
	5	-1.19-2	-7.71-3	1.41-3	1.96-3	-3.37-3		5	-1.35-2	-8.34-3	1.73-3	2.43-3	-4.16-3
	10	-2.16-2	-1.02-2	4.17-3	5.40-3	-9.57-3		10	-1.98-2	-1.00-2	3.60-3	4.61-3	-8.21-3
3p <sub>1/2</sub>	1	-1.01-2	-3.23-3	3.40-4	2.82-3	-3.16-3	3p <sub>1/2</sub>	1	-1.13-2	-3.57-3	4.52-4	3.20-3	-3.65-3
	3	-1.17-2	-1.30-3	-7.62-4	3.99-3	-3.23-3		3	-1.09-2	-1.25-3	-9.38-4	3.68-3	-2.74-3
	5	-4.10-2	-5.41-3	2.72-3	1.48-2	-1.75-2		5	-3.86-2	-4.96-3	2.30-3	1.39-2	-1.62-2
	10	-1.56-1	-2.64-2	1.49-2	5.47-2	-6.96-2		10	-1.51-1	-2.52-2	1.45-2	5.30-2	-6.75-2
3p <sub>3/2</sub>	1	-6.17-3	-3.59-3	1.61-3	1.36-3	-2.96-3	3p <sub>3/2</sub>	1	-7.19-3	-3.94-3	1.76-3	1.65-3	-3.41-3
	3	-5.09-3	-2.76-3	2.55-3	1.44-3	-3.99-3		3	-4.28-3	-2.71-3	2.38-3	1.11-3	-3.48-3
	5	-3.13-2	-8.28-3	8.61-3	1.09-2	-1.95-2		5	-2.90-2	-7.86-3	8.17-3	1.01-2	-1.83-2
	10	-1.36-1	-3.28-2	2.80-2	4.67-2	-7.47-2		10	-1.31-1	-3.18-2	2.76-2	4.53-2	-7.29-2

Table 1 (continued)

Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$	Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$
3d <sub>3/2</sub>	1	-6.82–3	2.90–4	-9.92–4	2.65–3	-1.66–3	3d <sub>3/2</sub>	1	-6.10–3	5.09–4	-1.06–3	2.43–3	-1.38–3
	3	-6.53–2	-9.64–3	7.96–4	2.24–2	-2.32–2		3	-6.33–2	-9.08–3	7.11–4	2.18–2	-2.26–2
	5	-1.41–1	-2.38–2	2.22–3	4.72–2	-4.94–2		5	-1.38–1	-2.31–2	2.36–3	4.64–2	-4.87–2
	10	-3.43–1	-6.40–2	-2.47–3	1.11–1	-1.09–1		10	-3.39–1	-6.30–2	-1.40–3	1.10–1	-1.09–1
3d <sub>5/2</sub>	1	-3.38–3	-1.08–4	4.07–4	1.39–3	-1.80–3	3d <sub>5/2</sub>	1	-2.57–3	1.06–4	3.84–4	1.15–3	-1.53–3
	3	-5.69–2	-1.10–2	4.19–3	1.92–2	-2.34–2		3	-5.50–2	-1.04–2	4.14–3	1.86–2	-2.28–2
	5	-1.28–1	-2.63–2	7.45–3	4.20–2	-4.95–2		5	-1.25–1	-2.55–2	7.60–3	4.12–2	-4.88–2
	10	-3.21–1	-7.01–2	7.04–3	1.02–1	-1.09–1		10	-3.18–1	-6.90–2	8.01–3	1.01–1	-1.09–1
4s <sub>1/2</sub>	1	-8.41–3	-6.97–4	2.51–3	3.59–3	-6.09–3	4s <sub>1/2</sub>	1	-7.91–3	-3.06–4	2.46–3	3.54–3	-6.00–3
	3	-1.89–2	-8.06–3	3.54–3	5.03–3	-8.57–3		3	-2.03–2	-8.39–3	3.88–3	5.52–3	-9.40–3
	5	-1.17–2	-7.74–3	1.31–3	1.84–3	-3.15–3		5	-1.32–2	-8.30–3	1.61–3	2.27–3	-3.89–3
	10	-2.09–2	-1.03–2	3.87–3	5.03–3	-8.90–3		10	-1.91–2	-1.01–2	3.32–3	4.26–3	-7.58–3
4p <sub>1/2</sub>	1	-7.90–3	-2.49–3	7.28–4	2.31–3	-3.04–3	4p <sub>1/2</sub>	1	-8.58–3	-2.61–3	8.40–4	2.55–3	-3.39–3
	3	-9.73–3	-1.71–3	-5.88–4	3.09–3	-2.50–3		3	-9.09–3	-1.73–3	-7.18–4	2.80–3	-2.08–3
	5	-3.65–2	-5.45–3	2.66–3	1.29–2	-1.56–2		5	-3.40–2	-5.05–3	2.25–3	1.20–2	-1.43–2
	10	-1.47–1	-2.53–2	1.46–2	5.16–2	-6.62–2		10	-1.41–1	-2.41–2	1.42–2	4.98–2	-6.39–2
4p <sub>3/2</sub>	1	-5.48–3	-2.83–3	1.49–3	1.36–3	-2.85–3	4p <sub>3/2</sub>	1	-6.13–3	-2.97–3	1.60–3	1.58–3	-3.18–3
	3	-4.25–3	-2.99–3	2.21–3	9.46–4	-3.16–3		3	-3.62–3	-2.99–3	2.05–3	6.63–4	-2.72–3
	5	-2.78–2	-8.11–3	8.01–3	9.49–3	-1.75–2		5	-2.56–2	-7.73–3	7.54–3	8.66–3	-1.62–2
	10	-1.28–1	-3.15–2	2.72–2	4.40–2	-7.12–2		10	-1.23–1	-3.04–2	2.67–2	4.25–2	-6.91–2
4d <sub>3/2</sub>	1	-3.97–3	-4.44–4	-3.92–4	1.33–3	-9.40–4	4d <sub>3/2</sub>	1	-3.46–3	-4.19–4	-3.72–4	1.14–3	-7.68–4
	3	-5.54–2	-8.60–3	1.25–3	1.90–2	-2.02–2		3	-5.27–2	-8.00–3	1.16–3	1.81–2	-1.93–2
	5	-1.29–1	-2.23–2	2.84–3	4.32–2	-4.61–2		5	-1.25–1	-2.15–2	3.02–3	4.21–2	-4.52–2
	10	-3.30–1	-6.18–2	-1.40–3	1.07–1	-1.06–1		10	-3.25–1	-6.04–2	-3.06–4	1.06–1	-1.05–1
4d <sub>5/2</sub>	1	-1.41–3	-7.73–4	6.56–4	3.86–4	-1.04–3	4d <sub>5/2</sub>	1	-8.90–4	-7.44–4	6.76–4	1.94–4	-8.69–4
	3	-4.78–2	-9.83–3	4.41–3	1.61–2	-2.05–2		3	-4.51–2	-9.21–3	4.32–3	1.52–2	-1.95–2
	5	-1.16–1	-2.47–2	7.89–3	3.83–2	-4.62–2		5	-1.13–1	-2.38–2	8.05–3	3.73–2	-4.53–2
	10	-3.09–1	-6.77–2	7.97–3	9.80–2	-1.06–1		10	-3.04–1	-6.63–2	8.95–3	9.67–2	-1.06–1
5s <sub>1/2</sub>	1	-8.18–3	-7.83–4	2.40–3	3.44–3	-5.84–3							
	3	-1.90–2	-8.18–3	3.55–3	5.06–3	-8.61–3							
	5	-1.19–2	-7.86–3	1.34–3	1.88–3	-3.22–3							
	10	-2.08–2	-1.03–2	3.82–3	4.95–3	-8.77–3							
<i>Z</i> = 47, Ag: 5s <sub>1/2</sub> <sup>1</sup> 4d <sub>3/2</sub> <sup>4</sup> 4d <sub>5/2</sub> <sup>6</sup>							<i>Z</i> = 48, Cd: 5s <sub>1/2</sub> <sup>2</sup> 4d <sub>3/2</sub> <sup>4</sup> 4d <sub>5/2</sub> <sup>6</sup>						
3s <sub>1/2</sub>	1	-1.31–2	-6.67–4	4.03–3	5.78–3	-9.81–3	3s <sub>1/2</sub>	1	-1.29–2	-2.74–4	4.09–3	5.87–3	-9.95–3
	3	-2.46–2	-9.77–3	4.87–3	6.92–3	-1.18–2		3	-2.64–2	-1.02–2	5.31–3	7.55–3	-1.29–2
	5	-1.51–2	-8.91–3	2.05–3	2.89–3	-4.94–3		5	-1.69–2	-9.56–3	2.42–3	3.42–3	-5.85–3
	10	-1.82–2	-9.91–3	3.11–3	3.93–3	-7.04–3		10	-1.69–2	-9.89–3	2.69–3	3.35–3	-6.04–3
3p <sub>1/2</sub>	1	-1.25–2	-3.91–3	5.49–4	3.56–3	-4.11–3	3p <sub>1/2</sub>	1	-1.38–2	-4.25–3	6.42–4	3.94–3	-4.58–3
	3	-1.03–2	-1.24–3	-1.09–3	3.41–3	-2.32–3		3	-9.88–3	-1.27–3	-1.23–3	3.20–3	-1.96–3
	5	-3.62–2	-4.48–3	1.93–3	1.31–2	-1.50–2		5	-3.40–2	-4.08–3	1.55–3	1.23–2	-1.38–2
	10	-1.45–1	-2.41–2	1.40–2	5.14–2	-6.54–2		10	-1.40–1	-2.29–2	1.35–2	4.97–2	-6.32–2
3p <sub>3/2</sub>	1	-8.20–3	-4.28–3	1.89–3	1.94–3	-3.83–3	3p <sub>3/2</sub>	1	-9.22–3	-4.63–3	2.02–3	2.24–3	-4.26–3
	3	-3.63–3	-2.69–3	2.23–3	8.22–4	-3.05–3		3	-3.09–3	-2.71–3	2.11–3	5.74–4	-2.68–3
	5	-2.67–2	-7.40–3	7.78–3	9.28–3	-1.71–2		5	-2.47–2	-7.02–3	7.40–3	8.53–3	-1.59–2
	10	-1.27–1	-3.07–2	2.71–2	4.38–2	-7.10–2		10	-1.22–1	-2.97–2	2.66–2	4.24–2	-6.90–2
3d <sub>3/2</sub>	1	-5.34–3	7.56–4	-1.11–3	2.21–3	-1.10–3	3d <sub>3/2</sub>	1	-4.70–3	9.67–4	-1.17–3	2.03–3	-8.63–4
	3	-6.15–2	-8.55–3	6.15–4	2.13–2	-2.19–2		3	-5.97–2	-8.02–3	5.07–4	2.08–2	-2.13–2
	5	-1.35–1	-2.23–2	2.43–3	4.56–2	-4.80–2		5	-1.32–1	-2.16–2	2.51–3	4.48–2	-4.73–2
	10	-3.35–1	-6.19–2	-4.04–4	1.09–1	-1.09–1		10	-3.32–1	-6.08–2	5.24–4	1.08–1	-1.09–1
3d <sub>5/2</sub>	1	-1.71–3	3.49–4	3.66–4	8.99–4	-1.26–3	3d <sub>5/2</sub>	1	-9.70–4	5.54–4	3.51–4	6.80–4	-1.03–3
	3	-5.31–2	-9.88–3	4.08–3	1.81–2	-2.22–2		3	-5.12–2	-9.35–3	4.01–3	1.76–2	-2.16–2
	5	-1.22–1	-2.48–2	7.67–3	4.04–2	-4.81–2		5	-1.19–1	-2.41–2	7.76–3	3.97–2	-4.75–2
	10	-3.14–1	-6.79–2	8.91–3	1.00–1	-1.09–1		10	-3.10–1	-6.68–2	9.75–3	9.92–2	-1.09–1
4s <sub>1/2</sub>	1	-7.42–3	4.89–5	2.41–3	3.47–3	-5.88–3	4s <sub>1/2</sub>	1	-6.94–3	4.10–4	2.37–3	3.42–3	-5.78–3
	3	-2.16–2	-8.69–3	4.21–3	5.99–3	-1.02–2		3	-2.29–2	-8.98–3	4.53–3	6.46–3	-1.10–2
	5	-1.46–2	-8.79–3	1.90–3	2.69–3	-4.59–3		5	-1.61–2	-9.32–3	2.24–3	3.17–3	-5.41–3
	10	-1.77–2	-1.01–2	2.85–3	3.61–3	-6.46–3		10	-1.65–2	-1.01–2	2.45–3	3.06–3	-5.51–3

(continued on next page)

Table 1 (continued)

Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$	Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$
4p <sub>1/2</sub>	1	-9.13-3	-2.69-3	9.24-4	2.76-3	-3.68-3	4p <sub>1/2</sub>	1	-9.68-3	-2.76-3	1.00-3	2.97-3	-3.97-3
	3	-8.62-3	-1.79-3	-8.15-4	2.57-3	-1.76-3		3	-8.30-3	-1.88-3	-8.93-4	2.39-3	-1.50-3
	5	-3.16-2	-4.62-3	1.89-3	1.12-2	-1.30-2		5	-2.93-2	-4.27-3	1.52-3	1.03-2	-1.18-2
	10	-1.36-1	-2.30-2	1.37-2	4.79-2	-6.16-2		10	-1.31-1	-2.19-2	1.32-2	4.62-2	-5.94-2
4p <sub>3/2</sub>	1	-6.67-3	-3.08-3	1.67-3	1.77-3	-3.45-3	4p <sub>3/2</sub>	1	-7.18-3	-3.17-3	1.75-3	1.95-3	-3.71-3
	3	-3.17-3	-3.04-3	1.93-3	4.41-4	-2.37-3		3	-2.84-3	-3.11-3	1.83-3	2.58-4	-2.09-3
	5	-2.33-2	-7.29-3	7.13-3	7.85-3	-1.50-2		5	-2.13-2	-6.94-3	6.70-3	7.09-3	-1.38-2
	10	-1.19-1	-2.94-2	2.61-2	4.09-2	-6.70-2		10	-1.14-1	-2.83-2	2.55-2	3.94-2	-6.49-2
4d <sub>3/2</sub>	1	-2.88-3	-3.25-4	-3.81-4	9.46-4	-5.64-4	4d <sub>3/2</sub>	1	-2.43-3	-2.77-4	-3.78-4	7.85-4	-4.07-4
	3	-5.04-2	-7.55-3	1.10-3	1.74-2	-1.85-2		3	-4.78-2	-6.99-3	9.98-4	1.65-2	-1.75-2
	5	-1.22-1	-2.07-2	3.18-3	4.11-2	-4.42-2		5	-1.18-1	-1.98-2	3.29-3	3.99-2	-4.32-2
	10	-3.20-1	-5.91-2	6.82-4	1.04-1	-1.05-1		10	-3.14-1	-5.77-2	1.60-3	1.03-1	-1.04-1
4d <sub>5/2</sub>	1	-3.24-4	-6.45-4	6.57-4	3.31-6	-6.60-4	4d <sub>5/2</sub>	1	1.30-4	-5.89-4	6.54-4	-1.57-4	-4.98-4
	3	-4.28-2	-8.75-3	4.27-3	1.45-2	-1.88-2		3	-4.03-2	-8.17-3	4.17-3	1.37-2	-1.79-2
	5	-1.09-1	-2.30-2	8.19-3	3.62-2	-4.44-2		5	-1.06-1	-2.21-2	8.28-3	3.52-2	-4.35-2
	10	-2.98-1	-6.49-2	9.84-3	9.53-2	-1.05-1		10	-2.93-1	-6.36-2	1.06-2	9.39-2	-1.05-1
5s <sub>1/2</sub>	1	-6.63-3	2.51-4	2.22-3	3.19-3	-5.41-3	5s <sub>1/2</sub>	1	-6.42-3	3.77-4	2.19-3	3.16-3	-5.34-3
	3	-2.11-2	-8.41-3	4.14-3	5.89-3	-1.00-2		3	-2.28-2	-9.04-3	4.51-3	6.43-3	-1.09-2
	5	-1.46-2	-8.82-3	1.92-3	2.71-3	-4.63-3		5	-1.63-2	-9.41-3	2.26-3	3.21-3	-5.47-3
	10	-1.76-2	-1.01-2	2.80-3	3.55-3	-6.35-3		10	-1.65-2	-1.02-2	2.40-3	3.00-3	-5.40-3
$Z = 49$ , In: $5s_{1/2}^2 4d_{3/2}^4 4d_{5/2}^6 5p_{1/2}^1$							$Z = 50$ , Sn: $5s_{1/2}^2 4d_{3/2}^4 4d_{5/2}^6 5p_{1/2}^2$						
3s <sub>1/2</sub>	1	-1.27-2	1.18-4	4.15-3	5.96-3	-1.01-2	3s <sub>1/2</sub>	1	-1.25-2	5.34-4	4.21-3	6.06-3	-1.03-2
	3	-2.82-2	-1.06-2	5.75-3	8.19-3	-1.39-2		3	-3.00-2	-1.10-2	6.20-3	8.83-3	-1.50-2
	5	-1.88-2	-1.02-2	2.83-3	4.00-3	-6.83-3		5	-2.09-2	-1.09-2	3.27-3	4.63-3	-7.90-3
	10	-1.60-2	-9.96-3	2.34-3	2.87-3	-5.20-3		10	-1.53-2	-1.01-2	2.05-3	2.48-3	-4.53-3
3p <sub>1/2</sub>	1	-1.50-2	-4.60-3	7.31-4	4.32-3	-5.06-3	3p <sub>1/2</sub>	1	-1.64-2	-4.95-3	8.16-4	4.73-3	-5.54-3
	3	-9.57-3	-1.33-3	-1.36-3	3.02-3	-1.67-3		3	-9.38-3	-1.43-3	-1.46-3	2.89-3	-1.42-3
	5	-3.19-2	-3.72-3	1.18-3	1.15-2	-1.27-2		5	-3.00-2	-3.39-3	8.25-4	1.08-2	-1.16-2
	10	-1.36-1	-2.18-2	1.30-2	4.81-2	-6.11-2		10	-1.31-1	-2.08-2	1.25-2	4.65-2	-5.90-2
3p <sub>3/2</sub>	1	-1.03-2	-4.99-3	2.15-3	2.54-3	-4.69-3	3p <sub>3/2</sub>	1	-1.13-2	-5.36-3	2.29-3	2.85-3	-5.13-3
	3	-2.67-3	-2.77-3	2.00-3	3.63-4	-2.37-3		3	-2.36-3	-2.85-3	1.92-3	1.85-4	-2.10-3
	5	-2.27-2	-6.67-3	7.03-3	7.82-3	-1.49-2		5	-2.09-2	-6.36-3	6.67-3	7.14-3	-1.38-2
	10	-1.18-1	-2.86-2	2.61-2	4.10-2	-6.71-2		10	-1.14-1	-2.77-2	2.55-2	3.96-2	-6.51-2
3d <sub>3/2</sub>	1	-3.98-3	1.22-3	-1.22-3	1.84-3	-6.13-4	3d <sub>3/2</sub>	1	-3.38-3	1.43-3	-1.28-3	1.67-3	-3.91-4
	3	-5.80-2	-7.50-3	3.90-4	2.03-2	-2.07-2		3	-5.63-2	-6.96-3	2.70-4	1.98-2	-2.01-2
	5	-1.30-1	-2.09-2	2.56-3	4.41-2	-4.67-2		5	-1.28-1	-2.02-2	2.59-3	4.35-2	-4.61-2
	10	-3.28-1	-5.97-2	1.38-3	1.07-1	-1.09-1		10	-3.24-1	-5.86-2	2.17-3	1.06-1	-1.09-1
3d <sub>5/2</sub>	1	-1.38-4	7.98-4	3.46-4	4.44-4	-7.89-4	3d <sub>5/2</sub>	1	5.88-4	1.00-3	3.41-4	2.34-4	-5.75-4
	3	-4.95-2	-8.84-3	3.94-3	1.71-2	-2.10-2		3	-4.77-2	-8.29-3	3.88-3	1.65-2	-2.04-2
	5	-1.17-1	-2.34-2	7.84-3	3.90-2	-4.69-2		5	-1.15-1	-2.27-2	7.90-3	3.83-2	-4.63-2
	10	-3.06-1	-6.57-2	1.05-2	9.83-2	-1.09-1		10	-3.02-1	-6.46-2	1.12-2	9.74-2	-1.09-1
4s <sub>1/2</sub>	1	-6.50-3	7.63-4	2.33-3	3.37-3	-5.70-3	4s <sub>1/2</sub>	1	-6.04-3	1.13-3	2.29-3	3.32-3	-5.62-3
	3	-2.42-2	-9.26-3	4.86-3	6.93-3	-1.18-2		3	-2.54-2	-9.51-3	5.18-3	7.39-3	-1.26-2
	5	-1.78-2	-9.87-3	2.60-3	3.69-3	-6.29-3		5	-1.95-2	-1.04-2	2.98-3	4.24-3	-7.22-3
	10	-1.57-2	-1.02-2	2.12-3	2.60-3	-4.72-3		10	-1.51-2	-1.04-2	1.85-3	2.24-3	-4.09-3
4p <sub>1/2</sub>	1	-1.02-2	-2.82-3	1.08-3	3.17-3	-4.25-3	4p <sub>1/2</sub>	1	-1.07-2	-2.85-3	1.15-3	3.36-3	-4.50-3
	3	-8.12-3	-2.00-3	-9.49-4	2.26-3	-1.31-3		3	-8.05-3	-2.16-3	-9.83-4	2.16-3	-1.18-3
	5	-2.73-2	-3.95-3	1.17-3	9.56-3	-1.07-2		5	-2.54-2	-3.68-3	8.26-4	8.84-3	-9.66-3
	10	-1.26-1	-2.09-2	1.27-2	4.44-2	-5.71-2		10	-1.21-1	-1.99-2	1.22-2	4.27-2	-5.49-2
4p <sub>3/2</sub>	1	-7.67-3	-3.26-3	1.82-3	2.13-3	-3.95-3	4p <sub>3/2</sub>	1	-8.12-3	-3.33-3	1.89-3	2.29-3	-4.18-3
	3	-2.64-3	-3.22-3	1.75-3	1.18-4	-1.87-3		3	-2.54-3	-3.36-3	1.70-3	1.27-5	-1.71-3
	5	-1.94-2	-6.62-3	6.30-3	6.38-3	-1.27-2		5	-1.76-2	-6.35-3	5.92-3	5.70-3	-1.16-2
	10	-1.10-1	-2.74-2	2.50-2	3.79-2	-6.28-2		10	-1.05-1	-2.65-2	2.44-2	3.64-2	-6.08-2
4d <sub>3/2</sub>	1	-2.07-3	-2.59-4	-3.62-4	6.53-4	-2.92-4	4d <sub>3/2</sub>	1	-1.78-3	-2.55-4	-3.47-4	5.42-4	-1.95-4
	3	-4.56-2	-6.53-3	9.08-4	1.58-2	-1.67-2		3	-4.34-2	-6.07-3	8.18-4	1.51-2	-1.59-2
	5	-1.15-1	-1.90-2	3.34-3	3.89-2	-4.22-2		5	-1.11-1	-1.82-2	3.39-3	3.78-2	-4.12-2
	10	-3.09-1	-5.65-2	2.45-3	1.01-1	-1.04-1		10	-3.04-1	-5.52-2	3.25-3	1.00-1	-1.03-1

Table 1 (continued)

Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$	Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$
4d <sub>5/2</sub>	1	5.02–4	−5.68–4	6.71–4	−2.94–4	−3.77–4	4d <sub>5/2</sub>	1	8.14–4	−5.61–4	6.87–4	−4.13–4	−2.74–4
	3	−3.82–2	−7.71–3	4.09–3	1.30–2	−1.71–2		3	−3.60–2	−7.24–3	4.01–3	1.23–2	−1.63–2
	5	−1.03–1	−2.13–2	8.33–3	3.42–2	−4.25–2		5	−9.92–2	−2.04–2	8.38–3	3.32–2	−4.15–2
	10	−2.88–1	−6.22–2	1.14–2	9.26–2	−1.04–1		10	−2.83–1	−6.10–2	1.21–2	9.12–2	−1.03–1
5s <sub>1/2</sub>	1	−5.36–3	1.03–3	2.05–3	2.97–3	−5.02–3	5s <sub>1/2</sub>	1	−5.03–3	1.25–3	2.01–3	2.91–3	−4.92–3
	3	−2.39–2	−9.20–3	4.80–3	6.85–3	−1.16–2		3	−2.51–2	−9.46–3	5.09–3	7.26–3	−1.23–2
	5	−1.79–2	−9.93–3	2.60–3	3.70–3	−6.31–3		5	−1.95–2	−1.04–2	2.97–3	4.23–3	−7.20–3
	10	−1.56–2	−1.03–2	2.07–3	2.55–3	−4.62–3		10	−1.51–2	−1.05–2	1.81–3	2.19–3	−3.99–3
5p <sub>1/2</sub>	1	−9.47–3	−2.41–3	1.10–3	3.04–3	−4.15–3	5p <sub>1/2</sub>	1	−1.01–2	−2.54–3	1.20–3	3.24–3	−4.44–3
	3	−8.07–3	−2.17–3	−8.87–4	2.18–3	−1.29–3		3	−8.13–3	−2.42–3	−8.77–4	2.11–3	−1.23–3
	5	−2.68–2	−4.06–3	1.15–3	9.31–3	−1.05–2		5	−2.48–2	−3.75–3	7.94–4	8.56–3	−9.36–3
	10	−1.24–1	−2.07–2	1.26–2	4.39–2	−5.66–2		10	−1.19–1	−1.98–2	1.21–2	4.22–2	−5.43–2
$Z = 51, \text{Sb: } 5s^2_{1/2} 4d^4_{3/2} 4d^6_{5/2} 5p^2_{1/2} 5p^1_{3/2}$							$Z = 52, \text{Te: } 5s^2_{1/2} 4d^4_{3/2} 4d^6_{5/2} 5p^2_{1/2} 5p^2_{3/2}$						
3s <sub>1/2</sub>	1	−1.23–2	9.69–4	4.27–3	6.17–3	−1.04–2	3s <sub>1/2</sub>	1	−1.21–2	1.42–3	4.34–3	6.28–3	−1.06–2
	3	−3.18–2	−1.14–2	6.65–3	9.47–3	−1.61–2		3	−3.35–2	−1.17–2	7.09–3	1.01–2	−1.72–2
	5	−2.30–2	−1.16–2	3.74–3	5.31–3	−9.04–3		5	−2.53–2	−1.23–2	4.24–3	6.03–3	−1.03–2
	10	−1.49–2	−1.04–2	1.84–3	2.18–3	−4.02–3		10	−1.48–2	−1.07–2	1.68–3	1.98–3	−3.66–3
3p <sub>1/2</sub>	1	−1.77–2	−5.31–3	8.97–4	5.14–3	−6.04–3	3p <sub>1/2</sub>	1	−1.91–2	−5.67–3	9.73–4	5.57–3	−6.54–3
	3	−9.31–3	−1.55–3	−1.55–3	2.79–3	−1.24–3		3	−9.38–3	−1.72–3	−1.63–3	2.74–3	−1.11–3
	5	−2.82–2	−3.09–3	4.75–4	1.01–2	−1.06–2		5	−2.66–2	−2.85–3	1.30–4	9.53–3	−9.66–3
	10	−1.26–1	−1.97–2	1.19–2	4.49–2	−5.68–2		10	−1.21–1	−1.87–2	1.14–2	4.33–2	−5.47–2
3p <sub>3/2</sub>	1	−1.24–2	−5.73–3	2.42–3	3.16–3	−5.58–3	3p <sub>3/2</sub>	1	−1.35–2	−6.11–3	2.55–3	3.48–3	−6.03–3
	3	−2.14–3	−2.97–3	1.86–3	3.86–5	−1.90–3		3	−2.03–3	−3.13–3	1.82–3	−7.50–5	−1.74–3
	5	−1.91–2	−6.07–3	6.32–3	6.49–3	−1.28–2		5	−1.76–2	−5.85–3	5.97–3	5.89–3	−1.19–2
	10	−1.10–1	−2.67–2	2.50–2	3.82–2	−6.32–2		10	−1.06–1	−2.58–2	2.44–2	3.69–2	−6.13–2
3d <sub>3/2</sub>	1	−2.72–3	1.67–3	−1.33–3	1.49–3	−1.58–4	3d <sub>3/2</sub>	1	−2.05–3	1.92–3	−1.38–3	1.31–3	7.19–5
	3	−5.45–2	−6.40–3	1.32–4	1.93–2	−1.94–2		3	−5.28–2	−5.82–3	−8.12–6	1.88–2	−1.88–2
	5	−1.25–1	−1.95–2	2.60–3	4.28–2	−4.54–2		5	−1.23–1	−1.88–2	2.62–3	4.21–2	−4.47–2
	10	−3.20–1	−5.75–2	2.89–3	1.05–1	−1.08–1		10	−3.16–1	−5.64–2	3.55–3	1.05–1	−1.08–1
3d <sub>5/2</sub>	1	1.38–3	1.23–3	3.43–4	8.21–6	−3.51–4	3d <sub>5/2</sub>	1	2.19–3	1.47–3	3.49–4	−2.20–4	−1.29–4
	3	−4.60–2	−7.75–3	3.80–3	1.60–2	−1.98–2		3	−4.41–2	−7.16–3	3.72–3	1.55–2	−1.92–2
	5	−1.12–1	−2.20–2	7.95–3	3.77–2	−4.56–2		5	−1.10–1	−2.12–2	8.01–3	3.70–2	−4.50–2
	10	−2.99–1	−6.34–2	1.19–2	9.65–2	−1.08–1		10	−2.95–1	−6.23–2	1.25–2	9.55–2	−1.08–1
4s <sub>1/2</sub>	1	−5.58–3	1.49–3	2.26–3	3.28–3	−5.54–3	4s <sub>1/2</sub>	1	−5.12–3	1.87–3	2.22–3	3.24–3	−5.46–3
	3	−2.66–2	−9.73–3	5.49–3	7.84–3	−1.33–2		3	−2.77–2	−9.92–3	5.80–3	8.28–3	−1.41–2
	5	−2.13–2	−1.10–2	3.38–3	4.82–3	−8.20–3		5	−2.32–2	−1.16–2	3.81–3	5.43–3	−9.24–3
	10	−1.48–2	−1.07–2	1.64–3	1.96–3	−3.60–3		10	−1.47–2	−1.10–2	1.50–3	1.77–3	−3.27–3
4p <sub>1/2</sub>	1	−1.11–2	−2.86–3	1.20–3	3.54–3	−4.74–3	4p <sub>1/2</sub>	1	−1.15–2	−2.86–3	1.26–3	3.71–3	−4.97–3
	3	−8.10–3	−2.34–3	−9.97–4	2.11–3	−1.11–3		3	−8.27–3	−2.54–3	−9.94–4	2.09–3	−1.10–3
	5	−2.36–2	−3.45–3	5.04–4	8.15–3	−8.66–3		5	−2.20–2	−3.29–3	1.99–4	7.53–3	−7.73–3
	10	−1.16–1	−1.89–2	1.16–2	4.10–2	−5.26–2		10	−1.11–1	−1.80–2	1.11–2	3.93–2	−5.04–2
4p <sub>3/2</sub>	1	−8.53–3	−3.38–3	1.95–3	2.45–3	−4.39–3	4p <sub>3/2</sub>	1	−8.93–3	−3.43–3	2.00–3	2.60–3	−4.60–3
	3	−2.55–3	−3.53–3	1.67–3	−5.61–5	−1.61–3		3	−2.66–3	−3.72–3	1.66–3	−9.26–5	−1.56–3
	5	−1.60–2	−6.11–3	5.55–3	5.07–3	−1.06–2		5	−1.46–2	−5.95–3	5.20–3	4.50–3	−9.70–3
	10	−1.01–1	−2.56–2	2.38–2	3.50–2	−5.87–2		10	−9.70–2	−2.47–2	2.32–2	3.35–2	−5.67–2
4d <sub>3/2</sub>	1	−1.55–3	−2.68–4	−3.25–4	4.48–4	−1.22–4	4d <sub>3/2</sub>	1	−1.39–3	−3.04–4	−2.98–4	3.74–4	−7.64–5
	3	−4.13–2	−5.63–3	7.19–4	1.44–2	−1.51–2		3	−3.92–2	−5.18–3	6.21–4	1.37–2	−1.43–2
	5	−1.08–1	−1.74–2	3.40–3	3.68–2	−4.02–2		5	−1.04–1	−1.66–2	3.40–3	3.57–2	−3.91–2
	10	−2.98–1	−5.40–2	4.01–3	9.86–2	−1.03–1		10	−2.93–1	−5.29–2	4.74–3	9.72–2	−1.02–1
4d <sub>5/2</sub>	1	1.08–3	−5.71–4	7.10–4	−5.17–4	−1.93–4	4d <sub>5/2</sub>	1	1.27–3	−6.03–4	7.40–4	−6.02–4	−1.38–4
	3	−3.39–2	−6.78–3	3.94–3	1.16–2	−1.56–2		3	−3.18–2	−6.32–3	3.86–3	1.10–2	−1.48–2
	5	−9.58–2	−1.96–2	8.40–3	3.22–2	−4.06–2		5	−9.24–2	−1.88–2	8.41–3	3.11–2	−3.96–2
	10	−2.78–1	−5.97–2	1.28–2	8.99–2	−1.03–1		10	−2.73–1	−5.85–2	1.34–2	8.86–2	−1.02–1
5s <sub>1/2</sub>	1	−4.61–3	1.53–3	1.95–3	2.85–3	−4.80–3	5s <sub>1/2</sub>	1	−4.11–3	1.86–3	1.89–3	2.77–3	−4.66–3
	3	−2.61–2	−9.61–3	5.37–3	7.66–3	−1.30–2		3	−2.71–2	−9.77–3	5.65–3	8.07–3	−1.37–2
	5	−2.12–2	−1.10–2	3.35–3	4.78–3	−8.13–3		5	−2.30–2	−1.15–2	3.76–3	5.36–3	−9.12–3
	10	−1.48–2	−1.08–2	1.60–3	1.92–3	−3.52–3		10	−1.47–2	−1.11–2	1.46–3	1.73–3	−3.19–3

(continued on next page)

Table 1 (continued)

Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$	Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$
5p <sub>1/2</sub>	1	-1.04-2	-2.54-3	1.26-3	3.38-3	-4.64-3	5p <sub>1/2</sub>	1	-1.05-2	-2.44-3	1.30-3	3.49-3	-4.79-3
	3	-8.11-3	-2.55-3	-8.96-4	2.04-3	-1.15-3		3	-8.32-3	-2.78-3	-8.72-4	2.04-3	-1.17-3
	5	-2.30-2	-3.54-3	4.96-4	7.87-3	-8.36-3		5	-2.13-2	-3.36-3	1.96-4	7.22-3	-7.42-3
	10	-1.14-1	-1.88-2	1.16-2	4.05-2	-5.20-2		10	-1.09-1	-1.79-2	1.10-2	3.87-2	-4.98-2
5p <sub>3/2</sub>	1	-8.19-3	-3.10-3	1.92-3	2.42-3	-4.33-3	5p <sub>3/2</sub>	1	-8.39-3	-3.05-3	1.94-3	2.52-3	-4.46-3
	3	-2.78-3	-3.72-3	1.67-3	-4.46-5	-1.63-3		3	-2.95-3	-3.94-3	1.67-3	-6.18-5	-1.61-3
	5	-1.56-2	-6.16-3	5.45-3	4.86-3	-1.03-2		5	-1.41-2	-5.96-3	5.08-3	4.26-3	-9.34-3
	10	-9.99-2	-2.55-2	2.36-2	3.45-2	-5.82-2		10	-9.57-2	-2.46-2	2.30-2	3.30-2	-5.60-2
$Z = 53$ , I: $5s_{1/2}^2 4d_{3/2}^4 4d_{5/2}^6 5p_{1/2}^2 5p_{3/2}^3$							$Z = 54$ , Xe: $5s_{1/2}^2 4d_{3/2}^4 4d_{5/2}^6 5p_{1/2}^2 5p_{3/2}^4$						
3s <sub>1/2</sub>	1	-1.19-2	1.90-3	4.41-3	6.39-3	-1.08-2	3s <sub>1/2</sub>	1	-1.16-2	2.41-3	4.49-3	6.52-3	-1.10-2
	3	-3.52-2	-1.21-2	7.54-3	1.08-2	-1.83-2		3	-3.69-2	-1.24-2	8.00-3	1.14-2	-1.94-2
	5	-2.76-2	-1.30-2	4.76-3	6.77-3	-1.15-2		5	-3.00-2	-1.38-2	5.31-3	7.56-3	-1.29-2
	10	-1.49-2	-1.11-2	1.59-3	1.86-3	-3.45-3		10	-1.53-2	-1.15-2	1.57-3	1.83-3	-3.40-3
3p <sub>1/2</sub>	1	-2.05-2	-6.03-3	1.04-3	6.01-3	-7.05-3	3p <sub>1/2</sub>	1	-2.20-2	-6.40-3	1.11-3	6.46-3	-7.57-3
	3	-9.57-3	-1.92-3	-1.69-3	2.72-3	-1.04-3		3	-9.90-3	-2.16-3	-1.73-3	2.75-3	-1.02-3
	5	-2.50-2	-2.61-3	-1.98-4	8.93-3	-8.73-3		5	-2.36-2	-2.41-3	-5.14-4	8.37-3	-7.86-3
	10	-1.17-1	-1.77-2	1.08-2	4.17-2	-5.26-2		10	-1.12-1	-1.67-2	1.02-2	4.02-2	-5.04-2
3p <sub>3/2</sub>	1	-1.47-2	-6.49-3	2.67-3	3.81-3	-6.48-3	3p <sub>3/2</sub>	1	-1.58-2	-6.88-3	2.79-3	4.14-3	-6.94-3
	3	-2.03-3	-3.31-3	1.79-3	-1.55-4	-1.64-3		3	-2.13-3	-3.53-3	1.79-3	-2.03-4	-1.59-3
	5	-1.61-2	-5.63-3	5.65-3	5.30-3	-1.09-2		5	-1.46-2	-5.43-3	5.34-3	4.74-3	-1.01-2
	10	-1.02-1	-2.49-2	2.38-2	3.55-2	-5.93-2		10	-9.79-2	-2.40-2	2.32-2	3.42-2	-5.74-2
3d <sub>3/2</sub>	1	-1.38-3	2.16-3	-1.43-3	1.13-3	2.99-4	3d <sub>3/2</sub>	1	-7.13-4	2.41-3	-1.48-3	9.55-4	5.23-4
	3	-5.11-2	-5.25-3	-1.69-4	1.83-2	-1.81-2		3	-4.93-2	-4.68-3	-3.39-4	1.78-2	-1.75-2
	5	-1.20-1	-1.80-2	2.59-3	4.14-2	-4.40-2		5	-1.18-1	-1.73-2	2.53-3	4.08-2	-4.33-2
	10	-3.12-1	-5.53-2	4.16-3	1.04-1	-1.08-1		10	-3.08-1	-5.42-2	4.73-3	1.03-1	-1.07-1
3d <sub>5/2</sub>	1	3.01-3	1.70-3	3.59-4	-4.50-4	9.06-5	3d <sub>5/2</sub>	1	3.84-3	1.95-3	3.75-4	-6.82-4	3.07-4
	3	-4.23-2	-6.60-3	3.63-3	1.50-2	-1.86-2		3	-4.05-2	-6.03-3	3.54-3	1.45-2	-1.80-2
	5	-1.07-1	-2.05-2	8.03-3	3.64-2	-4.44-2		5	-1.05-1	-1.98-2	8.03-3	3.57-2	-4.37-2
	10	-2.91-1	-6.12-2	1.31-2	9.45-2	-1.08-1		10	-2.87-1	-6.01-2	1.36-2	9.36-2	-1.07-1
4s <sub>1/2</sub>	1	-4.67-3	2.25-3	2.19-3	3.21-3	-5.40-3	4s <sub>1/2</sub>	1	-4.22-3	2.64-3	2.16-3	3.18-3	-5.34-3
	3	-2.88-2	-1.01-2	6.11-3	8.73-3	-1.48-2		3	-2.99-2	-1.02-2	6.41-3	9.16-3	-1.56-2
	5	-2.51-2	-1.21-2	4.24-3	6.05-3	-1.03-2		5	-2.71-2	-1.27-2	4.69-3	6.70-3	-1.14-2
	10	-1.49-2	-1.14-2	1.41-3	1.66-3	-3.08-3		10	-1.53-2	-1.19-2	1.39-3	1.64-3	-3.03-3
4p <sub>1/2</sub>	1	-1.19-2	-2.83-3	1.30-3	3.88-3	-5.18-3	4p <sub>1/2</sub>	1	-1.23-2	-2.80-3	1.34-3	4.05-3	-5.40-3
	3	-8.55-3	-2.78-3	-9.73-4	2.11-3	-1.14-3		3	-8.94-3	-3.03-3	-9.36-4	2.18-3	-1.24-3
	5	-2.06-2	-3.16-3	-7.84-5	6.95-3	-6.87-3		5	-1.93-2	-3.06-3	-3.33-4	6.42-3	-6.09-3
	10	-1.06-1	-1.70-2	1.05-2	3.77-2	-4.82-2		10	-1.01-1	-1.61-2	9.95-3	3.61-2	-4.60-2
4p <sub>3/2</sub>	1	-9.32-3	-3.47-3	2.05-3	2.75-3	-4.80-3	4p <sub>3/2</sub>	1	-9.69-3	-3.50-3	2.10-3	2.90-3	-5.00-3
	3	-2.87-3	-3.94-3	1.66-3	-9.49-5	-1.57-3		3	-3.18-3	-4.19-3	1.69-3	-6.58-5	-1.62-3
	5	-1.32-2	-5.81-3	4.88-3	3.95-3	-8.83-3		5	-1.20-2	-5.71-3	4.59-3	3.45-3	-8.04-3
	10	-9.29-2	-2.39-2	2.25-2	3.21-2	-5.46-2		10	-8.89-2	-2.30-2	2.19-2	3.07-2	-5.26-2
4d <sub>3/2</sub>	1	-1.29-3	-3.60-4	-2.64-4	3.20-4	-5.67-5	4d <sub>3/2</sub>	1	-1.27-3	-4.38-4	-2.25-4	2.87-4	-6.18-5
	3	-3.72-2	-4.77-3	5.11-4	1.31-2	-1.36-2		3	-3.52-2	-4.37-3	3.96-4	1.24-2	-1.28-2
	5	-1.01-1	-1.58-2	3.36-3	3.47-2	-3.80-2		5	-9.75-2	-1.50-2	3.30-3	3.36-2	-3.69-2
	10	-2.89-1	-5.17-2	5.42-3	9.58-2	-1.01-1		10	-2.84-1	-5.06-2	6.07-3	9.44-2	-1.01-1
4d <sub>5/2</sub>	1	1.40-3	-6.56-4	7.76-4	-6.68-4	-1.08-4	4d <sub>5/2</sub>	1	1.47-3	-7.30-4	8.18-4	-7.16-4	-1.02-4
	3	-2.98-2	-5.90-3	3.77-3	1.03-2	-1.41-2		3	-2.79-2	-5.48-3	3.68-3	9.68-3	-1.34-2
	5	-8.91-2	-1.80-2	8.39-3	3.01-2	-3.85-2		5	-8.58-2	-1.72-2	8.35-3	2.91-2	-3.75-2
	10	-2.68-1	-5.74-2	1.41-2	8.73-2	-1.01-1		10	-2.64-1	-5.62-2	1.46-2	8.60-2	-1.01-1
5s <sub>1/2</sub>	1	-3.55-3	2.22-3	1.82-3	2.67-3	-4.49-3	5s <sub>1/2</sub>	1	-3.05-3	2.55-3	1.76-3	2.59-3	-4.35-3
	3	-2.81-2	-9.88-3	5.92-3	8.46-3	-1.44-2		3	-2.88-2	-9.86-3	6.15-3	8.80-3	-1.50-2
	5	-2.49-2	-1.21-2	4.18-3	5.97-3	-1.02-2		5	-2.67-2	-1.26-2	4.61-3	6.58-3	-1.12-2
	10	-1.49-2	-1.15-2	1.38-3	1.63-3	-3.01-3		10	-1.53-2	-1.19-2	1.35-3	1.61-3	-2.96-3
5p <sub>1/2</sub>	1	-1.06-2	-2.28-3	1.31-3	3.58-3	-4.89-3	5p <sub>1/2</sub>	1	-1.07-2	-2.14-3	1.34-3	3.67-3	-5.01-3
	3	-8.63-3	-3.03-3	-8.37-4	2.07-3	-1.24-3		3	-8.88-3	-3.18-3	-8.21-4	2.12-3	-1.30-3
	5	-1.99-2	-3.28-3	-5.46-5	6.65-3	-6.59-3		5	-1.87-2	-3.22-3	-3.02-4	6.12-3	-5.82-3
	10	-1.04-1	-1.69-2	1.05-2	3.70-2	-4.75-2		10	-9.95-2	-1.60-2	9.89-3	3.54-2	-4.53-2

Table 1 (continued)

Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$	Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$
5p <sub>3/2</sub>	1	-8.47–3	-2.95–3	1.94–3	2.60–3	-4.54–3	5p <sub>3/2</sub>	1	-8.59–3	-2.87–3	1.96–3	2.68–3	-4.64–3
	3	-3.22–3	-4.17–3	1.68–3	-4.31–5	-1.64–3		3	-3.39–3	-4.29–3	1.67–3	-2.56–5	-1.64–3
	5	-1.28–2	-5.88–3	4.77–3	3.73–3	-8.50–3		5	-1.17–2	-5.81–3	4.47–3	3.24–3	-7.71–3
	10	-9.15–2	-2.37–2	2.23–2	3.16–2	-5.39–2		10	-8.75–2	-2.29–2	2.17–2	3.02–2	-5.18–2
<i>Z</i> = 55, Cs: 6s <sub>1/2</sub> <sup>1</sup>							<i>Z</i> = 56, Ba: 6s <sub>1/2</sub> <sup>2</sup>						
3s <sub>1/2</sub>	1	-1.15–2	2.84–3	4.56–3	6.64–3	-1.12–2	3s <sub>1/2</sub>	1	-1.13–2	3.29–3	4.64–3	6.78–3	-1.14–2
	3	-3.85–2	-1.26–2	8.42–3	1.20–2	-2.05–2		3	-4.00–2	-1.28–2	8.85–3	1.27–2	-2.15–2
	5	-3.24–2	-1.45–2	5.86–3	8.36–3	-1.42–2		5	-3.48–2	-1.51–2	6.41–3	9.15–3	-1.56–2
	10	-1.60–2	-1.21–2	1.60–3	1.89–3	-3.49–3		10	-1.69–2	-1.26–2	1.69–3	2.03–3	-3.72–3
3p <sub>1/2</sub>	1	-2.34–2	-6.74–3	1.16–3	6.88–3	-8.03–3	3p <sub>1/2</sub>	1	-2.48–2	-7.10–3	1.20–3	7.32–3	-8.51–3
	3	-1.03–2	-2.42–3	-1.75–3	2.82–3	-1.07–3		3	-1.09–2	-2.71–3	-1.76–3	2.92–3	-1.16–3
	5	-2.23–2	-2.25–3	-8.14–4	7.86–3	-7.04–3		5	-2.11–2	-2.11–3	-1.09–3	7.38–3	-6.29–3
	10	-1.08–1	-1.58–2	9.65–3	3.87–2	-4.84–2		10	-1.03–1	-1.49–2	9.06–3	3.72–2	-4.63–2
3p <sub>3/2</sub>	1	-1.69–2	-7.24–3	2.90–3	4.44–3	-7.34–3	3p <sub>3/2</sub>	1	-1.80–2	-7.63–3	3.00–3	4.75–3	-7.76–3
	3	-2.34–3	-3.78–3	1.81–3	-2.14–4	-1.59–3		3	-2.64–3	-4.05–3	1.84–3	-1.98–4	-1.64–3
	5	-1.33–2	-5.27–3	5.05–3	4.22–3	-9.27–3		5	-1.20–2	-5.13–3	4.78–3	3.72–3	-8.51–3
	10	-9.41–2	-2.32–2	2.26–2	3.29–2	-5.55–2		10	-9.04–2	-2.24–2	2.20–2	3.16–2	-5.36–2
3d <sub>3/2</sub>	1	-9.57–5	2.66–3	-1.52–3	7.97–4	7.24–4	3d <sub>3/2</sub>	1	6.02–4	2.93–3	-1.56–3	6.20–4	9.38–4
	3	-4.76–2	-4.08–3	-5.07–4	1.73–2	-1.68–2		3	-4.59–2	-3.51–3	-6.86–4	1.68–2	-1.61–2
	5	-1.16–1	-1.66–2	2.44–3	4.01–2	-4.26–2		5	-1.13–1	-1.58–2	2.34–3	3.94–2	-4.18–2
	10	-3.04–1	-5.32–2	5.24–3	1.02–1	-1.07–1		10	-3.01–1	-5.21–2	5.72–3	1.01–1	-1.06–1
3d <sub>5/2</sub>	1	4.60–3	2.18–3	3.92–4	-8.92–4	5.00–4	3d <sub>5/2</sub>	1	5.46–3	2.44–3	4.16–4	-1.12–3	7.08–4
	3	-3.86–2	-5.43–3	3.45–3	1.40–2	-1.74–2		3	-3.69–2	-4.87–3	3.35–3	1.35–2	-1.68–2
	5	-1.03–1	-1.91–2	8.00–3	3.51–2	-4.31–2		5	-1.00–1	-1.83–2	7.97–3	3.44–2	-4.23–2
	10	-2.84–1	-5.91–2	1.41–2	9.26–2	-1.07–1		10	-2.80–1	-5.80–2	1.45–2	9.17–2	-1.06–1
4s <sub>1/2</sub>	1	-3.82–3	2.98–3	2.13–3	3.15–3	-5.28–3	4s <sub>1/2</sub>	1	-3.43–3	3.32–3	2.11–3	3.12–3	-5.23–3
	3	-3.08–2	-1.03–2	6.67–3	9.54–3	-1.62–2		3	-3.17–2	-1.03–2	6.93–3	9.92–3	-1.68–2
	5	-2.90–2	-1.32–2	5.14–3	7.34–3	-1.25–2		5	-3.09–2	-1.37–2	5.58–3	7.97–3	-1.35–2
	10	-1.59–2	-1.23–2	1.42–3	1.70–3	-3.12–3		10	-1.67–2	-1.29–2	1.51–3	1.84–3	-3.34–3
4p <sub>1/2</sub>	1	-1.25–2	-2.74–3	1.37–3	4.18–3	-5.55–3	4p <sub>1/2</sub>	1	-1.28–2	-2.68–3	1.39–3	4.32–3	-5.71–3
	3	-9.40–3	-3.29–3	-8.85–4	2.27–3	-1.38–3		3	-9.94–3	-3.56–3	-8.21–4	2.39–3	-1.57–3
	5	-1.82–2	-3.01–3	-5.64–4	5.95–3	-5.38–3		5	-1.72–2	-3.00–3	-7.64–4	5.52–3	-4.76–3
	10	-9.67–2	-1.52–2	9.37–3	3.45–2	-4.38–2		10	-9.22–2	-1.44–2	8.77–3	3.29–2	-4.17–2
4p <sub>3/2</sub>	1	-9.97–3	-3.52–3	2.14–3	3.01–3	-5.15–3	4p <sub>3/2</sub>	1	-1.02–2	-3.52–3	2.16–3	3.12–3	-5.28–3
	3	-3.55–3	-4.44–3	1.73–3	-7.15–6	-1.72–3		3	-3.99–3	-4.70–3	1.78–3	7.44–5	-1.86–3
	5	-1.10–2	-5.64–3	4.32–3	2.99–3	-7.31–3		5	-1.00–2	-5.61–3	4.08–3	2.58–3	-6.66–3
	10	-8.50–2	-2.22–2	2.12–2	2.94–2	-5.06–2		10	-8.12–2	-2.15–2	2.06–2	2.80–2	-4.86–2
4d <sub>3/2</sub>	1	-1.30–3	-5.22–4	-1.89–4	2.75–4	-8.62–5	4d <sub>3/2</sub>	1	-1.40–3	-6.25–4	-1.52–4	2.81–4	-1.29–4
	3	-3.32–2	-3.96–3	2.82–4	1.18–2	-1.21–2		3	-3.14–2	-3.59–3	1.60–4	1.12–2	-1.13–2
	5	-9.42–2	-1.43–2	3.21–3	3.26–2	-3.58–2		5	-9.09–2	-1.36–2	3.11–3	3.16–2	-3.47–2
	10	-2.79–1	-4.94–2	6.67–3	9.31–2	-9.97–2		10	-2.74–1	-4.83–2	7.23–3	9.17–2	-9.89–2
4d <sub>5/2</sub>	1	1.47–3	-8.10–4	8.55–4	-7.40–4	-1.15–4	4d <sub>5/2</sub>	1	1.41–3	-9.08–4	8.93–4	-7.47–4	-1.46–4
	3	-2.59–2	-5.06–3	3.59–3	9.06–3	-1.27–2		3	-2.41–2	-4.68–3	3.49–3	8.47–3	-1.20–2
	5	-8.27–2	-1.65–2	8.28–3	2.81–2	-3.64–2		5	-7.94–2	-1.57–2	8.21–3	2.71–2	-3.54–2
	10	-2.59–1	-5.50–2	1.52–2	8.47–2	-9.98–2		10	-2.54–1	-5.38–2	1.57–2	8.34–2	-9.90–2
5s <sub>1/2</sub>	1	-2.71–3	2.76–3	1.71–3	2.53–3	-4.24–3	5s <sub>1/2</sub>	1	-2.30–3	3.05–3	1.66–3	2.47–3	-4.14–3
	3	-2.95–2	-9.89–3	6.37–3	9.11–3	-1.55–2		3	-3.02–2	-9.88–3	6.58–3	9.42–3	-1.60–2
	5	-2.85–2	-1.31–2	5.01–3	7.16–3	-1.22–2		5	-3.03–2	-1.36–2	5.44–3	7.79–3	-1.32–2
	10	-1.59–2	-1.24–2	1.39–3	1.67–3	-3.06–3		10	-1.67–2	-1.29–2	1.47–3	1.81–3	-3.28–3
5p <sub>1/2</sub>	1	-1.08–2	-2.09–3	1.37–3	3.74–3	-5.11–3	5p <sub>1/2</sub>	1	-1.07–2	-1.93–3	1.37–3	3.79–3	-5.17–3
	3	-9.38–3	-3.47–3	-7.33–4	2.21–3	-1.48–3		3	-9.92–3	-3.74–3	-6.52–4	2.34–3	-1.69–3
	5	-1.76–2	-3.19–3	-5.11–4	5.65–3	-5.13–3		5	-1.66–2	-3.22–3	-6.95–4	5.23–3	-4.53–3
	10	-9.48–2	-1.52–2	9.30–3	3.37–2	-4.30–2		10	-9.03–2	-1.43–2	8.70–3	3.21–2	-4.08–2
5p <sub>3/2</sub>	1	-8.78–3	-2.88–3	1.98–3	2.75–3	-4.73–3	5p <sub>3/2</sub>	1	-8.81–3	-2.79–3	1.97–3	2.80–3	-4.77–3
	3	-3.86–3	-4.58–3	1.73–3	5.69–5	-1.78–3		3	-4.33–3	-4.84–3	1.78–3	1.54–4	-1.94–3
	5	-1.06–2	-5.74–3	4.21–3	2.79–3	-7.00–3		5	-9.77–3	-5.75–3	3.97–3	2.40–3	-6.37–3
	10	-8.35–2	-2.21–2	2.10–2	2.87–2	-4.97–2		10	-7.95–2	-2.13–2	2.03–2	2.74–2	-4.77–2

(continued on next page)

Table 1 (continued)

Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$	Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$
6s <sub>1/2</sub>	1	-2.51-3	2.86-3	1.67-3	2.48-3	-4.16-3	6s <sub>1/2</sub>	1	-2.40-3	2.95-3	1.66-3	2.47-3	-4.14-3
	3	-2.95-2	-9.84-3	6.38-3	9.13-3	-1.55-2		3	-3.03-2	-9.91-3	6.61-3	9.46-3	-1.61-2
	5	-2.87-2	-1.32-2	5.06-3	7.23-3	-1.23-2		5	-3.05-2	-1.36-2	5.47-3	7.83-3	-1.33-2
	10	-1.59-2	-1.24-2	1.39-3	1.68-3	-3.06-3		10	-1.68-2	-1.30-2	1.48-3	1.82-3	-3.29-3
<i>Z</i> = 57, La: 5d <sub>3/2</sub> <sup>1</sup> 6s <sub>1/2</sub> <sup>2</sup>							<i>Z</i> = 58, Ce: 4f <sub>5/2</sub> <sup>2</sup> 6s <sub>1/2</sub> <sup>2</sup>						
3s <sub>1/2</sub>	1	-1.11-2	3.78-3	4.71-3	6.89-3	-1.16-2	3s <sub>1/2</sub>	1	-1.04-2	4.63-3	4.73-3	6.95-3	-1.17-2
	3	-4.15-2	-1.30-2	9.26-3	1.33-2	-2.25-2		3	-4.32-2	-1.31-2	9.75-3	1.40-2	-2.37-2
	5	-3.73-2	-1.58-2	7.00-3	9.99-3	-1.70-2		5	-4.01-2	-1.65-2	7.66-3	1.09-2	-1.86-2
	10	-1.80-2	-1.33-2	1.84-3	2.26-3	-4.10-3		10	-1.95-2	-1.40-2	2.06-3	2.59-3	-4.65-3
3p <sub>1/2</sub>	1	-2.62-2	-7.44-3	1.23-3	7.75-3	-8.99-3	3p <sub>1/2</sub>	1	-2.80-2	-7.81-3	1.27-3	8.34-3	-9.61-3
	3	-1.16-2	-3.04-3	-1.75-3	3.06-3	-1.31-3		3	-1.25-2	-3.47-3	-1.72-3	3.27-3	-1.55-3
	5	-2.01-2	-2.02-3	-1.36-3	6.94-3	-5.58-3		5	-1.91-2	-1.97-3	-1.64-3	6.51-3	-4.87-3
	10	-9.92-2	-1.40-2	8.45-3	3.58-2	-4.42-2		10	-9.49-2	-1.31-2	7.82-3	3.43-2	-4.21-2
3p <sub>3/2</sub>	1	-1.91-2	-7.99-3	3.09-3	5.06-3	-8.15-3	3p <sub>3/2</sub>	1	-2.05-2	-8.41-3	3.20-3	5.48-3	-8.68-3
	3	-3.04-3	-4.36-3	1.89-3	-1.49-4	-1.74-3		3	-3.61-3	-4.75-3	1.97-3	-6.18-5	-1.91-3
	5	-1.09-2	-5.03-3	4.52-3	3.26-3	-7.79-3		5	-9.81-3	-4.97-3	4.26-3	2.79-3	-7.04-3
	10	-8.67-2	-2.16-2	2.14-2	3.03-2	-5.17-2		10	-8.30-2	-2.08-2	2.07-2	2.90-2	-4.97-2
3d <sub>3/2</sub>	1	1.25-3	3.18-3	-1.59-3	4.54-4	1.14-3	3d <sub>3/2</sub>	1	1.96-3	3.41-3	-1.62-3	2.54-4	1.36-3
	3	-4.41-2	-2.92-3	-8.76-4	1.63-2	-1.54-2		3	-4.23-2	-2.30-3	-1.12-3	1.58-2	-1.47-2
	5	-1.11-1	-1.51-2	2.22-3	3.87-2	-4.09-2		5	-1.08-1	-1.42-2	2.05-3	3.80-2	-4.00-2
	10	-2.97-1	-5.10-2	6.17-3	9.95-2	-1.06-1		10	-2.93-1	-5.00-2	6.60-3	9.86-2	-1.05-1
3d <sub>5/2</sub>	1	6.25-3	2.68-3	4.41-4	-1.34-3	9.00-4	3d <sub>5/2</sub>	1	7.18-3	2.90-3	4.91-4	-1.62-3	1.12-3
	3	-3.50-2	-4.27-3	3.24-3	1.29-2	-1.62-2		3	-3.30-2	-3.66-3	3.09-3	1.24-2	-1.55-2
	5	-9.77-2	-1.75-2	7.91-3	3.36-2	-4.16-2		5	-9.50-2	-1.67-2	7.84-3	3.29-2	-4.08-2
	10	-2.76-1	-5.69-2	1.49-2	9.07-2	-1.06-1		10	-2.73-1	-5.59-2	1.54-2	8.98-2	-1.05-1
4s <sub>1/2</sub>	1	-2.98-3	3.69-3	2.07-3	3.08-3	-5.16-3	4s <sub>1/2</sub>	1	-2.17-3	4.33-3	2.00-3	3.00-3	-5.00-3
	3	-3.24-2	-1.03-2	7.17-3	1.03-2	-1.74-2		3	-3.33-2	-1.02-2	7.46-3	1.07-2	-1.82-2
	5	-3.28-2	-1.42-2	6.04-3	8.64-3	-1.47-2		5	-3.50-2	-1.48-2	6.57-3	9.41-3	-1.60-2
	10	-1.77-2	-1.34-2	1.65-3	2.06-3	-3.70-3		10	-1.91-2	-1.41-2	1.86-3	2.37-3	-4.23-3
4p <sub>1/2</sub>	1	-1.30-2	-2.58-3	1.40-3	4.44-3	-5.85-3	4p <sub>1/2</sub>	1	-1.31-2	-2.33-3	1.41-3	4.60-3	-6.01-3
	3	-1.06-2	-3.85-3	-7.39-4	2.54-3	-1.80-3		3	-1.14-2	-4.21-3	-6.29-4	2.76-3	-2.13-3
	5	-1.64-2	-3.04-3	-9.51-4	5.14-3	-4.19-3		5	-1.56-2	-3.11-3	-1.14-3	4.78-3	-3.64-3
	10	-8.78-2	-1.35-2	8.15-3	3.13-2	-3.95-2		10	-8.34-2	-1.27-2	7.51-3	2.98-2	-3.73-2
4p <sub>3/2</sub>	1	-1.04-2	-3.49-3	2.17-3	3.21-3	-5.38-3	4p <sub>3/2</sub>	1	-1.06-2	-3.35-3	2.18-3	3.33-3	-5.51-3
	3	-4.51-3	-4.97-3	1.85-3	1.85-4	-2.04-3		3	-5.19-3	-5.32-3	1.96-3	3.39-4	-2.30-3
	5	-9.21-3	-5.62-3	3.86-3	2.21-3	-6.06-3		5	-8.44-3	-5.67-3	3.64-3	1.83-3	-5.47-3
	10	-7.74-2	-2.07-2	1.99-2	2.67-2	-4.65-2		10	-7.36-2	-1.99-2	1.91-2	2.53-2	-4.44-2
4d <sub>3/2</sub>	1	-1.55-3	-7.44-4	-1.09-4	3.02-4	-1.93-4	4d <sub>3/2</sub>	1	-1.78-3	-9.10-4	-4.43-5	3.37-4	-2.93-4
	3	-2.96-2	-3.21-3	3.16-5	1.05-2	-1.06-2		3	-2.77-2	-2.85-3	-1.30-4	9.91-3	-9.78-3
	5	-8.77-2	-1.29-2	2.99-3	3.05-2	-3.35-2		5	-8.44-2	-1.21-2	2.84-3	2.95-2	-3.23-2
	10	-2.69-1	-4.71-2	7.73-3	9.02-2	-9.79-2		10	-2.64-1	-4.58-2	8.19-3	8.88-2	-9.70-2
4d <sub>5/2</sub>	1	1.29-3	-1.02-3	9.35-4	-7.39-4	-1.96-4	4d <sub>5/2</sub>	1	1.15-3	-1.19-3	1.01-3	-7.32-4	-2.76-4
	3	-2.23-2	-4.28-3	3.39-3	7.87-3	-1.13-2		3	-2.04-2	-3.90-3	3.26-3	7.23-3	-1.05-2
	5	-7.63-2	-1.50-2	8.13-3	2.62-2	-3.43-2		5	-7.30-2	-1.42-2	8.03-3	2.51-2	-3.32-2
	10	-2.49-1	-5.26-2	1.61-2	8.20-2	-9.81-2		10	-2.45-1	-5.13-2	1.66-2	8.07-2	-9.72-2
5s <sub>1/2</sub>	1	-1.88-3	3.34-3	1.62-3	2.41-3	-4.03-3	4f <sub>5/2</sub>	1	-1.61-2	-1.64-3	-1.22-3	5.55-3	-4.33-3
	3	-3.08-2	-9.84-3	6.79-3	9.73-3	-1.65-2		3	-1.03-1	-1.65-2	-3.92-3	3.37-2	-2.97-2
	5	-3.22-2	-1.41-2	5.89-3	8.43-3	-1.43-2		5	-2.11-1	-3.67-2	-9.18-3	6.78-2	-5.86-2
	10	-1.77-2	-1.35-2	1.62-3	2.03-3	-3.64-3		10	-4.84-1	-9.25-2	-3.33-2	1.50-1	-1.17-1
5p <sub>1/2</sub>	1	-1.07-2	-1.76-3	1.37-3	3.85-3	-5.22-3	5s <sub>1/2</sub>	1	-1.19-3	3.80-3	1.53-3	2.30-3	-3.83-3
	3	-1.06-2	-4.04-3	-5.50-4	2.50-3	-1.95-3		3	-3.14-2	-9.71-3	7.02-3	1.01-2	-1.71-2
	5	-1.59-2	-3.29-3	-8.67-4	4.86-3	-3.99-3		5	-3.42-2	-1.45-2	6.38-3	9.14-3	-1.55-2
	10	-8.58-2	-1.35-2	8.09-3	3.05-2	-3.86-2		10	-1.91-2	-1.41-2	1.82-3	2.34-3	-4.16-3
5p <sub>3/2</sub>	1	-8.82-3	-2.69-3	1.96-3	2.84-3	-4.80-3	5p <sub>1/2</sub>	1	-1.05-2	-1.44-3	1.35-3	3.90-3	-5.25-3
	3	-4.88-3	-5.12-3	1.86-3	2.79-4	-2.14-3		3	-1.14-2	-4.36-3	-4.26-4	2.72-3	-2.29-3
	5	-9.04-3	-5.80-3	3.75-3	2.04-3	-5.79-3		5	-1.52-2	-3.37-3	-1.04-3	4.51-3	-3.46-3
	10	-7.57-2	-2.05-2	1.96-2	2.60-2	-4.56-2		10	-8.13-2	-1.26-2	7.43-3	2.89-2	-3.64-2

Table 1 (continued)

Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$	Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$
5d <sub>3/2</sub>	1	-1.73–3	-9.98–4	6.58–5	3.08–4	-3.73–4	5p <sub>3/2</sub>	1	-8.74–3	-2.48–3	1.93–3	2.89–3	-4.82–3
	3	-2.79–2	-3.27–3	1.09–4	9.89–3	-1.00–2		3	-5.57–3	-5.44–3	1.97–3	4.45–4	-2.41–3
	5	-8.51–2	-1.26–2	3.13–3	2.96–2	-3.27–2		5	-8.33–3	-5.86–3	3.53–3	1.69–3	-5.22–3
	10	-2.66–1	-4.66–2	7.98–3	8.92–2	-9.72–2		10	-7.18–2	-1.98–2	1.88–2	2.46–2	-4.34–2
6s <sub>1/2</sub>	1	-1.83–3	3.31–3	1.59–3	2.37–3	-3.96–3	6s <sub>1/2</sub>	1	-1.08–3	3.78–3	1.48–3	2.24–3	-3.72–3
	3	-3.09–2	-9.90–3	6.81–3	9.76–3	-1.66–2		3	-3.14–2	-9.75–3	7.02–3	1.01–2	-1.71–2
	5	-3.23–2	-1.41–2	5.92–3	8.47–3	-1.44–2		5	-3.43–2	-1.46–2	6.40–3	9.18–3	-1.56–2
	10	-1.78–2	-1.36–2	1.62–3	2.03–3	-3.65–3		10	-1.91–2	-1.42–2	1.83–3	2.35–3	-4.18–3
<i>Z</i> = 59, Pr: 4f <sub>5/2</sub> <sup>3</sup> 6s <sub>1/2</sub> <sup>2</sup>							<i>Z</i> = 60, Nd: 4f <sub>5/2</sub> <sup>4</sup> 6s <sub>1/2</sub> <sup>2</sup>						
3s <sub>1/2</sub>	1	-9.83–3	5.35–3	4.77–3	7.02–3	-1.18–2	3s <sub>1/2</sub>	1	-9.23–3	6.09–3	4.79–3	7.08–3	-1.19–2
	3	-4.46–2	-1.32–2	1.02–2	1.46–2	-2.48–2		3	-4.59–2	-1.32–2	1.06–2	1.52–2	-2.58–2
	5	-4.28–2	-1.72–2	8.31–3	1.19–2	-2.02–2		5	-4.54–2	-1.78–2	8.95–3	1.28–2	-2.17–2
	10	-2.11–2	-1.48–2	2.34–3	3.00–3	-5.34–3		10	-2.30–2	-1.56–2	2.68–3	3.49–3	-6.17–3
3p <sub>1/2</sub>	1	-2.96–2	-8.11–3	1.28–3	8.84–3	-1.01–2	3p <sub>1/2</sub>	1	-3.10–2	-8.37–3	1.27–3	9.31–3	-1.06–2
	3	-1.35–2	-3.90–3	-1.66–3	3.50–3	-1.84–3		3	-1.46–2	-4.37–3	-1.59–3	3.79–3	-2.20–3
	5	-1.82–2	-1.97–3	-1.89–3	6.13–3	-4.24–3		5	-1.75–2	-2.01–3	-2.11–3	5.79–3	-3.68–3
	10	-9.07–2	-1.22–2	7.18–3	3.28–2	-4.00–2		10	-8.65–2	-1.14–2	6.53–3	3.13–2	-3.79–2
3p <sub>3/2</sub>	1	-2.17–2	-8.78–3	3.28–3	5.84–3	-9.11–3	3p <sub>3/2</sub>	1	-2.29–2	-9.10–3	3.33–3	6.17–3	-9.49–3
	3	-4.28–3	-5.16–3	2.08–3	6.17–5	-2.14–3		3	-5.05–3	-5.59–3	2.19–3	2.22–4	-2.42–3
	5	-8.85–3	-4.95–3	4.02–3	2.37–3	-6.39–3		5	-8.05–3	-4.97–3	3.81–3	1.99–3	-5.80–3
	10	-7.93–2	-2.01–2	2.01–2	2.77–2	-4.78–2		10	-7.57–2	-1.93–2	1.94–2	2.64–2	-4.58–2
3d <sub>3/2</sub>	1	2.61–3	3.62–3	-1.63–3	7.80–5	1.55–3	3d <sub>3/2</sub>	1	3.22–3	3.81–3	-1.63–3	-9.01–5	1.72–3
	3	-4.03–2	-1.66–3	-1.34–3	1.52–2	-1.38–2		3	-3.83–2	-1.02–3	-1.57–3	1.46–2	-1.30–2
	5	-1.05–1	-1.34–2	1.87–3	3.72–2	-3.90–2		5	-1.02–1	-1.24–2	1.69–3	3.63–2	-3.80–2
	10	-2.89–1	-4.89–2	6.98–3	9.75–2	-1.04–1		10	-2.85–1	-4.78–2	7.31–3	9.64–2	-1.04–1
3d <sub>5/2</sub>	1	7.98–3	3.10–3	5.37–4	-1.85–3	1.31–3	3d <sub>5/2</sub>	1	8.76–3	3.28–3	5.91–4	-2.07–3	1.48–3
	3	-3.09–2	-3.01–3	2.96–3	1.17–2	-1.47–2		3	-2.88–2	-2.37–3	2.82–3	1.11–2	-1.39–2
	5	-9.22–2	-1.58–2	7.74–3	3.21–2	-3.98–2		5	-8.92–2	-1.49–2	7.65–3	3.13–2	-3.89–2
	10	-2.69–1	-5.47–2	1.57–2	8.88–2	-1.05–1		10	-2.65–1	-5.36–2	1.60–2	8.78–2	-1.04–1
4s <sub>1/2</sub>	1	-1.51–3	4.83–3	1.94–3	2.93–3	-4.87–3	4s <sub>1/2</sub>	1	-8.58–4	5.32–3	1.88–3	2.85–3	-4.72–3
	3	-3.39–2	-1.01–2	7.70–3	1.11–2	-1.87–2		3	-3.43–2	-9.88–3	7.90–3	1.14–2	-1.93–2
	5	-3.71–2	-1.53–2	7.07–3	1.01–2	-1.72–2		5	-3.90–2	-1.57–2	7.56–3	1.08–2	-1.84–2
	10	-2.06–2	-1.48–2	2.11–3	2.75–3	-4.87–3		10	-2.23–2	-1.55–2	2.42–3	3.21–3	-5.63–3
4p <sub>1/2</sub>	1	-1.31–2	-2.07–3	1.38–3	4.68–3	-6.06–3	4p <sub>1/2</sub>	1	-1.29–2	-1.77–3	1.35–3	4.74–3	-6.09–3
	3	-1.23–2	-4.55–3	-5.05–4	3.00–3	-2.49–3		3	-1.32–2	-4.89–3	-3.65–4	3.26–3	-2.90–3
	5	-1.51–2	-3.21–3	-1.29–3	4.48–3	-3.18–3		5	-1.46–2	-3.35–3	-1.42–3	4.21–3	-2.79–3
	10	-7.90–2	-1.19–2	6.86–3	2.82–2	-3.51–2		10	-7.48–2	-1.12–2	6.21–3	2.67–2	-3.29–2
4p <sub>3/2</sub>	1	-1.06–2	-3.20–3	2.16–3	3.39–3	-5.55–3	4p <sub>3/2</sub>	1	-1.05–2	-3.02–3	2.12–3	3.42–3	-5.54–3
	3	-5.91–3	-5.65–3	2.07–3	5.16–4	-2.59–3		3	-6.69–3	-5.99–3	2.20–3	7.20–4	-2.92–3
	5	-7.83–3	-5.75–3	3.44–3	1.52–3	-4.96–3		5	-7.34–3	-5.86–3	3.28–3	1.25–3	-4.52–3
	10	-6.98–2	-1.92–2	1.84–2	2.39–2	-4.24–2		10	-6.62–2	-1.85–2	1.77–2	2.26–2	-4.03–2
4d <sub>3/2</sub>	1	-2.06–3	-1.08–3	1.58–5	3.96–4	-4.11–4	4d <sub>3/2</sub>	1	-2.40–3	-1.25–3	7.78–5	4.72–4	-5.50–4
	3	-2.58–2	-2.49–3	-2.77–4	9.27–3	-8.99–3		3	-2.39–2	-2.14–3	-4.25–4	8.63–3	-8.20–3
	5	-8.11–2	-1.14–2	2.68–3	2.84–2	-3.11–2		5	-7.77–2	-1.07–2	2.52–3	2.73–2	-2.99–2
	10	-2.59–1	-4.46–2	8.58–3	8.73–2	-9.59–2		10	-2.53–1	-4.33–2	8.90–3	8.57–2	-9.46–2
4d <sub>5/2</sub>	1	9.08–4	-1.35–3	1.07–3	-6.89–4	-3.76–4	4d <sub>5/2</sub>	1	6.07–4	-1.52–3	1.12–3	-6.26–4	-4.97–4
	3	-1.85–2	-3.52–3	3.13–3	6.60–3	-9.73–3		3	-1.66–2	-3.16–3	3.00–3	5.97–3	-8.98–3
	5	-6.98–2	-1.35–2	7.90–3	2.41–2	-3.20–2		5	-6.65–2	-1.27–2	7.79–3	2.31–2	-3.09–2
	10	-2.40–1	-5.00–2	1.69–2	7.92–2	-9.62–2		10	-2.34–1	-4.86–2	1.72–2	7.78–2	-9.50–2
4f <sub>5/2</sub>	1	-1.50–2	-1.39–3	-1.22–3	5.21–3	-3.99–3	4f <sub>5/2</sub>	1	-1.40–2	-1.16–3	-1.22–3	4.88–3	-3.66–3
	3	-1.00–1	-1.58–2	-3.76–3	3.30–2	-2.92–2		3	-9.76–2	-1.52–2	-3.62–3	3.22–2	-2.86–2
	5	-2.07–1	-3.57–2	-8.82–3	6.67–2	-5.79–2		5	-2.03–1	-3.47–2	-8.47–3	6.56–2	-5.71–2
	10	-4.81–1	-9.16–2	-3.16–2	1.49–1	-1.18–1		10	-4.78–1	-9.06–2	-3.01–2	1.49–1	-1.19–1
5s <sub>1/2</sub>	1	-6.52–4	4.15–3	1.46–3	2.21–3	-3.67–3	5s <sub>1/2</sub>	1	-1.36–4	4.49–3	1.39–3	2.13–3	-3.52–3
	3	-3.18–2	-9.52–3	7.20–3	1.03–2	-1.75–2		3	-3.20–2	-9.27–3	7.36–3	1.06–2	-1.79–2
	5	-3.61–2	-1.50–2	6.85–3	9.81–3	-1.67–2		5	-3.79–2	-1.53–2	7.31–3	1.05–2	-1.78–2
	10	-2.06–2	-1.48–2	2.08–3	2.72–3	-4.79–3		10	-2.22–2	-1.55–2	2.38–3	3.17–3	-5.55–3

(continued on next page)

Table 1 (continued)

Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$	Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$
5p <sub>1/2</sub>	1	-1.03–2	-1.15–3	1.32–3	3.91–3	-5.23–3	5p <sub>1/2</sub>	1	-9.93–3	-8.19–4	1.27–3	3.90–3	-5.17–3
	3	-1.22–2	-4.68–3	-2.87–4	2.96–3	-2.67–3		3	-1.31–2	-5.00–3	-1.33–4	3.22–3	-3.09–3
	5	-1.46–2	-3.48–3	-1.18–3	4.21–3	-3.03–3		5	-1.42–2	-3.64–3	-1.29–3	3.97–3	-2.68–3
	10	-7.70–2	-1.19–2	6.79–3	2.74–2	-3.42–2		10	-7.27–2	-1.11–2	6.14–3	2.59–2	-3.20–2
5p <sub>3/2</sub>	1	-8.59–3	-2.29–3	1.89–3	2.90–3	-4.79–3	5p <sub>3/2</sub>	1	-8.36–3	-2.07–3	1.84–3	2.89–3	-4.72–3
	3	-6.29–3	-5.75–3	2.08–3	6.32–4	-2.72–3		3	-7.07–3	-6.07–3	2.22–3	8.44–4	-3.06–3
	5	-7.77–3	-5.95–3	3.34–3	1.40–3	-4.74–3		5	-7.34–3	-6.07–3	3.18–3	1.14–3	-4.33–3
	10	-6.81–2	-1.90–2	1.81–2	2.32–2	-4.13–2		10	-6.44–2	-1.83–2	1.74–2	2.19–2	-3.93–2
6s <sub>1/2</sub>	1	-4.42–4	4.18–3	1.40–3	2.13–3	-3.52–3	6s <sub>1/2</sub>	1	2.35–4	4.60–3	1.31–3	2.01–3	-3.31–3
	3	-3.19–2	-9.59–3	7.21–3	1.04–2	-1.76–2		3	-3.23–2	-9.40–3	7.39–3	1.06–2	-1.80–2
	5	-3.62–2	-1.50–2	6.87–3	9.84–3	-1.67–2		5	-3.79–2	-1.53–2	7.33–3	1.05–2	-1.78–2
	10	-2.06–2	-1.49–2	2.09–3	2.73–3	-4.82–3		10	-2.23–2	-1.56–2	2.39–3	3.18–3	-5.58–3
<i>Z</i> = 61, Pm: 4f <sub>5/2</sub> <sup>5</sup> 6s <sub>1/2</sub> <sup>2</sup>							<i>Z</i> = 62, Sm: 4f <sub>5/2</sub> <sup>6</sup> 6s <sub>1/2</sub> <sup>2</sup>						
3s <sub>1/2</sub>	1	-8.61–3	6.86–3	4.82–3	7.15–3	-1.20–2	3s <sub>1/2</sub>	1	-7.96–3	7.65–3	4.85–3	7.22–3	-1.21–2
	3	-4.71–2	-1.31–2	1.10–2	1.58–2	-2.68–2		3	-4.82–2	-1.30–2	1.14–2	1.64–2	-2.77–2
	5	-4.80–2	-1.84–2	9.61–3	1.38–2	-2.34–2		5	-5.07–2	-1.90–2	1.03–2	1.47–2	-2.50–2
	10	-2.51–2	-1.65–2	3.07–3	4.07–3	-7.14–3		10	-2.74–2	-1.74–2	3.52–3	4.73–3	-8.25–3
3p <sub>1/2</sub>	1	-3.24–2	-8.60–3	1.25–3	9.77–3	-1.10–2	3p <sub>1/2</sub>	1	-3.38–2	-8.80–3	1.20–3	1.02–2	-1.14–2
	3	-1.59–2	-4.88–3	-1.50–3	4.11–3	-2.62–3		3	-1.73–2	-5.42–3	-1.39–3	4.49–3	-3.10–3
	5	-1.70–2	-2.09–3	-2.32–3	5.50–3	-3.18–3		5	-1.66–2	-2.22–3	-2.50–3	5.26–3	-2.76–3
	10	-8.24–2	-1.06–2	5.87–3	2.99–2	-3.58–2		10	-7.84–2	-9.78–3	5.22–3	2.85–2	-3.37–2
3p <sub>3/2</sub>	1	-2.39–2	-9.40–3	3.36–3	6.48–3	-9.84–3	3p <sub>3/2</sub>	1	-2.49–2	-9.67–3	3.38–3	6.79–3	-1.02–2
	3	-5.94–3	-6.06–3	2.33–3	4.18–4	-2.75–3		3	-6.94–3	-6.56–3	2.49–3	6.50–4	-3.14–3
	5	-7.32–3	-5.02–3	3.62–3	1.64–3	-5.26–3		5	-6.72–3	-5.12–3	3.45–3	1.33–3	-4.79–3
	10	-7.21–2	-1.86–2	1.87–2	2.51–2	-4.38–2		10	-6.86–2	-1.79–2	1.80–2	2.39–2	-4.19–2
3d <sub>3/2</sub>	1	3.80–3	3.99–3	-1.63–3	-2.50–4	1.88–3	3d <sub>3/2</sub>	1	4.35–3	4.16–3	-1.62–3	-4.00–4	2.02–3
	3	-3.63–2	-3.75–4	-1.80–3	1.40–2	-1.22–2		3	-3.42–2	2.64–4	-2.03–3	1.34–2	-1.14–2
	5	-9.95–2	-1.16–2	1.47–3	3.55–2	-3.69–2		5	-9.66–2	-1.07–2	1.22–3	3.46–2	-3.59–2
	10	-2.81–1	-4.66–2	7.59–3	9.54–2	-1.03–1		10	-2.77–1	-4.55–2	7.83–3	9.43–2	-1.02–1
3d <sub>5/2</sub>	1	9.50–3	3.45–3	6.53–4	-2.29–3	1.64–3	3d <sub>5/2</sub>	1	1.02–2	3.61–3	7.24–4	-2.50–3	1.78–3
	3	-2.66–2	-1.73–3	2.67–3	1.05–2	-1.32–2		3	-2.45–2	-1.09–3	2.53–3	9.86–3	-1.24–2
	5	-8.63–2	-1.40–2	7.52–3	3.04–2	-3.79–2		5	-8.34–2	-1.31–2	7.37–3	2.96–2	-3.70–2
	10	-2.61–1	-5.24–2	1.63–2	8.67–2	-1.03–1		10	-2.57–1	-5.12–2	1.66–2	8.57–2	-1.02–1
4s <sub>1/2</sub>	1	-2.16–4	5.81–3	1.81–3	2.77–3	-4.58–3	4s <sub>1/2</sub>	1	4.06–4	6.29–3	1.76–3	2.71–3	-4.46–3
	3	-3.47–2	-9.61–3	8.08–3	1.16–2	-1.97–2		3	-3.49–2	-9.28–3	8.25–3	1.19–2	-2.01–2
	5	-4.09–2	-1.61–2	8.05–3	1.16–2	-1.96–2		5	-4.28–2	-1.64–2	8.55–3	1.23–2	-2.08–2
	10	-2.42–2	-1.63–2	2.78–3	3.74–3	-6.52–3		10	-2.63–2	-1.71–2	3.19–3	4.34–3	-7.53–3
4p <sub>1/2</sub>	1	-1.27–2	-1.43–3	1.30–3	4.77–3	-6.07–3	4p <sub>1/2</sub>	1	-1.24–2	-1.05–3	1.24–3	4.78–3	-6.02–3
	3	-1.42–2	-5.23–3	-2.08–4	3.56–3	-3.35–3		3	-1.53–2	-5.59–3	-3.66–5	3.88–3	-3.85–3
	5	-1.43–2	-3.52–3	-1.52–3	4.00–3	-2.48–3		5	-1.41–2	-3.72–3	-1.61–3	3.85–3	-2.24–3
	10	-7.07–2	-1.04–2	5.57–3	2.52–2	-3.08–2		10	-6.68–2	-9.77–3	4.93–3	2.38–2	-2.87–2
4p <sub>3/2</sub>	1	-1.04–2	-2.80–3	2.07–3	3.44–3	-5.51–3	4p <sub>3/2</sub>	1	-1.02–2	-2.57–3	2.02–3	3.45–3	-5.46–3
	3	-7.54–3	-6.34–3	2.35–3	9.49–4	-3.30–3		3	-8.46–3	-6.71–3	2.51–3	1.20–3	-3.71–3
	5	-6.97–3	-6.00–3	3.13–3	1.01–3	-4.15–3		5	-6.72–3	-6.18–3	3.02–3	8.19–4	-3.84–3
	10	-6.26–2	-1.78–2	1.69–2	2.13–2	-3.82–2		10	-5.92–2	-1.72–2	1.62–2	2.01–2	-3.63–2
4d <sub>3/2</sub>	1	-2.79–3	-1.44–3	1.40–4	5.67–4	-7.07–4	4d <sub>3/2</sub>	1	-3.25–3	-1.65–3	2.02–4	6.81–4	-8.82–4
	3	-2.21–2	-1.82–3	-5.69–4	8.01–3	-7.44–3		3	-2.04–2	-1.53–3	-7.10–4	7.41–3	-6.70–3
	5	-7.45–2	-9.96–3	2.33–3	2.63–2	-2.86–2		5	-7.12–2	-9.28–3	2.12–3	2.52–2	-2.73–2
	10	-2.48–1	-4.20–2	9.16–3	8.41–2	-9.33–2		10	-2.42–1	-4.07–2	9.37–3	8.25–2	-9.19–2
4d <sub>5/2</sub>	1	2.49–4	-1.70–3	1.18–3	-5.45–4	-6.36–4	4d <sub>5/2</sub>	1	-1.62–4	-1.90–3	1.24–3	-4.49–4	-7.94–4
	3	-1.48–2	-2.81–3	2.87–3	5.36–3	-8.23–3		3	-1.31–2	-2.50–3	2.74–3	4.78–3	-7.52–3
	5	-6.32–2	-1.20–2	7.63–3	2.20–2	-2.97–2		5	-6.01–2	-1.13–2	7.47–3	2.10–2	-2.85–2
	10	-2.29–1	-4.73–2	1.75–2	7.62–2	-9.37–2		10	-2.24–1	-4.59–2	1.77–2	7.47–2	-9.24–2
4f <sub>5/2</sub>	1	-1.30–2	-9.51–4	-1.22–3	4.58–3	-3.36–3	4f <sub>5/2</sub>	1	-1.21–2	-7.64–4	-1.22–3	4.28–3	-3.07–3
	3	-9.52–2	-1.46–2	-3.50–3	3.16–2	-2.81–2		3	-9.28–2	-1.40–2	-3.40–3	3.09–2	-2.75–2
	5	-1.99–1	-3.37–2	-8.13–3	6.46–2	-5.64–2		5	-1.96–1	-3.28–2	-7.79–3	6.36–2	-5.58–2
	10	-4.74–1	-8.94–2	-2.88–2	1.48–1	-1.19–1		10	-4.70–1	-8.82–2	-2.75–2	1.47–1	-1.20–1

Table 1 (continued)

Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$	Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$
5s <sub>1/2</sub>	1	3.53–4	4.80–3	1.32–3	2.04–3	−3.37–3	5s <sub>1/2</sub>	1	8.11–4	5.10–3	1.26–3	1.97–3	−3.23–3
	3	−3.22–2	−8.95–3	7.49–3	1.08–2	−1.83–2		3	−3.22–2	−8.58–3	7.60–3	1.10–2	−1.86–2
	5	−3.97–2	−1.57–2	7.77–3	1.11–2	−1.89–2		5	−4.14–2	−1.60–2	8.22–3	1.18–2	−2.00–2
	10	−2.41–2	−1.63–2	2.74–3	3.69–3	−6.43–3		10	−2.62–2	−1.70–2	3.14–3	4.28–3	−7.42–3
5p <sub>1/2</sub>	1	−9.50–3	−4.61–4	1.21–3	3.86–3	−5.07–3	5p <sub>1/2</sub>	1	−9.02–3	−7.92–5	1.14–3	3.80–3	−4.95–3
	3	−1.41–2	−5.31–3	3.83–5	3.51–3	−3.55–3		3	−1.51–2	−5.63–3	2.22–4	3.83–3	−4.06–3
	5	−1.40–2	−3.82–3	−1.38–3	3.78–3	−2.40–3		5	−1.39–2	−4.04–3	−1.45–3	3.64–3	−2.19–3
	10	−6.87–2	−1.05–2	5.50–3	2.44–2	−2.99–2		10	−6.47–2	−9.82–3	4.87–3	2.29–2	−2.78–2
5p <sub>3/2</sub>	1	−8.05–3	−1.82–3	1.77–3	2.85–3	−4.62–3	5p <sub>3/2</sub>	1	−7.69–3	−1.55–3	1.69–3	2.80–3	−4.49–3
	3	−7.93–3	−6.40–3	2.37–3	1.08–3	−3.45–3		3	−8.81–3	−6.73–3	2.52–3	1.34–3	−3.86–3
	5	−7.02–3	−6.21–3	3.04–3	9.30–4	−3.97–3		5	−6.83–3	−6.40–3	2.94–3	7.60–4	−3.70–3
	10	−6.09–2	−1.77–2	1.66–2	2.06–2	−3.72–2		10	−5.75–2	−1.71–2	1.59–2	1.93–2	−3.52–2
6s <sub>1/2</sub>	1	6.90–4	4.91–3	1.25–3	1.94–3	−3.18–3	6s <sub>1/2</sub>	1	1.17–3	5.23–3	1.19–3	1.86–3	−3.05–3
	3	−3.21–2	−8.92–3	7.48–3	1.08–2	−1.83–2		3	−3.20–2	−8.49–3	7.58–3	1.09–2	−1.85–2
	5	−3.97–2	−1.57–2	7.79–3	1.12–2	−1.90–2		5	−4.14–2	−1.60–2	8.24–3	1.18–2	−2.01–2
	10	−2.42–2	−1.63–2	2.75–3	3.71–3	−6.46–3		10	−2.63–2	−1.71–2	3.16–3	4.30–3	−7.46–3
$Z = 63, \text{Eu: } 4f_{5/2}^6 4f_{7/2}^1 6s_{1/2}^2$							$Z = 64, \text{Gd: } 4f_{5/2}^6 4f_{7/2}^1 5d_{3/2}^1 6s_{1/2}^2$						
3s <sub>1/2</sub>	1	−7.32–3	8.46–3	4.88–3	7.29–3	−1.22–2	3s <sub>1/2</sub>	1	−6.89–3	9.14–3	4.94–3	7.40–3	−1.23–2
	3	−4.93–2	−1.29–2	1.17–2	1.69–2	−2.87–2		3	−5.02–2	−1.26–2	1.21–2	1.74–2	−2.95–2
	5	−5.33–2	−1.96–2	1.09–2	1.57–2	−2.66–2		5	−5.58–2	−2.00–2	1.16–2	1.66–2	−2.82–2
	10	−3.00–2	−1.83–2	4.03–3	5.46–3	−9.49–3		10	−3.26–2	−1.93–2	4.58–3	6.26–3	−1.08–2
3p <sub>1/2</sub>	1	−3.51–2	−8.96–3	1.13–3	1.07–2	−1.18–2	3p <sub>1/2</sub>	1	−3.63–2	−9.10–3	1.05–3	1.11–2	−1.21–2
	3	−1.89–2	−6.00–3	−1.26–3	4.91–3	−3.65–3		3	−2.05–2	−6.56–3	−1.13–3	5.33–3	−4.21–3
	5	−1.64–2	−2.39–3	−2.66–3	5.07–3	−2.41–3		5	−1.64–2	−2.61–3	−2.79–3	4.94–3	−2.15–3
	10	−7.45–2	−9.03–3	4.56–3	2.71–2	−3.17–2		10	−7.08–2	−8.33–3	3.92–3	2.58–2	−2.97–2
3p <sub>3/2</sub>	1	−2.59–2	−9.92–3	3.37–3	7.08–3	−1.04–2	3p <sub>3/2</sub>	1	−2.67–2	−1.01–2	3.36–3	7.30–3	−1.07–2
	3	−8.05–3	−7.10–3	2.67–3	9.18–4	−3.59–3		3	−9.17–3	−7.61–3	2.86–3	1.19–3	−4.05–3
	5	−6.26–3	−5.26–3	3.32–3	1.06–3	−4.38–3		5	−5.94–3	−5.42–3	3.21–3	8.49–4	−4.06–3
	10	−6.52–2	−1.72–2	1.73–2	2.26–2	−3.99–2		10	−6.19–2	−1.65–2	1.66–2	2.15–2	−3.80–2
3d <sub>3/2</sub>	1	4.85–3	4.31–3	−1.60–3	−5.38–4	2.14–3	3d <sub>3/2</sub>	1	5.34–3	4.48–3	−1.59–3	−6.62–4	2.25–3
	3	−3.23–2	8.61–4	−2.28–3	1.28–2	−1.05–2		3	−3.03–2	1.51–3	−2.49–3	1.22–2	−9.73–3
	5	−9.37–2	−9.77–3	9.48–4	3.38–2	−3.47–2		5	−9.09–2	−8.89–3	6.79–4	3.29–2	−3.36–2
	10	−2.73–1	−4.43–2	8.02–3	9.31–2	−1.01–1		10	−2.69–1	−4.31–2	8.17–3	9.20–2	−1.00–1
3d <sub>5/2</sub>	1	1.09–2	3.74–3	8.00–4	−2.70–3	1.90–3	3d <sub>5/2</sub>	1	1.15–2	3.90–3	8.71–4	−2.88–3	2.01–3
	3	−2.24–2	−4.86–4	2.38–3	9.25–3	−1.16–2		3	−2.03–2	1.66–4	2.26–3	8.63–3	−1.09–2
	5	−8.04–2	−1.22–2	7.21–3	2.87–2	−3.59–2		5	−7.75–2	−1.13–2	7.04–3	2.79–2	−3.49–2
	10	−2.53–1	−5.00–2	1.68–2	8.46–2	−1.01–1		10	−2.49–1	−4.88–2	1.70–2	8.35–2	−1.01–1
4s <sub>1/2</sub>	1	9.95–4	6.76–3	1.70–3	2.65–3	−4.35–3	4s <sub>1/2</sub>	1	1.42–3	7.11–3	1.67–3	2.61–3	−4.28–3
	3	−3.50–2	−8.89–3	8.40–3	1.21–2	−2.05–2		3	−3.49–2	−8.47–3	8.50–3	1.23–2	−2.08–2
	5	−4.47–2	−1.67–2	9.03–3	1.30–2	−2.20–2		5	−4.63–2	−1.69–2	9.48–3	1.36–2	−2.31–2
	10	−2.86–2	−1.79–2	3.65–3	5.00–3	−8.65–3		10	−3.09–2	−1.87–2	4.14–3	5.71–3	−9.85–3
4p <sub>1/2</sub>	1	−1.20–2	−6.45–4	1.17–3	4.79–3	−5.96–3	4p <sub>1/2</sub>	1	−1.16–2	−3.00–4	1.11–3	4.76–3	−5.86–3
	3	−1.65–2	−5.95–3	1.48–4	4.24–3	−4.39–3		3	−1.75–2	−6.25–3	3.29–4	4.58–3	−4.91–3
	5	−1.42–2	−3.97–3	−1.66–3	3.74–3	−2.08–3		5	−1.43–2	−4.22–3	−1.69–3	3.68–3	−1.99–3
	10	−6.30–2	−9.16–3	4.30–3	2.24–2	−2.67–2		10	−5.94–2	−8.59–3	3.70–3	2.11–2	−2.48–2
4p <sub>3/2</sub>	1	−9.87–3	−2.30–3	1.95–3	3.42–3	−5.37–3	4p <sub>3/2</sub>	1	−9.59–3	−2.08–3	1.88–3	3.38–3	−5.26–3
	3	−9.44–3	−7.07–3	2.68–3	1.48–3	−4.17–3		3	−1.04–2	−7.40–3	2.85–3	1.75–3	−4.60–3
	5	−6.59–3	−6.39–3	2.93–3	6.68–4	−3.60–3		5	−6.59–3	−6.61–3	2.87–3	5.66–4	−3.43–3
	10	−5.59–2	−1.66–2	1.55–2	1.88–2	−3.43–2		10	−5.28–2	−1.60–2	1.48–2	1.76–2	−3.24–2
4d <sub>3/2</sub>	1	−3.74–3	−1.85–3	2.62–4	8.08–4	−1.07–3	4d <sub>3/2</sub>	1	−4.23–3	−2.05–3	3.05–4	9.35–4	−1.24–3
	3	−1.88–2	−1.27–3	−8.49–4	6.84–3	−5.99–3		3	−1.73–2	−1.02–3	−9.64–4	6.30–3	−5.34–3
	5	−6.81–2	−8.61–3	1.90–3	2.42–2	−2.61–2		5	−6.50–2	−7.97–3	1.68–3	2.31–2	−2.48–2
	10	−2.37–1	−3.94–2	9.52–3	8.09–2	−9.04–2		10	−2.31–1	−3.81–2	9.62–3	7.92–2	−8.89–2
4d <sub>5/2</sub>	1	−6.11–4	−2.11–3	1.30–3	−3.38–4	−9.64–4	4d <sub>5/2</sub>	1	−1.08–3	−2.29–3	1.34–3	−2.20–4	−1.12–3
	3	−1.14–2	−2.22–3	2.62–3	4.21–3	−6.83–3		3	−9.88–3	−1.94–3	2.51–3	3.68–3	−6.19–3
	5	−5.69–2	−1.06–2	7.30–3	2.00–2	−2.73–2		5	−5.39–2	−9.88–3	7.12–3	1.90–2	−2.61–2
	10	−2.19–1	−4.46–2	1.79–2	7.32–2	−9.10–2		10	−2.13–1	−4.32–2	1.80–2	7.16–2	−8.96–2

(continued on next page)

Table 1 (continued)

Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$	Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$	
$4f_{5/2}$	1	-1.11–2	-5.69–4	-1.20–3	3.96–3	-2.77–3	$4f_{5/2}$	1	-1.02–2	-4.00–4	-1.17–3	3.68–3	-2.52–3	
	3	-9.02–2	-1.33–2	-3.30–3	3.01–2	-2.68–2		3	-8.75–2	-1.26–2	-3.21–3	2.93–2	-2.61–2	
	5	-1.92–1	-3.19–2	-7.46–3	6.25–2	-5.50–2		5	-1.88–1	-3.10–2	-7.13–3	6.14–2	-5.43–2	
	10	-4.66–1	-8.68–2	-2.62–2	1.46–1	-1.20–1		10	-4.61–1	-8.54–2	-2.50–2	1.45–1	-1.20–1	
$4f_{7/2}$	1	-8.51–3	-9.29–4	-1.58–4	3.00–3	-2.84–3	$4f_{7/2}$	1	-7.64–3	-7.55–4	-1.41–4	2.73–3	-2.59–3	
	3	-8.29–2	-1.46–2	2.54–6	2.73–2	-2.73–2		3	-8.02–2	-1.39–2	9.19–5	2.65–2	-2.66–2	
	5	-1.80–1	-3.44–2	-2.51–3	5.80–2	-5.54–2		5	-1.77–1	-3.34–2	-2.16–3	5.69–2	-5.48–2	
	10	-4.48–1	-9.27–2	-1.93–2	1.38–1	-1.19–1		10	-4.43–1	-9.13–2	-1.81–2	1.37–1	-1.19–1	
$5s_{1/2}$	1	1.23–3	5.39–3	1.21–3	1.91–3	-3.12–3	$5s_{1/2}$	1	1.52–3	5.60–3	1.18–3	1.87–3	-3.05–3	
	3	-3.21–2	-8.17–3	7.71–3	1.11–2	-1.88–2		3	-3.20–2	-7.74–3	7.77–3	1.12–2	-1.90–2	
	5	-4.30–2	-1.62–2	8.67–3	1.25–2	-2.11–2		5	-4.45–2	-1.64–2	9.08–3	1.31–2	-2.21–2	
	10	-2.84–2	-1.78–2	3.59–3	4.93–3	-8.52–3		10	-3.07–2	-1.87–2	4.06–3	5.63–3	-9.69–3	
$5p_{1/2}$	1	-8.48–3	3.24–4	1.07–3	3.74–3	-4.80–3	$5p_{1/2}$	1	-7.99–3	6.59–4	1.01–3	3.66–3	-4.67–3	
	3	-1.62–2	-5.94–3	4.18–4	4.18–3	-4.59–3		3	-1.72–2	-6.21–3	6.13–4	4.50–3	-5.12–3	
	5	-1.39–2	-4.28–3	-1.48–3	3.55–3	-2.06–3		5	-1.41–2	-4.55–3	-1.49–3	3.51–3	-2.02–3	
	10	-6.10–2	-9.23–3	4.25–3	2.16–2	-2.58–2		10	-5.75–2	-8.71–3	3.66–3	2.02–2	-2.39–2	
$5p_{3/2}$	1	-7.29–3	-1.27–3	1.61–3	2.73–3	-4.34–3	$5p_{3/2}$	1	-6.93–3	-1.04–3	1.54–3	2.66–3	-4.20–3	
	3	-9.75–3	-7.06–3	2.70–3	1.62–3	-4.31–3		3	-1.06–2	-7.36–3	2.87–3	1.88–3	-4.75–3	
	5	-6.76–3	-6.61–3	2.86–3	6.31–4	-3.49–3		5	-6.82–3	-6.85–3	2.80–3	5.51–4	-3.36–3	
	10	-5.42–2	-1.65–2	1.51–2	1.81–2	-3.33–2		10	-5.12–2	-1.60–2	1.44–2	1.70–2	-3.14–2	
$6s_{1/2}$	1	1.54–3	5.51–3	1.15–3	1.82–3	-2.97–3	$5d_{3/2}$	1	-4.60–3	-2.20–3	5.33–4	1.07–3	-1.60–3	
	3	-3.17–2	-7.94–3	7.65–3	1.10–2	-1.87–2		3	-1.59–2	-1.35–3	-8.12–4	5.65–3	-4.83–3	
	5	-4.31–2	-1.62–2	8.69–3	1.25–2	-2.12–2		5	-6.22–2	-7.96–3	1.74–3	2.20–2	-2.38–2	
	10	-2.85–2	-1.79–2	3.60–3	4.96–3	-8.57–3		10	-2.27–1	-3.75–2	9.83–3	7.77–2	-8.75–2	
$Z = 65$ , Tb: $4f_{5/2}^6 4f_{7/2}^3 6s_{1/2}^2$								$Z = 66$ , Dy: $4f_{5/2}^6 4f_{7/2}^4 6s_{1/2}^2$						
	3s <sub>1/2</sub>	1	-6.04–3	1.02–2	4.97–3	7.48–3	-1.25–2	3p <sub>1/2</sub>	1	-3.88–2	-9.21–3	7.86–4	1.20–2	-1.28–2
	3	-5.11–2	-1.23–2	1.25–2	1.80–2	-3.05–2		3	-2.44–2	-7.92–3	-7.86–4	6.44–3	-5.65–3	
	5	-5.86–2	-2.05–2	1.23–2	1.77–2	-3.00–2		5	-1.68–2	-3.22–3	-2.99–3	4.83–3	-1.84–3	
$3p_{1/2}$	10	-3.57–2	-2.04–2	5.21–3	7.18–3	-1.24–2		10	-6.36–2	-7.00–3	2.60–3	2.32–2	-2.58–2	
	1	-3.77–2	-9.18–3	9.25–4	1.16–2	-1.25–2	3p <sub>3/2</sub>	1	-2.85–2	-1.05–2	3.24–3	7.84–3	-1.11–2	
	3	-2.24–2	-7.25–3	-9.59–4	5.88–3	-4.93–3		3	-1.20–2	-8.89–3	3.33–3	1.92–3	-5.25–3	
	5	-1.65–2	-2.90–3	-2.91–3	4.86–3	-1.95–3		5	-5.67–3	-5.93–3	3.07–3	5.08–4	-3.58–3	
$3p_{3/2}$	10	-6.71–2	-7.64–3	3.25–3	2.45–2	-2.77–2		10	-5.54–2	-1.53–2	1.52–2	1.91–2	-3.43–2	
	1	-2.77–2	-1.03–2	3.31–3	7.61–3	-1.09–2	3d <sub>3/2</sub>	1	6.20–3	4.70–3	-1.51–3	-9.02–4	2.41–3	
	3	-1.06–2	-8.26–3	3.10–3	1.55–3	-4.65–3		3	-2.63–2	2.75–3	-2.99–3	1.10–2	-8.05–3	
	5	-5.73–3	-5.67–3	3.13–3	6.51–4	-3.78–3		5	-8.50–2	-7.05–3	3.93–5	3.12–2	-3.12–2	
$3d_{3/2}$	10	-5.86–2	-1.59–2	1.59–2	2.02–2	-3.61–2		10	-2.61–1	-4.07–2	8.32–3	8.97–2	-9.80–2	
	1	5.79–3	4.59–3	-1.55–3	-7.91–4	2.34–3	3d <sub>5/2</sub>	1	1.28–2	4.09–3	1.08–3	-3.27–3	2.19–3	
	3	-2.83–2	2.12–3	-2.75–3	1.16–2	-8.88–3		3	-1.60–2	1.41–3	1.97–3	7.35–3	-9.33–3	
	5	-8.79–2	-7.96–3	3.58–4	3.21–2	-3.24–2		5	-7.14–2	-9.43–3	6.66–3	2.61–2	-3.28–2	
$3d_{5/2}$	10	-2.65–1	-4.19–2	8.27–3	9.09–2	-9.91–2		10	-2.41–1	-4.63–2	1.73–2	8.14–2	-9.86–2	
	1	1.22–2	3.99–3	9.80–4	-3.09–3	2.11–3	4s <sub>1/2</sub>	1	2.61–3	8.21–3	1.61–3	2.56–3	-4.17–3	
	3	-1.81–2	7.80–4	2.11–3	7.99–3	-1.01–2		3	-3.47–2	-7.38–3	8.74–3	1.27–2	-2.14–2	
	5	-7.44–2	-1.03–2	6.86–3	2.70–2	-3.39–2		5	-4.98–2	-1.73–2	1.05–2	1.51–2	-2.56–2	
$4s_{1/2}$	10	-2.45–1	-4.76–2	1.72–2	8.25–2	-9.96–2		10	-3.64–2	-2.05–2	5.29–3	7.39–3	-1.27–2	
	1	2.10–3	7.73–3	1.63–3	2.58–3	-4.21–3	4p <sub>1/2</sub>	1	-1.05–2	8.05–4	9.25–4	4.71–3	-5.64–3	
	3	-3.49–2	-7.95–3	8.65–3	1.25–2	-2.12–2		3	-2.02–2	-6.98–3	7.69–4	5.46–3	-6.23–3	
	5	-4.82–2	-1.72–2	1.00–2	1.44–2	-2.44–2		5	-1.51–2	-4.88–3	-1.68–3	3.73–3	-2.05–3	
$4p_{1/2}$	10	-3.36–2	-1.96–2	4.70–3	6.54–3	-1.12–2		10	-5.27–2	-7.61–3	2.50–3	1.85–2	-2.10–2	
	1	-1.10–2	2.85–4	1.01–3	4.73–3	-5.74–3	4p <sub>3/2</sub>	1	-8.65–3	-1.35–3	1.69–3	3.26–3	-4.95–3	
	3	-1.89–2	-6.63–3	5.51–4	5.02–3	-5.57–3		3	-1.26–2	-8.19–3	3.28–3	2.42–3	-5.70–3	
	5	-1.46–2	-4.54–3	-1.70–3	3.68–3	-1.98–3		5	-6.93–3	-7.19–3	2.83–3	4.61–4	-3.29–3	
$4p_{3/2}$	10	-5.59–2	-8.07–3	3.08–3	1.98–2	-2.28–2		10	-4.68–2	-1.51–2	1.34–2	1.53–2	-2.87–2	

Table 1 (continued)

Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$	Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$
4p <sub>3/2</sub>	1	-9.13–3	-1.69–3	1.79–3	3.33–3	-5.12–3	4d <sub>3/2</sub>	1	-5.52–3	-2.53–3	4.14–4	1.28–3	-1.70–3
	3	-1.15–2	-7.82–3	3.07–3	2.09–3	-5.16–3		3	-1.44–2	-6.27–4	-1.21–3	5.26–3	-4.05–3
	5	-6.71–3	-6.90–3	2.83–3	4.90–4	-3.32–3		5	-5.89–2	-6.70–3	1.16–3	2.11–2	-2.23–2
	10	-4.97–2	-1.55–2	1.41–2	1.65–2	-3.05–2		10	-2.21–1	-3.56–2	9.67–3	7.60–2	-8.56–2
4d <sub>5/2</sub>	1	-4.89–3	-2.30–3	3.69–4	1.11–3	-1.48–3	4d <sub>5/2</sub>	1	-2.23–3	-2.78–3	1.47–3	7.62–5	-1.55–3
	3	-1.58–2	-8.13–4	-1.10–3	5.76–3	-4.66–3		3	-6.92–3	-1.51–3	2.29–3	2.62–3	-4.92–3
	5	-6.19–2	-7.32–3	1.42–3	2.21–2	-2.35–2		5	-4.78–2	-8.54–3	6.73–3	1.71–2	-2.38–2
	10	-2.26–1	-3.68–2	9.67–3	7.76–2	-8.73–2		10	-2.03–1	-4.06–2	1.81–2	6.85–2	-8.67–2
4d <sub>7/2</sub>	1	-1.66–3	-2.55–3	1.42–3	-7.38–5	-1.35–3	4f <sub>5/2</sub>	1	-8.72–3	-1.82–4	-1.14–3	3.19–3	-2.05–3
	3	-8.35–3	-1.72–3	2.39–3	3.13–3	-5.52–3		3	-8.27–2	-1.14–2	-3.14–3	2.79–2	-2.48–2
	5	-5.08–2	-9.20–3	6.93–3	1.80–2	-2.50–2		5	-1.82–1	-2.93–2	-6.60–3	5.96–2	-5.30–2
	10	-2.08–1	-4.19–2	1.81–2	7.01–2	-8.82–2		10	-4.51–1	-8.24–2	-2.30–2	1.43–1	-1.20–1
4f <sub>5/2</sub>	1	-9.45–3	-2.93–4	-1.16–3	3.43–3	-2.27–3	4f <sub>7/2</sub>	1	-6.14–3	-5.39–4	-1.03–4	2.22–3	-2.12–3
	3	-8.52–2	-1.20–2	-3.18–3	2.86–2	-2.55–2		3	-7.55–2	-1.27–2	1.86–4	2.52–2	-2.54–2
	5	-1.85–1	-3.02–2	-6.87–3	6.05–2	-5.37–2		5	-1.70–1	-3.17–2	-1.53–3	5.51–2	-5.36–2
	10	-4.56–1	-8.39–2	-2.40–2	1.44–1	-1.20–1		10	-4.34–1	-8.83–2	-1.60–2	1.35–1	-1.19–1
4f <sub>7/2</sub>	1	-6.88–3	-6.51–4	-1.26–4	2.47–3	-2.34–3	5s <sub>1/2</sub>	1	2.28–3	6.20–3	1.10–3	1.79–3	-2.89–3
	3	-7.80–2	-1.33–2	1.42–4	2.59–2	-2.60–2		3	-3.12–2	-6.58–3	7.88–3	1.14–2	-1.93–2
	5	-1.74–1	-3.26–2	-1.84–3	5.61–2	-5.42–2		5	-4.75–2	-1.66–2	9.95–3	1.43–2	-2.43–2
	10	-4.39–1	-8.98–2	-1.70–2	1.36–1	-1.19–1		10	-3.60–2	-2.04–2	5.18–3	7.26–3	-1.24–2
5s <sub>1/2</sub>	1	1.97–3	5.95–3	1.13–3	1.82–3	-2.95–3	5p <sub>1/2</sub>	1	-6.56–3	1.65–3	8.21–4	3.44–3	-4.27–3
	3	-3.17–2	-7.16–3	7.84–3	1.14–2	-1.92–2		3	-1.95–2	-6.76–3	1.06–3	5.30–3	-6.36–3
	5	-4.61–2	-1.65–2	9.53–3	1.37–2	-2.33–2		5	-1.49–2	-5.20–3	-1.44–3	3.59–3	-2.16–3
	10	-3.33–2	-1.95–2	4.61–3	6.43–3	-1.10–2		10	-5.08–2	-7.78–3	2.48–3	1.77–2	-2.02–2
5p <sub>1/2</sub>	1	-7.24–3	1.19–3	9.07–4	3.55–3	-4.46–3	5p <sub>3/2</sub>	1	-5.79–3	-3.32–4	1.33–3	2.45–3	-3.78–3
	3	-1.84–2	-6.50–3	8.37–4	4.91–3	-5.75–3		3	-1.27–2	-8.00–3	3.27–3	2.52–3	-5.79–3
	5	-1.44–2	-4.85–3	-1.48–3	3.52–3	-2.04–3		5	-7.29–3	-7.42–3	2.78–3	5.01–4	-3.28–3
	10	-5.40–2	-8.22–3	3.05–3	1.89–2	-2.20–2		10	-4.53–2	-1.51–2	1.30–2	1.47–2	-2.77–2
5p <sub>3/2</sub>	1	-6.34–3	-6.56–4	1.43–3	2.56–3	-3.99–3	6s <sub>1/2</sub>	1	2.20–3	6.03–3	1.08–3	1.75–3	-2.83–3
	3	-1.17–2	-7.70–3	3.07–3	2.21–3	-5.28–3		3	-3.10–2	-6.50–3	7.83–3	1.14–2	-1.92–2
	5	-7.01–3	-7.13–3	2.77–3	5.06–4	-3.28–3		5	-4.75–2	-1.66–2	9.97–3	1.44–2	-2.43–2
	10	-4.81–2	-1.55–2	1.37–2	1.58–2	-2.95–2		10	-3.61–2	-2.05–2	5.20–3	7.29–3	-1.25–2
6s <sub>1/2</sub>	1	2.04–3	5.90–3	1.10–3	1.76–3	-2.86–3							
	3	-3.12–2	-6.95–3	7.77–3	1.13–2	-1.90–2							
	5	-4.62–2	-1.65–2	9.56–3	1.38–2	-2.33–2							
	10	-3.34–2	-1.96–2	4.63–3	6.46–3	-1.11–2							
<i>Z</i> = 67, Ho: 4f <sub>5/2</sub> <sup>6</sup> 4f <sub>7/2</sub> <sup>5</sup> 6s <sub>1/2</sub> <sup>2</sup>							<i>Z</i> = 68, Er: 4f <sub>5/2</sub> <sup>6</sup> 4f <sub>7/2</sub> <sup>6</sup> 6s <sub>1/2</sub> <sup>2</sup>						
3p <sub>1/2</sub>	1	-3.98–2	-9.19–3	6.23–4	1.24–2	-1.30–2	3p <sub>3/2</sub>	1	-2.98–2	-1.07–2	3.05–3	8.24–3	-1.13–2
	3	-2.65–2	-8.62–3	-5.99–4	7.03–3	-6.43–3		3	-1.52–2	-1.02–2	3.85–3	2.74–3	-6.60–3
	5	-1.73–2	-3.61–3	-3.05–3	4.87–3	-1.82–3		5	-5.98–3	-6.62–3	3.05–3	3.56–4	-3.41–3
	10	-6.03–2	-6.40–3	1.97–3	2.19–2	-2.39–2		10	-4.94–2	-1.43–2	1.39–2	1.68–2	-3.07–2
3p <sub>3/2</sub>	1	-2.92–2	-1.06–2	3.16–3	8.05–3	-1.12–2	3d <sub>3/2</sub>	1	6.92–3	4.89–3	-1.42–3	-1.10–3	2.51–3
	3	-1.35–2	-9.55–3	3.58–3	2.32–3	-5.90–3		3	-2.24–2	3.97–3	-3.45–3	9.86–3	-6.41–3
	5	-5.77–3	-6.26–3	3.04–3	4.12–4	-3.46–3		5	-7.96–2	-5.38–3	-6.85–4	2.95–2	-2.88–2
	10	-5.23–2	-1.48–2	1.45–2	1.79–2	-3.25–2		10	-2.52–1	-3.82–2	8.28–3	8.73–2	-9.56–2
3d <sub>3/2</sub>	1	6.58–3	4.80–3	-1.47–3	-1.00–3	2.47–3	3d <sub>5/2</sub>	1	1.39–2	4.25–3	1.31–3	-3.60–3	2.30–3
	3	-2.44–2	3.36–3	-3.22–3	1.04–2	-7.22–3		3	-1.17–2	2.64–3	1.72–3	6.09–3	-7.81–3
	5	-8.25–2	-6.29–3	-3.40–4	3.04–2	-3.01–2		5	-6.57–2	-7.73–3	6.21–3	2.44–2	-3.06–2
	10	-2.57–1	-3.95–2	8.32–3	8.85–2	-9.69–2		10	-2.33–1	-4.38–2	1.74–2	7.91–2	-9.65–2
3d <sub>5/2</sub>	1	1.34–2	4.17–3	1.19–3	-3.44–3	2.25–3	4s <sub>1/2</sub>	1	3.49–3	9.10–3	1.58–3	2.56–3	-4.14–3
	3	-1.39–2	2.02–3	1.84–3	6.72–3	-8.56–3		3	-3.39–2	-6.08–3	8.86–3	1.29–2	-2.18–2
	5	-6.87–2	-8.65–3	6.41–3	2.53–2	-3.17–2		5	-5.29–2	-1.74–2	1.14–2	1.64–2	-2.78–2
	10	-2.37–1	-4.51–2	1.74–2	8.02–2	-9.76–2		10	-4.22–2	-2.24–2	6.57–3	9.26–3	-1.58–2
4s <sub>1/2</sub>	1	3.08–3	8.68–3	1.59–3	2.56–3	-4.15–3	4p <sub>1/2</sub>	1	-9.19–3	1.95–3	7.32–4	4.60–3	-5.33–3
	3	-3.44–2	-6.77–3	8.82–3	1.28–2	-2.17–2		3	-2.29–2	-7.62–3	1.23–3	6.38–3	-7.60–3
	5	-5.15–2	-1.75–2	1.10–2	1.58–2	-2.68–2		5	-1.64–2	-5.65–3	-1.56–3	4.00–3	-2.44–3
	10	-3.93–2	-2.14–2	5.91–3	8.31–3	-1.42–2		10	-4.67–2	-6.84–3	1.39–3	1.62–2	-1.76–2

(continued on next page)

Table 1 (continued)

Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$	Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$		
4p <sub>1/2</sub>	1	-9.89–3	1.36–3	8.31–4	4.67–3	-5.50–3	4p <sub>3/2</sub>	1	-7.55–3	-6.05–4	1.50–3	3.08–3	-4.58–3		
	3	-2.16–2	-7.31–3	9.95–4	5.91–3	-6.91–3		3	-1.49–2	-8.92–3	3.72–3	3.12–3	-6.84–3		
	5	-1.57–2	-5.27–3	-1.63–3	3.85–3	-2.21–3		5	-7.78–3	-7.89–3	2.90–3	5.35–4	-3.43–3		
	10	-4.96–2	-7.20–3	1.93–3	1.74–2	-1.93–2		10	-4.14–2	-1.43–2	1.21–2	1.32–2	-2.53–2		
4p <sub>3/2</sub>	1	-8.13–3	-9.86–4	1.60–3	3.18–3	-4.77–3	4d <sub>3/2</sub>	1	-6.89–3	-2.99–3	4.84–4	1.66–3	-2.14–3		
	3	-1.37–2	-8.56–3	3.50–3	2.76–3	-6.26–3		3	-1.19–2	-3.44–4	-1.40–3	4.33–3	-2.94–3		
	5	-7.32–3	-7.54–3	2.85–3	4.83–4	-3.33–3		5	-5.33–2	-5.60–3	6.02–4	1.92–2	-1.98–2		
	10	-4.40–2	-1.47–2	1.27–2	1.43–2	-2.70–2		10	-2.10–1	-3.31–2	9.54–3	7.27–2	-8.22–2		
4d <sub>3/2</sub>	1	-6.19–3	-2.76–3	4.53–4	1.46–3	-1.92–3	4d <sub>5/2</sub>	1	-3.47–3	-3.24–3	1.57–3	4.05–4	-1.97–3		
	3	-1.31–2	-4.70–4	-1.31–3	4.78–3	-3.47–3		3	-4.32–3	-1.18–3	2.12–3	1.68–3	-3.80–3		
	5	-5.62–2	-6.18–3	8.69–4	2.02–2	-2.10–2		5	-4.22–2	-7.38–3	6.29–3	1.52–2	-2.15–2		
	10	-2.15–1	-3.43–2	9.62–3	7.43–2	-8.39–2		10	-1.92–1	-3.80–2	1.81–2	6.54–2	-8.35–2		
4d <sub>5/2</sub>	1	-2.84–3	-3.01–3	1.52–3	2.36–4	-1.76–3	4f <sub>5/2</sub>	1	-7.41–3	-7.44–6	-1.08–3	2.74–3	-1.67–3		
	3	-5.57–3	-1.33–3	2.20–3	2.14–3	-4.34–3		3	-7.77–2	-1.01–2	-3.12–3	2.64–2	-2.33–2		
	5	-4.51–2	-8.00–3	6.49–3	1.61–2	-2.26–2		5	-1.75–1	-2.75–2	-6.09–3	5.76–2	-5.15–2		
	10	-1.98–1	-3.93–2	1.81–2	6.70–2	-8.51–2		10	-4.41–1	-7.93–2	-2.12–2	1.40–1	-1.19–1		
4f <sub>5/2</sub>	1	-8.04–3	-8.71–5	-1.11–3	2.96–3	-1.85–3	4f <sub>7/2</sub>	1	-4.81–3	-3.63–4	-4.85–5	1.77–3	-1.72–3		
	3	-8.02–2	-1.07–2	-3.12–3	2.72–2	-2.40–2		3	-7.06–2	-1.14–2	2.31–4	2.37–2	-2.40–2		
	5	-1.78–1	-2.84–2	-6.32–3	5.86–2	-5.23–2		5	-1.64–1	-2.99–2	-9.42–4	5.33–2	-5.23–2		
	10	-4.46–1	-8.09–2	-2.21–2	1.42–1	-1.20–1		10	-4.23–1	-8.52–2	-1.42–2	1.32–1	-1.18–1		
4f <sub>7/2</sub>	1	-5.45–3	-4.44–4	-7.74–5	1.99–3	-1.91–3	5s <sub>1/2</sub>	1	2.79–3	6.65–3	1.07–3	1.76–3	-2.83–3		
	3	-7.30–2	-1.20–2	2.16–4	2.45–2	-2.47–2		3	-3.01–2	-5.27–3	7.89–3	1.15–2	-1.94–2		
	5	-1.67–1	-3.08–2	-1.21–3	5.42–2	-5.30–2		5	-5.00–2	-1.66–2	1.07–2	1.55–2	-2.63–2		
	10	-4.29–1	-8.68–2	-1.51–2	1.34–1	-1.19–1		10	-4.16–2	-2.22–2	6.43–3	9.08–3	-1.55–2		
5s <sub>1/2</sub>	1	2.56–3	6.43–3	1.08–3	1.77–3	-2.85–3	5p <sub>1/2</sub>	1	-5.09–3	2.59–3	6.51–4	3.20–3	-3.85–3		
	3	-3.07–2	-5.95–3	7.89–3	1.15–2	-1.94–2		3	-2.17–2	-7.20–3	1.51–3	6.11–3	-7.62–3		
	5	-4.88–2	-1.66–2	1.04–2	1.50–2	-2.53–2		5	-1.62–2	-5.91–3	-1.27–3	3.86–3	-2.59–3		
	10	-3.87–2	-2.13–2	5.79–3	8.14–3	-1.39–2		10	-4.49–2	-7.08–3	1.39–3	1.54–2	-1.68–2		
5p <sub>1/2</sub>	1	-5.83–3	2.11–3	7.36–4	3.33–3	-4.06–3	5p <sub>3/2</sub>	1	-4.62–3	3.35–4	1.14–3	2.21–3	-3.36–3		
	3	-2.06–2	-6.99–3	1.28–3	5.70–3	-6.98–3		3	-1.47–2	-8.58–3	3.67–3	3.17–3	-6.85–3		
	5	-1.55–2	-5.55–3	-1.37–3	3.70–3	-2.33–3		5	-8.16–3	-8.08–3	2.86–3	6.05–4	-3.47–3		
	10	-4.78–2	-7.41–3	1.92–3	1.65–2	-1.85–2		10	-4.00–2	-1.44–2	1.17–2	1.26–2	-2.43–2		
5p <sub>3/2</sub>	1	-5.22–3	-1.39–6	1.24–3	2.33–3	-3.57–3	6s <sub>1/2</sub>	1	2.50–3	6.32–3	1.06–3	1.74–3	-2.79–3		
	3	-1.37–2	-8.30–3	3.47–3	2.85–3	-6.31–3		3	-2.99–2	-5.22–3	7.85–3	1.14–2	-1.93–2		
	5	-7.68–3	-7.74–3	2.81–3	5.34–4	-3.34–3		5	-4.99–2	-1.65–2	1.07–2	1.55–2	-2.62–2		
	10	-4.26–2	-1.47–2	1.24–2	1.36–2	-2.60–2		10	-4.18–2	-2.22–2	6.45–3	9.11–3	-1.56–2		
6s <sub>1/2</sub>	1	2.36–3	6.18–3	1.07–3	1.74–3	-2.81–3	Z = 69, Tm: 4f <sub>5/2</sub> <sup>6</sup> 4f <sub>7/2</sub> <sup>7</sup> 6s <sub>1/2</sub> <sup>2</sup>	Z = 70, Yb: 4f <sub>5/2</sub> <sup>6</sup> 4f <sub>7/2</sub> <sup>8</sup> 6s <sub>1/2</sub> <sup>2</sup>	3p <sub>3/2</sub>	1	-3.07–2	-1.08–2	2.75–3	8.51–3	-1.13–2
	3	-3.05–2	-5.90–3	7.85–3	1.14–2	-1.93–2									
	5	-4.88–2	-1.66–2	1.04–2	1.49–2	-2.53–2									
	10	-3.89–2	-2.14–2	5.81–3	8.18–3	-1.40–2									
3p <sub>3/2</sub>	1	-3.03–2	-1.08–2	2.91–3	8.39–3	-1.13–2									
	3	-1.69–2	-1.09–2	4.13–3	3.20–3	-7.33–3									
	5	-6.33–3	-7.02–3	3.09–3	3.43–4	-3.43–3									
	10	-4.66–2	-1.38–2	1.32–2	1.58–2	-2.90–2									
3d <sub>3/2</sub>	1	7.23–3	4.96–3	-1.36–3	-1.18–3	2.54–3	3d <sub>5/2</sub>	1	7.50–3	5.02–3	-1.30–3	-1.25–3	2.55–3		
	3	-2.05–2	4.58–3	-3.68–3	9.28–3	-5.60–3		3	-1.85–2	5.17–3	-3.90–3	8.70–3	-4.80–3		
	5	-7.66–2	-4.47–3	-1.04–3	2.87–2	-2.76–2		5	-7.37–2	-3.55–3	-1.41–3	2.78–2	-2.64–2		
	10	-2.48–1	-3.69–2	8.19–3	8.61–2	-9.43–2		10	-2.44–1	-3.56–2	8.05–3	8.49–2	-9.29–2		
3d <sub>5/2</sub>	1	1.44–2	4.30–3	1.43–3	-3.76–3	2.33–3	4s <sub>1/2</sub>	1	1.49–2	4.35–3	1.56–3	-3.91–3	2.35–3		
	3	-9.63–3	3.24–3	1.60–3	5.47–3	-7.06–3		3	-7.53–3	3.84–3	1.48–3	4.84–3	-6.33–3		
	5	-6.27–2	-6.80–3	5.99–3	2.36–2	-2.95–2		5	-5.96–2	-5.88–3	5.78–3	2.27–2	-2.84–2		
	10	-2.29–1	-4.25–2	1.74–2	7.79–2	-9.54–2		10	-2.24–1	-4.12–2	1.74–2	7.68–2	-9.42–2		
4s <sub>1/2</sub>	1	3.87–3	9.54–3	1.58–3	2.59–3	-4.17–3	4p <sub>3/2</sub>	1	4.19–3	9.96–3	1.60–3	2.63–3	-4.22–3		
	3	-3.34–2	-5.34–3	8.90–3	1.30–2	-2.19–2		3	-3.27–2	-4.55–3	8.91–3	1.30–2	-2.20–2		
	5	-5.42–2	-1.74–2	1.18–2	1.71–2	-2.89–2		5	-5.53–2	-1.72–2	1.22–2	1.77–2	-2.99–2		
	10	-4.54–2	-2.33–2	7.27–3	1.03–2	-1.75–2		10	-4.86–2	-2.42–2	7.99–3	1.13–2	-1.93–2		

Table 1 (continued)

Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$	Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$
4p <sub>1/2</sub>	1	-8.42–3	2.56–3	6.31–4	4.52–3	-5.15–3	4p <sub>1/2</sub>	1	-7.60–3	3.20–3	5.30–4	4.43–3	-4.96–3
	3	-2.43–2	-7.90–3	1.46–3	6.85–3	-8.32–3		3	-2.57–2	-8.16–3	1.70–3	7.34–3	-9.04–3
	5	-1.73–2	-6.06–3	-1.46–3	4.19–3	-2.73–3		5	-1.82–2	-6.48–3	-1.33–3	4.44–3	-3.10–3
	10	-4.40–2	-6.53–3	8.59–4	1.52–2	-1.60–2		10	-4.15–2	-6.28–3	3.56–4	1.41–2	-1.45–2
4p <sub>3/2</sub>	1	-6.93–3	-2.06–4	1.39–3	2.97–3	-4.36–3	4p <sub>3/2</sub>	1	-6.25–3	2.07–4	1.29–3	2.84–3	-4.13–3
	3	-1.60–2	-9.27–3	3.94–3	3.48–3	-7.43–3		3	-1.72–2	-9.61–3	4.17–3	3.85–3	-8.02–3
	5	-8.34–3	-8.27–3	2.98–3	6.24–4	-3.60–3		5	-9.01–3	-8.67–3	3.08–3	7.51–4	-3.83–3
	10	-3.89–2	-1.40–2	1.15–2	1.23–2	-2.37–2		10	-3.66–2	-1.38–2	1.09–2	1.13–2	-2.22–2
4d <sub>3/2</sub>	1	-7.61–3	-3.22–3	5.05–4	1.86–3	-2.36–3	4d <sub>3/2</sub>	1	-8.36–3	-3.45–3	5.17–4	2.07–3	-2.58–3
	3	-1.08–2	-2.49–4	-1.47–3	3.91–3	-2.44–3		3	-9.76–3	-1.86–4	-1.53–3	3.52–3	-1.99–3
	5	-5.04–2	-5.04–3	3.32–4	1.82–2	-1.86–2		5	-4.77–2	-4.51–3	5.92–5	1.73–2	-1.73–2
	10	-2.05–1	-3.19–2	9.41–3	7.10–2	-8.04–2		10	-1.99–1	-3.07–2	9.25–3	6.94–2	-7.86–2
4d <sub>5/2</sub>	1	-4.13–3	-3.48–3	1.61–3	5.83–4	-2.19–3	4d <sub>5/2</sub>	1	-4.80–3	-3.71–3	1.65–3	7.67–4	-2.41–3
	3	-3.15–3	-1.06–3	2.05–3	1.24–3	-3.29–3		3	-2.07–3	-9.73–4	1.99–3	8.36–4	-2.83–3
	5	-3.94–2	-6.78–3	6.08–3	1.43–2	-2.03–2		5	-3.66–2	-6.21–3	5.87–3	1.33–2	-1.92–2
	10	-1.87–1	-3.67–2	1.81–2	6.39–2	-8.20–2		10	-1.82–1	-3.55–2	1.80–2	6.23–2	-8.03–2
4f <sub>5/2</sub>	1	-6.84–3	5.85–5	-1.05–3	2.55–3	-1.50–3	4f <sub>5/2</sub>	1	-6.31–3	1.13–4	-1.02–3	2.36–3	-1.35–3
	3	-7.52–2	-9.49–3	-3.12–3	2.57–2	-2.26–2		3	-7.28–2	-8.88–3	-3.14–3	2.49–2	-2.18–2
	5	-1.71–1	-2.66–2	-5.88–3	5.67–2	-5.08–2		5	-1.68–1	-2.58–2	-5.70–3	5.57–2	-5.00–2
	10	-4.36–1	-7.79–2	-2.04–2	1.39–1	-1.19–1		10	-4.30–1	-7.64–2	-1.96–2	1.38–1	-1.18–1
4f <sub>7/2</sub>	1	-4.23–3	-2.98–4	-1.70–5	1.57–3	-1.55–3	4f <sub>7/2</sub>	1	-3.68–3	-2.43–4	1.66–5	1.38–3	-1.39–3
	3	-6.82–2	-1.08–2	2.35–4	2.30–2	-2.32–2		3	-6.57–2	-1.01–2	2.27–4	2.23–2	-2.25–2
	5	-1.60–1	-2.91–2	-6.93–4	5.23–2	-5.16–2		5	-1.57–1	-2.82–2	-4.65–4	5.14–2	-5.09–2
	10	-4.18–1	-8.37–2	-1.33–2	1.31–1	-1.18–1		10	-4.13–1	-8.22–2	-1.24–2	1.30–1	-1.17–1
5s <sub>1/2</sub>	1	2.98–3	6.85–3	1.06–3	1.76–3	-2.82–3	5s <sub>1/2</sub>	1	3.12–3	7.03–3	1.06–3	1.78–3	-2.84–3
	3	-2.94–2	-4.54–3	7.86–3	1.15–2	-1.94–2		3	-2.85–2	-3.78–3	7.82–3	1.15–2	-1.93–2
	5	-5.10–2	-1.64–2	1.11–2	1.61–2	-2.72–2		5	-5.19–2	-1.62–2	1.14–2	1.66–2	-2.80–2
	10	-4.46–2	-2.30–2	7.10–3	1.01–2	-1.72–2		10	-4.77–2	-2.39–2	7.80–3	1.11–2	-1.89–2
5p <sub>1/2</sub>	1	-4.32–3	3.07–3	5.71–4	3.07–3	-3.64–3	5p <sub>1/2</sub>	1	-3.55–3	3.54–3	4.96–4	2.94–3	-3.43–3
	3	-2.28–2	-7.37–3	1.74–3	6.53–3	-8.27–3		3	-2.39–2	-7.52–3	1.97–3	6.94–3	-8.91–3
	5	-1.70–2	-6.29–3	-1.15–3	4.06–3	-2.91–3		5	-1.80–2	-6.68–3	-1.00–3	4.31–3	-3.31–3
	10	-4.23–2	-6.80–3	8.84–4	1.44–2	-1.52–2		10	-3.98–2	-6.58–3	4.01–4	1.34–2	-1.38–2
5p <sub>3/2</sub>	1	-4.00–3	6.73–4	1.05–3	2.08–3	-3.13–3	5p <sub>3/2</sub>	1	-3.37–3	1.01–3	9.61–4	1.95–3	-2.91–3
	3	-1.57–2	-8.85–3	3.87–3	3.51–3	-7.38–3		3	-1.67–2	-9.10–3	4.08–3	3.84–3	-7.92–3
	5	-8.75–3	-8.43–3	2.94–3	7.13–4	-3.66–3		5	-9.42–3	-8.81–3	3.06–3	8.56–4	-3.91–3
	10	-3.76–2	-1.41–2	1.11–2	1.16–2	-2.28–2		10	-3.54–2	-1.39–2	1.05–2	1.07–2	-2.12–2
6s <sub>1/2</sub>	1	2.63–3	6.46–3	1.05–3	1.74–3	-2.79–3	6s <sub>1/2</sub>	1	2.80–3	6.63–3	1.04–3	1.74–3	-2.79–3
	3	-2.91–2	-4.47–3	7.81–3	1.14–2	-1.92–2		3	-2.80–2	-3.58–3	7.73–3	1.13–2	-1.91–2
	5	-5.09–2	-1.63–2	1.11–2	1.60–2	-2.71–2		5	-5.17–2	-1.61–2	1.14–2	1.65–2	-2.79–2
	10	-4.48–2	-2.31–2	7.12–3	1.01–2	-1.72–2		10	-4.79–2	-2.40–2	7.82–3	1.11–2	-1.89–2
<i>Z = 71, Lu: 4f<sub>5/2</sub><sup>6</sup>4f<sub>7/2</sub><sup>8</sup>5d<sub>3/2</sub><sup>1</sup>6s<sub>1/2</sub></i>							<i>Z = 72, Hf: 4f<sub>5/2</sub><sup>6</sup>4f<sub>7/2</sub><sup>8</sup>5d<sub>3/2</sub><sup>1</sup>6s<sub>1/2</sub></i>						
3d <sub>3/2</sub>	1	7.77–3	5.11–3	-1.25–3	-1.32–3	2.57–3	3d <sub>3/2</sub>	1	8.06–3	5.21–3	-1.20–3	-1.38–3	2.58–3
	3	-1.67–2	5.73–3	-4.10–3	8.17–3	-4.07–3		3	-1.49–2	6.33–3	-4.31–3	7.64–3	-3.33–3
	5	-7.09–2	-2.68–3	-1.76–3	2.69–2	-2.52–2		5	-6.81–2	-1.81–3	-2.12–3	2.61–2	-2.40–2
	10	-2.39–1	-3.44–2	7.87–3	8.36–2	-9.15–2		10	-2.35–1	-3.31–2	7.66–3	8.24–2	-9.01–2
3d <sub>5/2</sub>	1	1.54–2	4.42–3	1.68–3	-4.05–3	2.37–3	3d <sub>5/2</sub>	1	1.59–2	4.50–3	1.81–3	-4.20–3	2.39–3
	3	-5.57–3	4.41–3	1.39–3	4.27–3	-5.66–3		3	-3.53–3	5.02–3	1.30–3	3.68–3	-4.98–3
	5	-5.67–2	-5.00–3	5.57–3	2.18–2	-2.74–2		5	-5.39–2	-4.11–3	5.37–3	2.10–2	-2.64–2
	10	-2.20–1	-3.99–2	1.74–2	7.56–2	-9.30–2		10	-2.16–1	-3.86–2	1.73–2	7.45–2	-9.18–2
4s <sub>1/2</sub>	1	4.40–3	1.03–2	1.63–3	2.69–3	-4.32–3	4s <sub>1/2</sub>	1	4.58–3	1.07–2	1.68–3	2.78–3	-4.46–3
	3	-3.20–2	-3.79–3	8.92–3	1.31–2	-2.20–2		3	-3.14–2	-3.00–3	8.93–3	1.31–2	-2.21–2
	5	-5.64–2	-1.71–2	1.26–2	1.82–2	-3.08–2		5	-5.73–2	-1.68–2	1.29–2	1.88–2	-3.17–2
	10	-5.18–2	-2.51–2	8.73–3	1.24–2	-2.12–2		10	-5.51–2	-2.60–2	9.50–3	1.36–2	-2.31–2
4p <sub>1/2</sub>	1	-6.92–3	3.69–3	4.50–4	4.34–3	-4.79–3	4p <sub>1/2</sub>	1	-6.34–3	4.24–3	3.81–4	4.31–3	-4.69–3
	3	-2.68–2	-8.35–3	1.92–3	7.77–3	-9.69–3		3	-2.82–2	-8.57–3	2.14–3	8.26–3	-1.04–2
	5	-1.92–2	-6.89–3	-1.19–3	4.70–3	-3.52–3		5	-2.04–2	-7.33–3	-1.02–3	5.03–3	-4.00–3
	10	-3.91–2	-6.07–3	-1.09–4	1.32–2	-1.31–2		10	-3.71–2	-5.93–3	-5.48–4	1.23–2	-1.18–2

(continued on next page)

Table 1 (continued)

Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$	Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$
4p <sub>3/2</sub>	1	-5.73-3	5.15-4	1.21-3	2.74-3	-3.94-3	4p <sub>3/2</sub>	1	-5.24-3	8.24-4	1.14-3	2.65-3	-3.79-3
	3	-1.82-2	-9.91-3	4.37-3	4.19-3	-8.56-3		3	-1.93-2	-1.02-2	4.59-3	4.54-3	-9.13-3
	5	-9.72-3	-9.06-3	3.21-3	9.06-4	-4.11-3		5	-1.05-2	-9.49-3	3.36-3	1.09-3	-4.45-3
	10	-3.45-2	-1.35-2	1.03-2	1.04-2	-2.07-2		10	-3.25-2	-1.34-2	9.79-3	9.61-3	-1.94-2
4d <sub>3/2</sub>	1	-9.01-3	-3.65-3	5.14-4	2.25-3	-2.76-3	4d <sub>3/2</sub>	1	-9.75-3	-3.87-3	5.05-4	2.45-3	-2.96-3
	3	-8.90-3	-1.53-4	-1.57-3	3.18-3	-1.61-3		3	-8.14-3	-1.41-4	-1.61-3	2.88-3	-1.27-3
	5	-4.51-2	-4.01-3	-1.99-4	1.64-2	-1.62-2		5	-4.26-2	-3.55-3	-4.55-4	1.55-2	-1.51-2
	10	-1.94-1	-2.95-2	9.05-3	6.77-2	-7.68-2		10	-1.89-1	-2.84-2	8.83-3	6.62-2	-7.50-2
4d <sub>5/2</sub>	1	-5.41-3	-3.91-3	1.66-3	9.32-4	-2.60-3	4d <sub>5/2</sub>	1	-6.06-3	-4.14-3	1.68-3	1.10-3	-2.79-3
	3	-1.15-3	-9.16-4	1.95-3	4.84-4	-2.43-3		3	-3.03-4	-8.78-4	1.92-3	1.53-4	-2.07-3
	5	-3.40-2	-5.68-3	5.67-3	1.25-2	-1.81-2		5	-3.15-2	-5.17-3	5.47-3	1.16-2	-1.71-2
	10	-1.77-1	-3.42-2	1.79-2	6.08-2	-7.87-2		10	-1.72-1	-3.31-2	1.78-2	5.93-2	-7.71-2
4f <sub>5/2</sub>	1	-5.77-3	2.05-4	-9.83-4	2.19-3	-1.21-3	4f <sub>5/2</sub>	1	-5.27-3	2.99-4	-9.52-4	2.04-3	-1.08-3
	3	-7.04-2	-8.27-3	-3.14-3	2.42-2	-2.11-2		3	-6.81-2	-7.70-3	-3.16-3	2.35-2	-2.04-2
	5	-1.65-1	-2.49-2	-5.52-3	5.48-2	-4.92-2		5	-1.61-1	-2.40-2	-5.37-3	5.39-2	-4.85-2
	10	-4.25-1	-7.49-2	-1.89-2	1.36-1	-1.17-1		10	-4.20-1	-7.36-2	-1.82-2	1.35-1	-1.17-1
4f <sub>7/2</sub>	1	-3.13-3	-1.50-4	5.22-5	1.20-3	-1.26-3	4f <sub>7/2</sub>	1	-2.61-3	-5.63-5	8.98-5	1.04-3	-1.13-3
	3	-6.33-2	-9.53-3	2.29-4	2.16-2	-2.18-2		3	-6.11-2	-8.96-3	2.18-4	2.09-2	-2.11-2
	5	-1.54-1	-2.73-2	-2.47-4	5.05-2	-5.02-2		5	-1.50-1	-2.64-2	-4.90-5	4.96-2	-4.96-2
	10	-4.08-1	-8.08-2	-1.16-2	1.29-1	-1.17-1		10	-4.03-1	-7.94-2	-1.08-2	1.27-1	-1.16-1
5s <sub>1/2</sub>	1	3.19-3	7.16-3	1.07-3	1.80-3	-2.88-3	5s <sub>1/2</sub>	1	3.24-3	7.31-3	1.10-3	1.85-3	-2.94-3
	3	-2.77-2	-3.06-3	7.77-3	1.14-2	-1.92-2		3	-2.69-2	-2.32-3	7.72-3	1.14-2	-1.91-2
	5	-5.26-2	-1.60-2	1.17-2	1.70-2	-2.88-2		5	-5.33-2	-1.56-2	1.20-2	1.75-2	-2.95-2
	10	-5.08-2	-2.48-2	8.51-3	1.21-2	-2.06-2		10	-5.39-2	-2.56-2	9.24-3	1.32-2	-2.24-2
5p <sub>1/2</sub>	1	-2.94-3	3.91-3	4.47-4	2.83-3	-3.28-3	5p <sub>1/2</sub>	1	-2.36-3	4.29-3	4.07-4	2.74-3	-3.15-3
	3	-2.48-2	-7.63-3	2.19-3	7.32-3	-9.51-3		3	-2.58-2	-7.72-3	2.40-3	7.71-3	-1.01-2
	5	-1.89-2	-7.06-3	-8.36-4	4.58-3	-3.75-3		5	-2.00-2	-7.46-3	-6.47-4	4.90-3	-4.25-3
	10	-3.75-2	-6.42-3	-4.30-5	1.24-2	-1.24-2		10	-3.55-2	-6.31-3	-4.59-4	1.16-2	-1.11-2
5p <sub>3/2</sub>	1	-2.89-3	1.25-3	8.93-4	1.84-3	-2.73-3	5p <sub>3/2</sub>	1	-2.43-3	1.49-3	8.35-4	1.74-3	-2.57-3
	3	-1.75-2	-9.31-3	4.26-3	4.14-3	-8.40-3		3	-1.84-2	-9.54-3	4.45-3	4.45-3	-8.89-3
	5	-1.02-2	-9.19-3	3.19-3	1.03-3	-4.21-3		5	-1.10-2	-9.59-3	3.34-3	1.23-3	-4.57-3
	10	-3.33-2	-1.37-2	9.98-3	9.85-3	-1.98-2		10	-3.14-2	-1.35-2	9.47-3	9.04-3	-1.85-2
5d <sub>3/2</sub>	1	-8.33-3	-3.12-3	6.63-4	2.22-3	-2.88-3	5d <sub>3/2</sub>	1	-8.81-3	-3.22-3	6.52-4	2.37-3	-3.02-3
	3	-7.99-3	-7.24-4	-1.29-3	2.65-3	-1.36-3		3	-7.40-3	-8.17-4	-1.27-3	2.38-3	-1.11-3
	5	-4.18-2	-4.12-3	-8.01-5	1.51-2	-1.50-2		5	-3.93-2	-3.70-3	-3.19-4	1.42-2	-1.39-2
	10	-1.89-1	-2.89-2	9.19-3	6.57-2	-7.49-2		10	-1.83-1	-2.78-2	8.96-3	6.40-2	-7.29-2
6s <sub>1/2</sub>	1	2.83-3	6.74-3	1.06-3	1.78-3	-2.84-3	6s <sub>1/2</sub>	1	2.87-3	6.84-3	1.07-3	1.80-3	-2.87-3
	3	-2.74-2	-2.94-3	7.69-3	1.13-2	-1.90-2		3	-2.60-2	-1.95-3	7.56-3	1.11-2	-1.87-2
	5	-5.24-2	-1.59-2	1.17-2	1.70-2	-2.87-2		5	-5.31-2	-1.56-2	1.20-2	1.74-2	-2.94-2
	10	-5.09-2	-2.48-2	8.53-3	1.22-2	-2.07-2		10	-5.41-2	-2.56-2	9.26-3	1.32-2	-2.25-2
<i>Z</i> = 73, Ta: 4f <sub>5/2</sub> <sup>6</sup> 4f <sub>7/2</sub> <sup>8</sup> 5d <sub>3/2</sub> <sup>3</sup> 6s <sub>1/2</sub> <sup>2</sup>							<i>Z</i> = 74, W: 4f <sub>5/2</sub> <sup>6</sup> 4f <sub>7/2</sub> <sup>8</sup> 5d <sub>3/2</sub> <sup>4</sup> 6s <sub>1/2</sub> <sup>2</sup>						
3d <sub>3/2</sub>	1	8.34-3	5.31-3	-1.15-3	-1.44-3	2.59-3	3d <sub>3/2</sub>	1	8.62-3	5.41-3	-1.09-3	-1.50-3	2.59-3
	3	-1.32-2	6.90-3	-4.51-3	7.14-3	-2.63-3		3	-1.15-2	7.45-3	-4.70-3	6.65-3	-1.95-3
	5	-6.55-2	-9.42-4	-2.49-3	2.53-2	-2.28-2		5	-6.28-2	-7.63-5	-2.87-3	2.45-2	-2.16-2
	10	-2.31-1	-3.19-2	7.41-3	8.12-2	-8.87-2		10	-2.27-1	-3.06-2	7.13-3	8.00-2	-8.72-2
3d <sub>5/2</sub>	1	1.64-2	4.59-3	1.94-3	-4.35-3	2.41-3	3d <sub>5/2</sub>	1	1.70-2	4.67-3	2.08-3	-4.50-3	2.41-3
	3	-1.62-3	5.58-3	1.22-3	3.12-3	-4.34-3		3	2.80-4	6.15-3	1.14-3	2.58-3	-3.72-3
	5	-5.11-2	-3.24-3	5.17-3	2.02-2	-2.53-2		5	-4.83-2	-2.36-3	4.97-3	1.94-2	-2.43-2
	10	-2.12-1	-3.73-2	1.72-2	7.33-2	-9.06-2		10	-2.08-1	-3.60-2	1.72-2	7.22-2	-8.93-2
4s <sub>1/2</sub>	1	4.73-3	1.11-2	1.74-3	2.89-3	-4.62-3	4s <sub>1/2</sub>	1	4.83-3	1.14-2	1.80-3	3.00-3	-4.81-3
	3	-3.06-2	-2.17-3	8.92-3	1.32-2	-2.21-2		3	-2.98-2	-1.31-3	8.91-3	1.32-2	-2.21-2
	5	-5.82-2	-1.65-2	1.33-2	1.93-2	-3.26-2		5	-5.89-2	-1.61-2	1.36-2	1.98-2	-3.34-2
	10	-5.85-2	-2.69-2	1.03-2	1.47-2	-2.50-2		10	-6.19-2	-2.77-2	1.11-2	1.59-2	-2.70-2
4p <sub>1/2</sub>	1	-5.74-3	4.80-3	3.15-4	4.28-3	-4.59-3	4p <sub>1/2</sub>	1	-5.13-3	5.35-3	2.53-4	4.24-3	-4.50-3
	3	-2.94-2	-8.76-3	2.37-3	8.74-3	-1.11-2		3	-3.07-2	-8.92-3	2.59-3	9.22-3	-1.18-2
	5	-2.17-2	-7.78-3	-8.37-4	5.39-3	-4.55-3		5	-2.30-2	-8.23-3	-6.31-4	5.78-3	-5.15-3
	10	-3.52-2	-5.84-3	-9.60-4	1.15-2	-1.06-2		10	-3.34-2	-5.78-3	-1.35-3	1.08-2	-9.45-3

Table 1 (continued)

Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$	Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$
4p <sub>3/2</sub>	1	-4.75–3	1.13–3	1.07–3	2.57–3	-3.63–3	4p <sub>3/2</sub>	1	-4.25–3	1.44–3	9.99–4	2.47–3	-3.47–3
	3	-2.04–2	-1.05–2	4.80–3	4.89–3	-9.70–3		3	-2.14–2	-1.08–2	5.01–3	5.24–3	-1.02–2
	5	-1.14–2	-9.93–3	3.53–3	1.31–3	-4.84–3		5	-1.24–2	-1.04–2	3.72–3	1.55–3	-5.27–3
	10	-3.07–2	-1.33–2	9.30–3	8.84–3	-1.81–2		10	-2.90–2	-1.32–2	8.84–3	8.10–3	-1.69–2
4d <sub>3/2</sub>	1	-1.05–2	-4.09–3	4.86–4	2.65–3	-3.14–3	4d <sub>3/2</sub>	1	-1.12–2	-4.30–3	4.57–4	2.85–3	-3.31–3
	3	-7.49–3	-1.66–4	-1.62–3	2.61–3	-9.84–4		3	-6.94–3	-2.18–4	-1.63–3	2.36–3	-7.36–4
	5	-4.02–2	-3.11–3	-7.06–4	1.47–2	-1.40–2		5	-3.79–2	-2.69–3	-9.52–4	1.39–2	-1.29–2
	10	-1.84–1	-2.73–2	8.57–3	6.46–2	-7.31–2		10	-1.79–1	-2.62–2	8.28–3	6.30–2	-7.12–2
4d <sub>5/2</sub>	1	-6.71–3	-4.36–3	1.70–3	1.28–3	-2.97–3	4d <sub>5/2</sub>	1	-7.38–3	-4.58–3	1.70–3	1.46–3	-3.16–3
	3	4.29–4	-8.78–4	1.90–3	-1.43–4	-1.75–3		3	1.07–3	-9.06–4	1.89–3	-4.13–4	-1.48–3
	5	-2.91–2	-4.69–3	5.28–3	1.08–2	-1.61–2		5	-2.67–2	-4.24–3	5.09–3	1.00–2	-1.51–2
	10	-1.67–1	-3.19–2	1.77–2	5.78–2	-7.55–2		10	-1.63–1	-3.07–2	1.76–2	5.63–2	-7.38–2
4f <sub>5/2</sub>	1	-4.78–3	3.94–4	-9.21–4	1.89–3	-9.66–4	4f <sub>5/2</sub>	1	-4.30–3	4.91–4	-8.88–4	1.74–3	-8.52–4
	3	-6.59–2	-7.13–3	-3.18–3	2.29–2	-1.97–2		3	-6.37–2	-6.57–3	-3.20–3	2.22–2	-1.90–2
	5	-1.58–1	-2.32–2	-5.23–3	5.29–2	-4.77–2		5	-1.55–1	-2.23–2	-5.12–3	5.20–2	-4.69–2
	10	-4.15–1	-7.22–2	-1.75–2	1.34–1	-1.16–1		10	-4.10–1	-7.08–2	-1.68–2	1.32–1	-1.16–1
4f <sub>7/2</sub>	1	-2.09–3	3.86–5	1.29–4	8.78–4	-1.01–3	4f <sub>7/2</sub>	1	-1.58–3	1.34–4	1.69–4	7.20–4	-8.89–4
	3	-5.88–2	-8.38–3	2.11–4	2.02–2	-2.04–2		3	-5.65–2	-7.81–3	2.02–4	1.95–2	-1.97–2
	5	-1.47–1	-2.55–2	1.30–4	4.87–2	-4.88–2		5	-1.44–1	-2.46–2	2.92–4	4.78–2	-4.81–2
	10	-3.98–1	-7.80–2	-1.01–2	1.26–1	-1.16–1		10	-3.93–1	-7.66–2	-9.31–3	1.25–1	-1.15–1
5s <sub>1/2</sub>	1	3.27–3	7.46–3	1.12–3	1.90–3	-3.02–3	5s <sub>1/2</sub>	1	3.29–3	7.60–3	1.16–3	1.96–3	-3.11–3
	3	-2.60–2	-1.56–3	7.66–3	1.13–2	-1.90–2		3	-2.51–2	-7.83–4	7.59–3	1.13–2	-1.88–2
	5	-5.38–2	-1.53–2	1.23–2	1.79–2	-3.02–2		5	-5.42–2	-1.48–2	1.25–2	1.83–2	-3.08–2
	10	-5.71–2	-2.64–2	9.99–3	1.43–2	-2.43–2		10	-6.04–2	-2.72–2	1.08–2	1.54–2	-2.62–2
5p <sub>1/2</sub>	1	-1.79–3	4.67–3	3.75–4	2.66–3	-3.03–3	5p <sub>1/2</sub>	1	-1.23–3	5.05–3	3.51–4	2.58–3	-2.93–3
	3	-2.67–2	-7.78–3	2.61–3	8.10–3	-1.07–2		3	-2.76–2	-7.80–3	2.82–3	8.48–3	-1.13–2
	5	-2.12–2	-7.86–3	-4.37–4	5.25–3	-4.81–3		5	-2.24–2	-8.26–3	-2.06–4	5.63–3	-5.42–3
	10	-3.37–2	-6.25–3	-8.48–4	1.08–2	-9.95–3		10	-3.20–2	-6.23–3	-1.21–3	1.01–2	-8.86–3
5p <sub>3/2</sub>	1	-1.98–3	1.73–3	7.82–4	1.64–3	-2.42–3	5p <sub>3/2</sub>	1	-1.53–3	1.96–3	7.34–4	1.54–3	-2.28–3
	3	-1.93–2	-9.74–3	4.62–3	4.75–3	-9.37–3		3	-2.01–2	-9.92–3	4.79–3	5.04–3	-9.83–3
	5	-1.19–2	-9.99–3	3.51–3	1.45–3	-4.97–3		5	-1.28–2	-1.04–2	3.71–3	1.70–3	-5.41–3
	10	-2.97–2	-1.34–2	8.98–3	8.28–3	-1.73–2		10	-2.81–2	-1.34–2	8.52–3	7.57–3	-1.61–2
5d <sub>3/2</sub>	1	-9.34–3	-3.35–3	6.41–4	2.53–3	-3.17–3	5d <sub>3/2</sub>	1	-9.84–3	-3.45–3	6.17–4	2.68–3	-3.30–3
	3	-6.84–3	-8.79–4	-1.26–3	2.13–3	-8.65–4		3	-6.36–3	-9.65–4	-1.24–3	1.91–3	-6.67–4
	5	-3.69–2	-3.33–3	-5.48–4	1.33–2	-1.28–2		5	-3.46–2	-2.98–3	-7.65–4	1.25–2	-1.17–2
	10	-1.78–1	-2.67–2	8.70–3	6.23–2	-7.10–2		10	-1.73–1	-2.56–2	8.42–3	6.06–2	-6.90–2
6s <sub>1/2</sub>	1	3.08–3	7.09–3	1.07–3	1.82–3	-2.89–3	6s <sub>1/2</sub>	1	3.21–3	7.31–3	1.09–3	1.86–3	-2.95–3
	3	-2.54–2	-1.38–3	7.52–3	1.11–2	-1.87–2		3	-2.48–2	-7.64–4	7.48–3	1.11–2	-1.86–2
	5	-5.35–2	-1.51–2	1.22–2	1.78–2	-3.00–2		5	-5.38–2	-1.47–2	1.25–2	1.81–2	-3.06–2
	10	-5.72–2	-2.64–2	1.00–2	1.43–2	-2.43–2		10	-6.04–2	-2.72–2	1.08–2	1.55–2	-2.62–2
<i>Z</i> = 75, Re: 4f <sub>5/2</sub> <sup>6</sup> 4f <sub>7/2</sub> <sup>8</sup> 5d <sub>3/2</sub> <sup>4</sup> 5d <sub>5/2</sub> <sup>1</sup> 6s <sub>1/2</sub> <sup>2</sup>							<i>Z</i> = 76, Os: 4f <sub>5/2</sub> <sup>6</sup> 4f <sub>7/2</sub> <sup>8</sup> 5d <sub>3/2</sub> <sup>4</sup> 5d <sub>5/2</sub> <sup>2</sup> 6s <sub>1/2</sub> <sup>2</sup>						
3d <sub>3/2</sub>	1	8.87–3	5.51–3	-1.03–3	-1.55–3	2.58–3	3d <sub>5/2</sub>	1	1.79–2	4.82–3	2.37–3	-4.77–3	2.40–3
	3	-9.86–3	8.01–3	-4.89–3	6.17–3	-1.28–3		3	4.03–3	7.25–3	1.02–3	1.49–3	-2.51–3
	5	-6.01–2	7.87–4	-3.24–3	2.37–2	-2.05–2		5	-4.26–2	-6.08–4	4.58–3	1.77–2	-2.23–2
	10	-2.23–1	-2.93–2	6.80–3	7.88–2	-8.56–2		10	-2.00–1	-3.34–2	1.69–2	6.99–2	-8.68–2
3d <sub>5/2</sub>	1	1.75–2	4.75–3	2.22–3	-4.64–3	2.41–3	4s <sub>1/2</sub>	1	4.91–3	1.22–2	1.98–3	3.30–3	-5.27–3
	3	2.16–3	6.70–3	1.08–3	2.03–3	-3.11–3		3	-2.80–2	4.94–4	8.85–3	1.32–2	-2.20–2
	5	-4.54–2	-1.48–3	4.77–3	1.85–2	-2.33–2		5	-5.99–2	-1.52–2	1.42–2	2.07–2	-3.50–2
	10	-2.04–1	-3.47–2	1.70–2	7.10–2	-8.81–2		10	-6.88–2	-2.93–2	1.28–2	1.84–2	-3.12–2
4s <sub>1/2</sub>	1	4.91–3	1.18–2	1.88–3	3.14–3	-5.02–3	4p <sub>1/2</sub>	1	-3.93–3	6.49–3	1.43–4	4.19–3	-4.34–3
	3	-2.89–2	-4.26–4	8.88–3	1.32–2	-2.21–2		3	-3.31–2	-9.14–3	3.01–3	1.02–2	-1.32–2
	5	-5.95–2	-1.57–2	1.39–2	2.03–2	-3.42–2		5	-2.59–2	-9.15–3	-1.60–4	6.68–3	-6.52–3
	10	-6.54–2	-2.85–2	1.19–2	1.71–2	-2.91–2		10	-3.06–2	-5.83–3	-2.03–3	9.49–3	-7.46–3
4p <sub>1/2</sub>	1	-4.52–3	5.91–3	1.98–4	4.21–3	-4.41–3	4p <sub>3/2</sub>	1	-3.25–3	2.05–3	8.71–4	2.29–3	-3.16–3
	3	-3.19–2	-9.04–3	2.80–3	9.70–3	-1.25–2		3	-2.35–2	-1.14–2	5.40–3	5.92–3	-1.13–2
	5	-2.44–2	-8.69–3	-4.05–4	6.21–3	-5.81–3		5	-1.45–2	-1.13–2	4.17–3	2.11–3	-6.28–3
	10	-3.19–2	-5.78–3	-1.70–3	1.01–2	-8.41–3		10	-2.61–2	-1.31–2	8.01–3	6.78–3	-1.48–2

(continued on next page)

Table 1 (continued)

Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$	Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$
4p <sub>3/2</sub>	1	-3.75-3	1.75-3	9.35-4	2.38-3	-3.32-3	4d <sub>3/2</sub>	1	-1.27-2	-4.72-3	3.69-4	3.26-3	-3.62-3
	3	-2.24-2	-1.11-2	5.21-3	5.58-3	-1.08-2		3	-6.11-3	-4.05-4	-1.60-3	1.96-3	-3.65-4
	5	-1.34-2	-1.08-2	3.94-3	1.82-3	-5.75-3		5	-3.35-2	-1.95-3	-1.42-3	1.23-2	-1.09-2
	10	-2.75-2	-1.31-2	8.41-3	7.42-3	-1.58-2		10	-1.70-1	-2.40-2	7.62-3	5.98-2	-6.74-2
4d <sub>5/2</sub>	1	-1.20-2	-4.52-3	4.18-4	3.06-3	-3.48-3	4f <sub>5/2</sub>	1	-8.69-3	-5.01-3	1.69-3	1.81-3	-3.50-3
	3	-6.48-3	-2.98-4	-1.62-3	2.15-3	-5.30-4		3	2.09-3	-1.04-3	1.90-3	-8.73-4	-1.03-3
	5	-3.57-2	-2.31-3	-1.19-3	1.31-2	-1.19-2		5	-2.22-2	-3.41-3	4.73-3	8.46-3	-1.32-2
	10	-1.75-1	-2.51-2	7.96-3	6.14-2	-6.93-2		10	-1.53-1	-2.84-2	1.72-2	5.33-2	-7.05-2
4f <sub>5/2</sub>	1	-8.05-3	-4.80-3	1.70-3	1.64-3	-3.34-3	4f <sub>7/2</sub>	1	-3.37-3	6.78-4	-8.19-4	1.46-3	-6.37-4
	3	1.63-3	-9.60-4	1.89-3	-6.56-4	-1.24-3		3	-5.92-2	-5.46-3	-3.23-3	2.09-2	-1.76-2
	5	-2.44-2	-3.81-3	4.91-3	9.22-3	-1.41-2		5	-1.48-1	-2.05-2	-4.94-3	5.01-2	-4.52-2
	10	-1.58-1	-2.96-2	1.74-2	5.48-2	-7.22-2		10	-4.00-1	-6.82-2	-1.56-2	1.30-1	-1.14-1
4f <sub>7/2</sub>	1	-3.83-3	5.89-4	-8.54-4	1.60-3	-7.42-4	5s <sub>1/2</sub>	1	-6.08-4	3.21-4	2.50-4	4.22-4	-6.71-4
	3	-6.15-2	-6.01-3	-3.22-3	2.15-2	-1.83-2		3	-5.21-2	-6.70-3	1.83-4	1.82-2	-1.84-2
	5	-1.52-1	-2.14-2	-5.02-3	5.11-2	-4.61-2		5	-1.38-1	-2.28-2	5.58-4	4.60-2	-4.65-2
	10	-4.05-1	-6.95-2	-1.62-2	1.31-1	-1.15-1		10	-3.84-1	-7.40-2	-7.86-3	1.22-1	-1.14-1
5s <sub>1/2</sub>	1	-1.08-3	2.32-4	2.10-4	5.67-4	-7.76-4	5p <sub>1/2</sub>	1	3.23-3	7.87-3	1.24-3	2.10-3	-3.34-3
	3	-5.43-2	-7.25-3	1.93-4	1.89-2	-1.91-2		3	-2.32-2	8.30-4	7.43-3	1.11-2	-1.85-2
	5	-1.41-1	-2.37-2	4.34-4	4.69-2	-4.73-2		5	-5.47-2	-1.38-2	1.30-2	1.89-2	-3.19-2
	10	-3.88-1	-7.53-2	-8.58-3	1.24-1	-1.15-1		10	-6.68-2	-2.86-2	1.23-2	1.78-2	-3.01-2
5p <sub>3/2</sub>	1	3.28-3	7.74-3	1.19-3	2.02-3	-3.21-3	5p <sub>3/2</sub>	1	-1.57-4	5.81-3	3.28-4	2.45-3	-2.78-3
	3	-2.42-2	1.32-5	7.51-3	1.12-2	-1.87-2		3	-2.92-2	-7.75-3	3.21-3	9.22-3	-1.24-2
	5	-5.45-2	-1.44-2	1.28-2	1.86-2	-3.14-2		5	-2.51-2	-9.05-3	3.12-4	6.48-3	-6.80-3
	10	-6.36-2	-2.79-2	1.16-2	1.66-2	-2.81-2		10	-2.93-2	-6.35-3	-1.84-3	8.82-3	-6.98-3
5p <sub>1/2</sub>	1	-6.87-4	5.43-3	3.36-4	2.51-3	-2.85-3	5d <sub>3/2</sub>	1	-6.51-4	2.42-3	6.54-4	1.36-3	-2.01-3
	3	-2.84-2	-7.79-3	3.02-3	8.85-3	-1.19-2		3	-2.17-2	-1.02-2	5.12-3	5.60-3	-1.07-2
	5	-2.37-2	-8.66-3	4.38-5	6.04-3	-6.08-3		5	-1.49-2	-1.13-2	4.15-3	2.27-3	-6.43-3
	10	-3.06-2	-6.26-3	-1.54-3	9.41-3	-7.87-3		10	-2.53-2	-1.34-2	7.71-3	6.30-3	-1.40-2
5d <sub>5/2</sub>	1	-1.09-3	2.19-3	6.92-4	1.45-3	-2.14-3	5d <sub>5/2</sub>	1	-1.06-2	-3.53-3	5.27-4	2.94-3	-3.47-3
	3	-2.09-2	-1.01-2	4.96-3	5.32-3	-1.03-2		3	-5.82-3	-1.30-3	-1.12-3	1.59-3	-4.61-4
	5	-1.38-2	-1.08-2	3.92-3	1.98-3	-5.90-3		5	-3.02-2	-2.39-3	-1.17-3	1.09-2	-9.73-3
	10	-2.66-2	-1.34-2	8.10-3	6.91-3	-1.50-2		10	-1.62-1	-2.35-2	7.75-3	5.72-2	-6.49-2
5d <sub>3/2</sub>	1	-1.03-2	-3.51-3	5.79-4	2.82-3	-3.40-3	5d <sub>5/2</sub>	1	-7.79-3	-3.92-3	1.55-3	1.86-3	-3.41-3
	3	-6.01-3	-1.09-3	-1.20-3	1.73-3	-5.27-4		3	1.74-3	-1.86-3	2.00-3	-1.04-3	-9.64-4
	5	-3.23-2	-2.66-3	-9.76-4	1.17-2	-1.07-2		5	-1.95-2	-3.75-3	4.68-3	7.24-3	-1.19-2
	10	-1.68-1	-2.45-2	8.10-3	5.89-2	-6.70-2		10	-1.46-1	-2.77-2	1.72-2	5.09-2	-6.81-2
5d <sub>5/2</sub>	1	-7.43-3	-3.89-3	1.58-3	1.73-3	-3.32-3	6s <sub>1/2</sub>	1	3.02-3	7.44-3	1.19-3	2.01-3	-3.19-3
	3	1.51-3	-1.68-3	1.96-3	-8.85-4	-1.08-3		3	-2.24-2	1.05-3	7.24-3	1.08-2	-1.81-2
	5	-2.16-2	-4.07-3	4.84-3	8.00-3	-1.28-2		5	-5.42-2	-1.36-2	1.28-2	1.88-2	-3.16-2
	10	-1.51-1	-2.89-2	1.74-2	5.25-2	-6.99-2		10	-6.68-2	-2.86-2	1.23-2	1.78-2	-3.01-2
6s <sub>1/2</sub>	1	3.22-3	7.46-3	1.13-3	1.92-3	-3.05-3	Z = 78, Pt: 4f <sub>5/2</sub> <sup>6</sup> 4f <sub>7/2</sub> <sup>8</sup> 5d <sub>3/2</sub> <sup>4</sup> 5d <sub>5/2</sub> <sup>5</sup> 6s <sub>1/2</sub> <sup>1</sup>	1	4.88-3	1.30-2	2.20-3	3.67-3	-5.87-3
	3	-2.40-2	-6.37-5	7.42-3	1.10-2	-1.85-2		3	-2.61-2	2.47-3	8.78-3	1.32-2	-2.19-2
	5	-5.41-2	-1.42-2	1.27-2	1.85-2	-3.11-2		5	-6.06-2	-1.39-2	1.47-2	2.16-2	-3.64-2
	10	-6.36-2	-2.79-2	1.16-2	1.66-2	-2.82-2		10	-7.59-2	-3.08-2	1.45-2	2.10-2	-3.55-2
Z = 77, Ir: 4f <sub>5/2</sub> <sup>6</sup> 4f <sub>7/2</sub> <sup>8</sup> 5d <sub>3/2</sub> <sup>4</sup> 5d <sub>5/2</sub> <sup>5</sup> 6s <sub>1/2</sub> <sup>2</sup>	1	4.92-3	1.25-2	2.08-3	3.47-3	-5.54-3	4s <sub>1/2</sub>	1	2.21-3	7.74-3	6.54-5	4.19-3	-4.25-3
	3	-2.71-2	1.45-3	8.82-3	1.32-2	-2.20-2		3	-3.54-2	-9.23-3	3.42-3	1.12-2	-1.46-2
	5	-6.03-2	-1.46-2	1.45-2	2.12-2	-3.57-2		5	-2.92-2	-1.01-2	3.88-4	7.73-3	-8.11-3
	10	-7.23-2	-3.00-2	1.37-2	1.96-2	-3.33-2		10	-2.85-2	-6.06-3	-2.59-3	8.44-3	-5.85-3
4p <sub>1/2</sub>	1	-3.34-3	7.08-3	1.02-4	4.19-3	-4.29-3	4p <sub>1/2</sub>	1	-2.69-3	7.74-3	6.54-5	4.19-3	-4.25-3
	3	-3.42-2	-9.20-3	3.22-3	1.07-2	-1.39-2		3	-3.54-2	-9.23-3	3.42-3	1.12-2	-1.46-2
	5	-2.75-2	-9.61-3	1.03-4	7.18-3	-7.28-3		5	-2.92-2	-1.01-2	3.88-4	7.73-3	-8.11-3
	10	-2.94-2	-5.92-3	-2.32-3	8.94-3	-6.61-3		10	-2.85-2	-6.06-3	-2.59-3	8.44-3	-5.85-3
4p <sub>3/2</sub>	1	-2.75-3	2.36-3	8.17-4	2.21-3	-3.02-3	4p <sub>3/2</sub>	1	-2.19-3	2.71-3	7.62-4	2.11-3	-2.87-3
	3	-2.44-2	-1.16-2	5.59-3	6.25-3	-1.18-2		3	-2.55-2	-1.19-2	5.78-3	6.59-3	-1.24-2
	5	-1.57-2	-1.18-2	4.42-3	2.42-3	-6.84-3		5	-1.69-2	-1.23-2	4.69-3	2.76-3	-7.46-3
	10	-2.48-2	-1.32-2	7.65-3	6.19-3	-1.38-2		10	-2.37-2	-1.33-2	7.32-3	5.64-3	-1.30-2

Table 1 (continued)

Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$	Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$	
4d <sub>3/2</sub>	1	-1.34–2	-4.93–3	3.08–4	3.47–3	-3.77–3	4d <sub>3/2</sub>	1	-1.43–2	-5.18–3	2.30–4	3.71–3	-3.94–3	
	3	-5.83–3	-5.37–4	-1.56–3	1.80–3	-2.40–4		3	-5.65–3	-7.04–4	-1.52–3	1.67–3	-1.55–4	
	5	-3.14–2	-1.63–3	-1.64–3	1.16–2	-9.96–3		5	-2.95–2	-1.33–3	-1.85–3	1.09–2	-9.04–3	
	10	-1.65–1	-2.30–2	7.24–3	5.82–2	-6.55–2		10	-1.60–1	-2.20–2	6.85–3	5.67–2	-6.35–2	
4d <sub>5/2</sub>	1	-9.40–3	-5.24–3	1.68–3	2.00–3	-3.68–3	4d <sub>5/2</sub>	1	-1.02–2	-5.50–3	1.66–3	2.21–3	-3.87–3	
	3	2.48–3	-1.15–3	1.93–3	-1.06–3	-8.65–4		3	2.79–3	-1.29–3	1.97–3	-1.24–3	-7.32–4	
	5	-2.01–2	-3.05–3	4.57–3	7.73–3	-1.23–2		5	-1.80–2	-2.71–3	4.41–3	7.00–3	-1.14–2	
	10	-1.48–1	-2.73–2	1.70–2	5.18–2	-6.88–2		10	-1.44–1	-2.62–2	1.68–2	5.04–2	-6.72–2	
4f <sub>5/2</sub>	1	-2.92–3	7.80–4	-7.86–4	1.32–3	-5.35–4	4f <sub>5/2</sub>	1	-2.50–3	8.64–4	-7.54–4	1.19–3	-4.41–4	
	3	-5.71–2	-4.93–3	-3.25–3	2.02–2	-1.70–2		3	-5.50–2	-4.38–3	-3.26–3	1.96–2	-1.63–2	
	5	-1.45–1	-1.96–2	-4.88–3	4.92–2	-4.43–2		5	-1.42–1	-1.87–2	-4.83–3	4.83–2	-4.34–2	
	10	-3.96–1	-6.69–2	-1.50–2	1.28–1	-1.13–1		10	-3.91–1	-6.56–2	-1.44–2	1.27–1	-1.13–1	
4f <sub>7/2</sub>	1	-1.13–4	4.22–4	2.93–4	2.73–4	-5.65–4	4f <sub>7/2</sub>	1	3.46–4	5.03–4	3.38–4	1.30–4	-4.68–4	
	3	-5.00–2	-6.17–3	1.74–4	1.76–2	-1.77–2		3	-4.78–2	-5.62–3	1.73–4	1.69–2	-1.71–2	
	5	-1.34–1	-2.19–2	6.66–4	4.51–2	-4.57–2		5	-1.31–1	-2.11–2	7.57–4	4.41–2	-4.49–2	
	10	-3.79–1	-7.27–2	-7.15–3	1.21–1	-1.14–1		10	-3.74–1	-7.14–2	-6.45–3	1.20–1	-1.13–1	
5s <sub>1/2</sub>	1	3.19–3	8.01–3	1.29–3	2.19–3	-3.48–3	5s <sub>1/2</sub>	1	3.13–3	8.19–3	1.35–3	2.29–3	-3.64–3	
	3	-2.22–2	1.67–3	7.34–3	1.10–2	-1.83–2		3	-2.11–2	2.55–3	7.25–3	1.09–2	-1.82–2	
	5	-5.48–2	-1.32–2	1.31–2	1.93–2	-3.24–2		5	-5.48–2	-1.26–2	1.33–2	1.96–2	-3.29–2	
	10	-7.00–2	-2.93–2	1.32–2	1.89–2	-3.21–2		10	-7.33–2	-2.99–2	1.40–2	2.02–2	-3.41–2	
5p <sub>1/2</sub>	1	3.61–4	6.19–3	3.34–4	2.40–3	-2.73–3	5p <sub>1/2</sub>	1	9.22–4	6.62–3	3.54–4	2.35–3	-2.70–3	
	3	-2.99–2	-7.67–3	3.40–3	9.57–3	-1.30–2		3	-3.06–2	-7.53–3	3.58–3	9.93–3	-1.35–2	
	5	-2.65–2	-9.44–3	5.96–4	6.95–3	-7.55–3		5	-2.80–2	-9.83–3	9.02–4	7.46–3	-8.36–3	
	10	-2.82–2	-6.46–3	-2.10–3	8.28–3	-6.18–3		10	-2.73–2	-6.63–3	-2.34–3	7.82–3	-5.48–3	
5p <sub>3/2</sub>	1	-2.22–4	2.65–3	6.25–4	1.27–3	-1.90–3	5p <sub>3/2</sub>	1	2.59–4	2.91–3	6.00–4	1.18–3	-1.78–3	
	3	-2.24–2	-1.04–2	5.26–3	5.87–3	-1.11–2		3	-2.31–2	-1.05–2	5.40–3	6.13–3	-1.15–2	
	5	-1.60–2	-1.17–2	4.40–3	2.59–3	-6.99–3		5	-1.72–2	-1.22–2	4.67–3	2.93–3	-7.59–3	
	10	-2.41–2	-1.35–2	7.36–3	5.74–3	-1.31–2		10	-2.31–2	-1.36–2	7.04–3	5.21–3	-1.22–2	
5d <sub>3/2</sub>	1	-1.09–2	-3.55–3	4.67–4	3.05–3	-3.52–3	5d <sub>3/2</sub>	1	-1.13–2	-3.54–3	3.92–4	3.18–3	-3.57–3	
	3	-5.69–3	-1.49–3	-1.05–3	1.47–3	-4.20–4		3	-5.57–3	-1.66–3	-9.82–4	1.37–3	-3.84–4	
	5	-2.82–2	-2.15–3	-1.35–3	1.02–2	-8.80–3		5	-2.62–2	-1.92–3	-1.53–3	9.42–3	-7.89–3	
	10	-1.57–1	-2.24–2	7.38–3	5.55–2	-6.28–2		10	-1.52–1	-2.14–2	6.98–3	5.38–2	-6.08–2	
5d <sub>5/2</sub>	1	-8.15–3	-3.95–3	1.51–3	1.98–3	-3.49–3	5d <sub>5/2</sub>	1	-8.52–3	-3.97–3	1.46–3	2.11–3	-3.57–3	
	3	1.92–3	-2.03–3	2.04–3	-1.17–3	-8.68–4		3	2.11–3	-2.18–3	2.07–3	-1.30–3	-7.63–4	
	5	-1.75–2	-3.46–3	4.52–3	6.50–3	-1.10–2		5	-1.54–2	-3.17–3	4.35–3	5.78–3	-1.01–2	
	10	-1.41–1	-2.66–2	1.70–2	4.93–2	-6.64–2		10	-1.37–1	-2.55–2	1.68–2	4.78–2	-6.45–2	
6s <sub>1/2</sub>	1	2.79–3	7.41–3	1.24–3	2.10–3	-3.34–3	6s <sub>1/2</sub>	1	2.61–3	7.37–3	1.27–3	2.16–3	-3.43–3	
	3	-2.12–2	1.96–3	7.11–3	1.07–2	-1.78–2		3	-2.07–2	2.45–3	7.10–3	1.07–2	-1.78–2	
	5	-5.41–2	-1.30–2	1.30–2	1.91–2	-3.21–2		5	-5.44–2	-1.25–2	1.32–2	1.94–2	-3.26–2	
	10	-7.00–2	-2.92–2	1.31–2	1.89–2	-3.21–2		10	-7.32–2	-2.98–2	1.40–2	2.01–2	-3.41–2	
<i>Z</i> = 79, Au: 4f <sub>5/2</sub> <sup>6</sup> 4f <sub>7/2</sub> <sup>8</sup> 5d <sub>3/2</sub> <sup>4</sup> 5d <sub>5/2</sub> <sup>6</sup> 6s <sub>1/2</sub>	1	4.81–3	1.33–2	2.33–3	3.88–3	-6.21–3	<i>Z</i> = 80, Hg: 4f <sub>5/2</sub> <sup>6</sup> 4f <sub>7/2</sub> <sup>8</sup> 5d <sub>3/2</sub> <sup>4</sup> 5d <sub>5/2</sub> <sup>6</sup> 6s <sub>1/2</sub> <sup>2</sup>	4s <sub>1/2</sub>	1	4.75–3	1.38–2	2.47–3	4.12–3	-6.59–3
	3	-2.50–2	3.49–3	8.74–3	1.32–2	-2.19–2		3	-2.41–2	4.53–3	8.71–3	1.32–2	-2.19–2	
	5	-6.08–2	-1.32–2	1.50–2	2.20–2	-3.70–2		5	-6.09–2	-1.25–2	1.52–2	2.24–2	-3.76–2	
	10	-7.94–2	-3.14–2	1.54–2	2.23–2	-3.77–2		10	-8.29–2	-3.20–2	1.63–2	2.36–2	-3.99–2	
4p <sub>1/2</sub>	1	-2.13–3	8.37–3	4.26–5	4.21–3	-4.25–3	4p <sub>1/2</sub>	1	-1.66–3	8.97–3	3.44–5	4.26–3	-4.29–3	
	3	-3.65–2	-9.23–3	3.62–3	1.16–2	-1.53–2		3	-3.76–2	-9.20–3	3.80–3	1.21–2	-1.59–2	
	5	-3.09–2	-1.05–2	6.84–4	8.30–3	-8.98–3		5	-3.27–2	-1.10–2	9.90–4	8.88–3	-9.87–3	
	10	-2.77–2	-6.24–3	-2.82–3	8.02–3	-5.20–3		10	-2.71–2	-6.47–3	-3.02–3	7.67–3	-4.65–3	
4p <sub>3/2</sub>	1	-1.69–3	3.02–3	7.19–4	2.03–3	-2.75–3	4p <sub>3/2</sub>	1	-1.28–3	3.30–3	6.87–4	1.97–3	-2.66–3	
	3	-2.64–2	-1.21–2	5.96–3	6.91–3	-1.29–2		3	-2.73–2	-1.23–2	6.12–3	7.23–3	-1.33–2	
	5	-1.82–2	-1.28–2	4.98–3	3.12–3	-8.10–3		5	-1.95–2	-1.34–2	5.27–3	3.49–3	-8.76–3	
	10	-2.27–2	-1.34–2	7.03–3	5.14–3	-1.22–2		10	-2.19–2	-1.36–2	6.78–3	4.69–3	-1.15–2	
4d <sub>3/2</sub>	1	-1.51–2	-5.39–3	1.44–4	3.93–3	-4.07–3	4d <sub>3/2</sub>	1	-1.60–2	-5.62–3	5.53–5	4.15–3	-4.21–3	
	3	-5.55–3	-8.89–4	-1.46–3	1.57–3	-1.08–4		3	-5.55–3	-1.09–3	-1.41–3	1.50–3	-9.66–5	
	5	-2.76–2	-1.07–3	-2.04–3	1.02–2	-8.17–3		5	-2.59–2	-8.45–4	-2.22–3	9.59–3	-7.36–3	
	10	-1.56–1	-2.09–2	6.42–3	5.51–2	-6.16–2		10	-1.51–1	-2.00–2	5.99–3	5.37–2	-5.96–2	

(continued on next page)

Table 1 (continued)

Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$	Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$
4d <sub>5/2</sub>	1	-1.09–2	-5.74–3	1.63–3	2.41–3	-4.04–3	4d <sub>5/2</sub>	1	-1.17–2	-5.98–3	1.61–3	2.59–3	-4.21–3
	3	3.01–3	-1.45–3	2.02–3	-1.38–3	-6.34–4		3	3.16–3	-1.63–3	2.07–3	-1.50–3	-5.72–4
	5	-1.61–2	-2.40–3	4.27–3	6.32–3	-1.06–2		5	-1.43–2	-2.13–3	4.14–3	5.68–3	-9.82–3
	10	-1.39–1	-2.51–2	1.66–2	4.90–2	-6.55–2		10	-1.35–1	-2.41–2	1.63–2	4.76–2	-6.39–2
4f <sub>5/2</sub>	1	-2.05–3	9.69–4	-7.20–4	1.07–3	-3.45–4	4f <sub>5/2</sub>	1	-1.58–3	1.10–3	-6.86–4	9.33–4	-2.47–4
	3	-5.30–2	-3.88–3	-3.28–3	1.90–2	-1.57–2		3	-5.11–2	-3.39–3	-3.30–3	1.84–2	-1.51–2
	5	-1.39–1	-1.78–2	-4.80–3	4.73–2	-4.25–2		5	-1.35–1	-1.70–2	-4.78–3	4.64–2	-4.16–2
	10	-3.86–1	-6.43–2	-1.39–2	1.26–1	-1.12–1		10	-3.82–1	-6.31–2	-1.34–2	1.25–1	-1.11–1
4f <sub>7/2</sub>	1	8.38–4	6.06–4	3.85–4	-1.56–5	-3.70–4	4f <sub>7/2</sub>	1	1.37–3	7.33–4	4.35–4	-1.66–4	-2.70–4
	3	-4.58–2	-5.11–3	1.65–4	1.63–2	-1.65–2		3	-4.39–2	-4.62–3	1.61–4	1.57–2	-1.59–2
	5	-1.28–1	-2.02–2	8.36–4	4.32–2	-4.41–2		5	-1.25–1	-1.93–2	9.06–4	4.24–2	-4.33–2
	10	-3.70–1	-7.01–2	-5.78–3	1.19–1	-1.13–1		10	-3.65–1	-6.89–2	-5.13–3	1.18–1	-1.12–1
5s <sub>1/2</sub>	1	3.04–3	8.32–3	1.42–3	2.39–3	-3.81–3	5s <sub>1/2</sub>	1	2.96–3	8.50–3	1.49–3	2.51–3	-4.00–3
	3	-2.00–2	3.43–3	7.15–3	1.08–2	-1.79–2		3	-1.89–2	4.31–3	7.06–3	1.07–2	-1.78–2
	5	-5.46–2	-1.19–2	1.35–2	1.98–2	-3.33–2		5	-5.45–2	-1.11–2	1.36–2	2.01–2	-3.37–2
	10	-7.64–2	-3.04–2	1.48–2	2.14–2	-3.62–2		10	-7.96–2	-3.09–2	1.56–2	2.26–2	-3.82–2
5p <sub>1/2</sub>	1	1.40–3	6.99–3	3.87–4	2.31–3	-2.70–3	5p <sub>1/2</sub>	1	1.79–3	7.35–3	4.31–4	2.31–3	-2.74–3
	3	-3.11–2	-7.36–3	3.75–3	1.03–2	-1.40–2		3	-3.17–2	-7.16–3	3.90–3	1.06–2	-1.45–2
	5	-2.95–2	-1.02–2	1.22–3	7.98–3	-9.19–3		5	-3.10–2	-1.05–2	1.54–3	8.51–3	-1.00–2
	10	-2.66–2	-6.83–3	-2.54–3	7.42–3	-4.88–3		10	-2.61–2	-7.06–3	-2.70–3	7.09–3	-4.39–3
5p <sub>3/2</sub>	1	6.65–4	3.12–3	5.86–4	1.10–3	-1.69–3	5p <sub>3/2</sub>	1	1.00–3	3.32–3	5.81–4	1.04–3	-1.62–3
	3	-2.37–2	-1.06–2	5.53–3	6.38–3	-1.19–2		3	-2.43–2	-1.07–2	5.64–3	6.60–3	-1.22–2
	5	-1.84–2	-1.26–2	4.94–3	3.28–3	-8.21–3		5	-1.96–2	-1.31–2	5.22–3	3.63–3	-8.85–3
	10	-2.22–2	-1.37–2	6.75–3	4.74–3	-1.15–2		10	-2.15–2	-1.39–2	6.51–3	4.33–3	-1.08–2
5d <sub>3/2</sub>	1	-1.16–2	-3.55–3	3.21–4	3.29–3	-3.61–3	5d <sub>3/2</sub>	1	-1.19–2	-3.54–3	2.47–4	3.39–3	-3.63–3
	3	-5.65–3	-1.93–3	-8.76–4	1.31–3	-4.38–4		3	-5.75–3	-2.16–3	-7.86–4	1.28–3	-4.94–4
	5	-2.45–2	-1.76–3	-1.67–3	8.75–3	-7.08–3		5	-2.28–2	-1.63–3	-1.81–3	8.13–3	-6.32–3
	10	-1.47–1	-2.04–2	6.55–3	5.21–2	-5.87–2		10	-1.43–1	-1.94–2	6.12–3	5.05–2	-5.66–2
5d <sub>5/2</sub>	1	-8.90–3	-4.01–3	1.42–3	2.24–3	-3.66–3	5d <sub>5/2</sub>	1	-9.14–3	-4.00–3	1.37–3	2.33–3	-3.69–3
	3	2.09–3	-2.42–3	2.14–3	-1.38–3	-7.57–4		3	2.07–3	-2.62–3	2.18–3	-1.44–3	-7.45–4
	5	-1.36–2	-2.97–3	4.22–3	5.11–3	-9.34–3		5	-1.19–2	-2.77–3	4.09–3	4.48–3	-8.58–3
	10	-1.32–1	-2.44–2	1.65–2	4.62–2	-6.27–2		10	-1.27–1	-2.33–2	1.63–2	4.47–2	-6.09–2
6s <sub>1/2</sub>	1	2.67–3	7.58–3	1.31–3	2.23–3	-3.54–3	6s <sub>1/2</sub>	1	2.42–3	7.54–3	1.38–3	2.32–3	-3.70–3
	3	-1.91–2	3.61–3	6.91–3	1.05–2	-1.74–2		3	-1.84–2	4.18–3	6.86–3	1.04–2	-1.73–2
	5	-5.39–2	-1.16–2	1.33–2	1.96–2	-3.29–2		5	-5.37–2	-1.09–2	1.34–2	1.98–2	-3.32–2
	10	-7.63–2	-3.03–2	1.48–2	2.13–2	-3.61–2		10	-7.93–2	-3.08–2	1.56–2	2.25–2	-3.81–2
<i>Z = 81, Tl: 4f<sub>5/2</sub><sup>6</sup>4f<sub>7/2</sub><sup>8</sup>5d<sub>3/2</sub><sup>4</sup>5d<sub>5/2</sub><sup>6</sup>6s<sub>1/2</sub><sup>2</sup>6p<sub>1/2</sub><sup>1</sup></i>							<i>Z = 82, Pb: 4f<sub>5/2</sub><sup>6</sup>4f<sub>7/2</sub><sup>8</sup>5d<sub>3/2</sub><sup>4</sup>5d<sub>5/2</sub><sup>6</sup>6s<sub>1/2</sub><sup>2</sup>6p<sub>1/2</sub><sup>2</sup></i>						
4s <sub>1/2</sub>	1	4.61–3	1.42–2	2.64–3	4.38–3	-7.01–3	4s <sub>1/2</sub>	1	4.52–3	1.47–2	2.80–3	4.64–3	-7.44–3
	3	-2.31–2	5.57–3	8.69–3	1.32–2	-2.19–2		3	-2.21–2	6.66–3	8.67–3	1.32–2	-2.19–2
	5	-6.10–2	-1.17–2	1.55–2	2.28–2	-3.82–2		5	-6.10–2	-1.09–2	1.57–2	2.32–2	-3.89–2
	10	-8.63–2	-3.26–2	1.72–2	2.49–2	-4.22–2		10	-8.97–2	-3.30–2	1.81–2	2.63–2	-4.44–2
4p <sub>1/2</sub>	1	-1.27–3	9.58–3	3.21–5	4.35–3	-4.38–3	4p <sub>1/2</sub>	1	-8.83–4	1.02–2	4.63–5	4.45–3	-4.49–3
	3	-3.87–2	-9.15–3	3.98–3	1.26–2	-1.66–2		3	-3.97–2	-9.06–3	4.15–3	1.31–2	-1.73–2
	5	-3.46–2	-1.15–2	1.31–3	9.52–3	-1.08–2		5	-3.65–2	-1.19–2	1.64–3	1.02–2	-1.18–2
	10	-2.68–2	-6.73–3	-3.18–3	7.38–3	-4.21–3		10	-2.66–2	-7.03–3	-3.31–3	7.17–3	-3.86–3
4p <sub>3/2</sub>	1	-9.21–4	3.55–3	6.62–4	1.92–3	-2.58–3	4p <sub>3/2</sub>	1	-5.71–4	3.82–3	6.46–4	1.89–3	-2.53–3
	3	-2.83–2	-1.26–2	6.28–3	7.54–3	-1.38–2		3	-2.92–2	-1.28–2	6.44–3	7.85–3	-1.43–2
	5	-2.08–2	-1.39–2	5.58–3	3.88–3	-9.47–3		5	-2.22–2	-1.45–2	5.91–3	4.28–3	-1.02–2
	10	-2.12–2	-1.38–2	6.57–3	4.30–3	-1.09–2		10	-2.07–2	-1.40–2	6.41–3	3.95–3	-1.04–2
4d <sub>3/2</sub>	1	-1.68–2	-5.84–3	-4.23–5	4.36–3	-4.32–3	4d <sub>3/2</sub>	1	-1.76–2	-6.07–3	-1.47–4	4.58–3	-4.43–3
	3	-5.63–3	-1.31–3	-1.34–3	1.46–3	-1.18–4		3	-5.79–3	-1.56–3	-1.27–3	1.44–3	-1.71–4
	5	-2.42–2	-5.99–4	-2.39–3	8.96–3	-6.57–3		5	-2.27–2	-4.39–4	-2.54–3	8.40–3	-5.86–3
	10	-1.47–1	-1.90–2	5.53–3	5.22–2	-5.77–2		10	-1.42–1	-1.81–2	5.05–3	5.07–2	-5.58–2
4d <sub>5/2</sub>	1	-1.23–2	-6.21–3	1.58–3	2.77–3	-4.35–3	4d <sub>5/2</sub>	1	-1.31–2	-6.45–3	1.55–3	2.95–3	-4.50–3
	3	3.23–3	-1.82–3	2.13–3	-1.59–3	-5.39–4		3	3.23–3	-2.04–3	2.20–3	-1.67–3	-5.36–4
	5	-1.24–2	-1.84–3	4.03–3	5.03–3	-9.06–3		5	-1.08–2	-1.63–3	3.92–3	4.45–3	-8.37–3
	10	-1.30–1	-2.30–2	1.61–2	4.62–2	-6.23–2		10	-1.26–1	-2.20–2	1.58–2	4.48–2	-6.06–2

Table 1 (continued)

Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$	Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$
4f <sub>5/2</sub>	1	-1.20–3	1.21–3	-6.61–4	8.29–4	-1.69–4	4f <sub>5/2</sub>	1	-7.16–4	1.35–3	-6.27–4	7.02–4	-7.45–5
	3	-4.94–2	-2.94–3	-3.33–3	1.79–2	-1.46–2		3	-4.77–2	-2.47–3	-3.35–3	1.74–2	-1.41–2
	5	-1.33–1	-1.63–2	-4.81–3	4.56–2	-4.08–2		5	-1.30–1	-1.54–2	-4.81–3	4.48–2	-4.00–2
	10	-3.78–1	-6.19–2	-1.29–2	1.24–1	-1.11–1		10	-3.73–1	-6.07–2	-1.24–2	1.23–1	-1.10–1
4f <sub>7/2</sub>	1	1.81–3	8.36–4	4.81–4	-2.93–4	-1.88–4	4f <sub>7/2</sub>	1	2.36–3	9.80–4	5.37–4	-4.46–4	-9.12–5
	3	-4.22–2	-4.18–3	1.48–4	1.52–2	-1.54–2		3	-4.04–2	-3.71–3	1.46–4	1.47–2	-1.49–2
	5	-1.22–1	-1.86–2	9.26–4	4.16–2	-4.25–2		5	-1.19–1	-1.78–2	9.76–4	4.08–2	-4.17–2
	10	-3.61–1	-6.77–2	-4.50–3	1.17–1	-1.12–1		10	-3.57–1	-6.65–2	-3.89–3	1.15–1	-1.12–1
5s <sub>1/2</sub>	1	2.86–3	8.69–3	1.57–3	2.65–3	-4.22–3	5s <sub>1/2</sub>	1	2.76–3	8.86–3	1.64–3	2.77–3	-4.41–3
	3	-1.79–2	5.19–3	6.98–3	1.06–2	-1.76–2		3	-1.69–2	6.08–3	6.89–3	1.06–2	-1.74–2
	5	-5.42–2	-1.03–2	1.37–2	2.03–2	-3.41–2		5	-5.38–2	-9.47–3	1.39–2	2.05–2	-3.44–2
	10	-8.26–2	-3.13–2	1.64–2	2.38–2	-4.02–2		10	-8.56–2	-3.17–2	1.72–2	2.50–2	-4.23–2
5p <sub>1/2</sub>	1	2.14–3	7.72–3	4.89–4	2.33–3	-2.82–3	5p <sub>1/2</sub>	1	2.48–3	8.10–3	5.60–4	2.36–3	-2.92–3
	3	-3.22–2	-6.95–3	4.05–3	1.09–2	-1.50–2		3	-3.27–2	-6.68–3	4.20–3	1.12–2	-1.54–2
	5	-3.26–2	-1.09–2	1.87–3	9.08–3	-1.09–2		5	-3.42–2	-1.12–2	2.21–3	9.65–3	-1.19–2
	10	-2.58–2	-7.34–3	-2.82–3	6.83–3	-4.01–3		10	-2.57–2	-7.66–3	-2.91–3	6.64–3	-3.73–3
5p <sub>3/2</sub>	1	1.31–3	3.50–3	5.85–4	9.94–4	-1.58–3	5p <sub>3/2</sub>	1	1.59–3	3.68–3	5.95–4	9.54–4	-1.55–3
	3	-2.49–2	-1.07–2	5.75–3	6.83–3	-1.26–2		3	-2.55–2	-1.08–2	5.85–3	7.04–3	-1.29–2
	5	-2.08–2	-1.35–2	5.51–3	4.00–3	-9.50–3		5	-2.21–2	-1.40–2	5.81–3	4.39–3	-1.02–2
	10	-2.09–2	-1.41–2	6.32–3	3.96–3	-1.03–2		10	-2.04–2	-1.44–2	6.16–3	3.64–3	-9.80–3
5d <sub>3/2</sub>	1	-1.22–2	-3.54–3	1.74–4	3.49–3	-3.66–3	5d <sub>3/2</sub>	1	-1.24–2	-3.52–3	9.75–5	3.57–3	-3.67–3
	3	-6.00–3	-2.45–3	-6.74–4	1.29–3	-6.11–4		3	-6.27–3	-2.72–3	-5.63–4	1.30–3	-7.42–4
	5	-2.14–2	-1.54–3	-1.92–3	7.56–3	-5.63–3		5	-1.99–2	-1.44–3	-2.03–3	6.98–3	-4.95–3
	10	-1.38–1	-1.85–2	5.67–3	4.89–2	-5.46–2		10	-1.33–1	-1.76–2	5.19–3	4.73–2	-5.25–2
5d <sub>5/2</sub>	1	-9.46–3	-4.04–3	1.33–3	2.43–3	-3.76–3	5d <sub>5/2</sub>	1	-9.71–3	-4.05–3	1.28–3	2.52–3	-3.80–3
	3	1.90–3	-2.89–3	2.26–3	-1.46–3	-8.00–4		3	1.71–3	-3.14–3	2.33–3	-1.47–3	-8.61–4
	5	-1.04–2	-2.64–3	3.99–3	3.91–3	-7.90–3		5	-8.83–3	-2.47–3	3.89–3	3.32–3	-7.21–3
	10	-1.22–1	-2.23–2	1.60–2	4.32–2	-5.92–2		10	-1.18–1	-2.13–2	1.57–2	4.17–2	-5.74–2
6s <sub>1/2</sub>	1	2.42–3	7.71–3	1.43–3	2.40–3	-3.83–3	6s <sub>1/2</sub>	1	2.33–3	7.82–3	1.48–3	2.49–3	-3.98–3
	3	-1.68–2	5.26–3	6.67–3	1.02–2	-1.68–2		3	-1.60–2	5.96–3	6.59–3	1.01–2	-1.67–2
	5	-5.31–2	-1.00–2	1.35–2	1.99–2	-3.34–2		5	-5.26–2	-9.21–3	1.36–2	2.01–2	-3.36–2
	10	-8.22–2	-3.11–2	1.63–2	2.37–2	-4.00–2		10	-8.50–2	-3.15–2	1.71–2	2.49–2	-4.20–2
6p <sub>1/2</sub>	1	2.48–3	7.48–3	5.74–4	2.11–3	-2.69–3	6p <sub>1/2</sub>	1	3.00–3	7.87–3	6.34–4	2.08–3	-2.71–3
	3	-3.12–2	-6.46–3	4.06–3	1.07–2	-1.48–2		3	-3.18–2	-6.35–3	4.25–3	1.10–2	-1.53–2
	5	-3.26–2	-1.08–2	1.98–3	9.09–3	-1.11–2		5	-3.41–2	-1.11–2	2.33–3	9.65–3	-1.20–2
	10	-2.58–2	-7.47–3	-2.79–3	6.76–3	-3.97–3		10	-2.56–2	-7.78–3	-2.85–3	6.56–3	-3.71–3
$Z = 83, \text{Bi}: 4f_{5/2}^6 4f_{7/2}^8 5d_{3/2}^4 5d_{5/2}^6 6s_{1/2}^2 6p_{1/2}^2 6p_{3/2}^1$							$Z = 84, \text{Po}: 4f_{5/2}^6 4f_{7/2}^8 5d_{3/2}^4 5d_{5/2}^6 6s_{1/2}^2 6p_{1/2}^2 6p_{3/2}^2$						
4s <sub>1/2</sub>	1	4.35–3	1.52–2	2.97–3	4.92–3	-7.89–3	4s <sub>1/2</sub>	1	4.15–3	1.56–2	3.16–3	5.23–3	-8.39–3
	3	-2.10–2	7.77–3	8.65–3	1.32–2	-2.19–2		3	-1.99–2	8.92–3	8.62–3	1.33–2	-2.19–2
	5	-6.08–2	-9.97–3	1.59–2	2.35–2	-3.94–2		5	-6.06–2	-8.99–3	1.61–2	2.39–2	-3.99–2
	10	-9.31–2	-3.35–2	1.90–2	2.76–2	-4.67–2		10	-9.64–2	-3.38–2	2.00–2	2.90–2	-4.90–2
4p <sub>1/2</sub>	1	-5.44–4	1.08–2	6.61–5	4.56–3	-4.63–3	4p <sub>1/2</sub>	1	-2.30–4	1.14–2	9.56–5	4.69–3	-4.78–3
	3	-4.07–2	-8.93–3	4.31–3	1.36–2	-1.79–2		3	-4.17–2	-8.74–3	4.46–3	1.41–2	-1.85–2
	5	-3.84–2	-1.23–2	1.98–3	1.08–2	-1.28–2		5	-4.04–2	-1.27–2	2.33–3	1.15–2	-1.38–2
	10	-2.66–2	-7.37–3	-3.40–3	7.01–3	-3.61–3		10	-2.68–2	-7.75–3	-3.45–3	6.92–3	-3.47–3
4p <sub>3/2</sub>	1	-2.41–4	4.06–3	6.30–4	1.85–3	-2.48–3	4p <sub>3/2</sub>	1	7.94–5	4.28–3	6.14–4	1.80–3	-2.42–3
	3	-3.01–2	-1.30–2	6.58–3	8.14–3	-1.47–2		3	-3.08–2	-1.31–2	6.69–3	8.40–3	-1.51–2
	5	-2.36–2	-1.50–2	6.23–3	4.69–3	-1.09–2		5	-2.50–2	-1.55–2	6.55–3	5.10–3	-1.17–2
	10	-2.03–2	-1.43–2	6.28–3	3.64–3	-9.91–3		10	-1.99–2	-1.46–2	6.18–3	3.37–3	-9.55–3
4d <sub>3/2</sub>	1	-1.84–2	-6.29–3	-2.61–4	4.79–3	-4.53–3	4d <sub>3/2</sub>	1	-1.92–2	-6.50–3	-3.86–4	4.99–3	-4.60–3
	3	-6.01–3	-1.82–3	-1.19–3	1.44–3	-2.53–4		3	-6.31–3	-2.10–3	-1.10–3	1.46–3	-3.64–4
	5	-2.13–2	-3.10–4	-2.68–3	7.88–3	-5.19–3		5	-2.00–2	-2.09–4	-2.80–3	7.38–3	-4.57–3
	10	-1.38–1	-1.71–2	4.56–3	4.93–2	-5.38–2		10	-1.34–1	-1.62–2	4.05–3	4.78–2	-5.19–2
4d <sub>5/2</sub>	1	-1.37–2	-6.69–3	1.51–3	3.12–3	-4.64–3	4d <sub>5/2</sub>	1	-1.44–2	-6.93–3	1.47–3	3.30–3	-4.77–3
	3	3.16–3	-2.27–3	2.28–3	-1.72–3	-5.59–4		3	3.03–3	-2.53–3	2.36–3	-1.75–3	-6.08–4
	5	-9.29–3	-1.46–3	3.83–3	3.90–3	-7.73–3		5	-7.86–3	-1.31–3	3.75–3	3.37–3	-7.12–3
	10	-1.22–1	-2.10–2	1.56–2	4.34–2	-5.90–2		10	-1.18–1	-2.00–2	1.53–2	4.21–2	-5.74–2

(continued on next page)

Table 1 (continued)

Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$	Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$
4f <sub>5/2</sub>	1	-2.78–4	1.49–3	-5.97–4	5.87–4	1.03–5	4f <sub>5/2</sub>	1	1.65–4	1.62–3	-5.64–4	4.70–4	9.41–5
	3	-4.61–2	-2.04–3	-3.37–3	1.69–2	-1.36–2		3	-4.44–2	-1.57–3	-3.39–3	1.64–2	-1.30–2
	5	-1.27–1	-1.46–2	-4.82–3	4.40–2	-3.92–2		5	-1.24–1	-1.38–2	-4.83–3	4.32–2	-3.83–2
	10	-3.69–1	-5.94–2	-1.20–2	1.21–1	-1.09–1		10	-3.65–1	-5.82–2	-1.16–2	1.20–1	-1.09–1
4f <sub>7/2</sub>	1	2.86–3	1.11–3	5.89–4	-5.86–4	-3.30–6	4f <sub>7/2</sub>	1	3.38–3	1.24–3	6.44–4	-7.28–4	8.37–5
	3	-3.88–2	-3.28–3	1.35–4	1.42–2	-1.44–2		3	-3.70–2	-2.81–3	1.35–4	1.37–2	-1.38–2
	5	-1.16–1	-1.70–2	1.02–3	3.99–2	-4.09–2		5	-1.13–1	-1.62–2	1.06–3	3.91–2	-4.02–2
	10	-3.53–1	-6.52–2	-3.31–3	1.14–1	-1.11–1		10	-3.49–1	-6.40–2	-2.74–3	1.13–1	-1.11–1
5s <sub>1/2</sub>	1	2.63–3	9.01–3	1.72–3	2.90–3	-4.62–3	5s <sub>1/2</sub>	1	2.48–3	9.19–3	1.82–3	3.04–3	-4.86–3
	3	-1.58–2	6.97–3	6.80–3	1.05–2	-1.73–2		3	-1.47–2	7.89–3	6.72–3	1.04–2	-1.71–2
	5	-5.33–2	-8.57–3	1.39–2	2.07–2	-3.46–2		5	-5.27–2	-7.61–3	1.40–2	2.09–2	-3.49–2
	10	-8.85–2	-3.19–2	1.80–2	2.62–2	-4.42–2		10	-9.13–2	-3.22–2	1.88–2	2.74–2	-4.63–2
5p <sub>1/2</sub>	1	2.78–3	8.47–3	6.44–4	2.41–3	-3.05–3	5p <sub>1/2</sub>	1	3.05–3	8.83–3	7.41–4	2.46–3	-3.20–3
	3	-3.31–2	-6.38–3	4.33–3	1.15–2	-1.59–2		3	-3.34–2	-6.03–3	4.45–3	1.18–2	-1.63–2
	5	-3.58–2	-1.15–2	2.55–3	1.02–2	-1.28–2		5	-3.74–2	-1.17–2	2.90–3	1.08–2	-1.37–2
	10	-2.58–2	-8.01–3	-2.96–3	6.52–3	-3.56–3		10	-2.60–2	-8.39–3	-2.97–3	6.45–3	-3.49–3
5p <sub>3/2</sub>	1	1.86–3	3.85–3	6.09–4	9.16–4	-1.53–3	5p <sub>3/2</sub>	1	2.11–3	4.00–3	6.29–4	8.82–4	-1.51–3
	3	-2.60–2	-1.08–2	5.93–3	7.24–3	-1.32–2		3	-2.64–2	-1.09–2	6.00–3	7.42–3	-1.34–2
	5	-2.33–2	-1.44–2	6.10–3	4.77–3	-1.09–2		5	-2.46–2	-1.49–2	6.40–3	5.16–3	-1.16–2
	10	-2.01–2	-1.47–2	6.05–3	3.37–3	-9.42–3		10	-1.99–2	-1.50–2	5.97–3	3.14–3	-9.11–3
5d <sub>3/2</sub>	1	-1.26–2	-3.49–3	1.51–5	3.64–3	-3.66–3	5d <sub>3/2</sub>	1	-1.27–2	-3.44–3	-7.16–5	3.70–3	-3.63–3
	3	-6.61–3	-3.02–3	-4.45–4	1.35–3	-9.04–4		3	-7.02–3	-3.33–3	-3.17–4	1.41–3	-1.10–3
	5	-1.87–2	-1.41–3	-2.11–3	6.47–3	-4.36–3		5	-1.75–2	-1.41–3	-2.18–3	6.00–3	-3.81–3
	10	-1.29–1	-1.67–2	4.71–3	4.57–2	-5.04–2		10	-1.24–1	-1.58–2	4.21–3	4.42–2	-4.84–2
5d <sub>5/2</sub>	1	-9.93–3	-4.04–3	1.23–3	2.60–3	-3.83–3	5d <sub>5/2</sub>	1	-1.01–2	-4.02–3	1.18–3	2.67–3	-3.84–3
	3	1.45–3	-3.41–3	2.42–3	-1.46–3	-9.54–4		3	1.11–3	-3.71–3	2.50–3	-1.43–3	-1.08–3
	5	-7.49–3	-2.39–3	3.81–3	2.80–3	-6.61–3		5	-6.25–3	-2.34–3	3.73–3	2.31–3	-6.04–3
	10	-1.13–1	-2.03–2	1.54–2	4.02–2	-5.56–2		10	-1.09–1	-1.94–2	1.51–2	3.87–2	-5.39–2
6s <sub>1/2</sub>	1	2.16–3	7.85–3	1.54–3	2.58–3	-4.12–3	6s <sub>1/2</sub>	1	1.97–3	7.89–3	1.61–3	2.69–3	-4.29–3
	3	-1.51–2	6.70–3	6.50–3	1.00–2	-1.65–2		3	-1.40–2	7.58–3	6.39–3	9.89–3	-1.63–2
	5	-5.19–2	-8.27–3	1.36–2	2.02–2	-3.38–2		5	-5.13–2	-7.31–3	1.36–2	2.03–2	-3.39–2
	10	-8.78–2	-3.17–2	1.79–2	2.60–2	-4.39–2		10	-9.05–2	-3.19–2	1.87–2	2.72–2	-4.58–2
6p <sub>1/2</sub>	1	3.20–3	8.05–3	7.32–4	2.09–3	-2.82–3	6p <sub>1/2</sub>	1	3.35–3	8.25–3	8.46–4	2.13–3	-2.97–3
	3	-3.22–2	-6.13–3	4.40–3	1.13–2	-1.57–2		3	-3.23–2	-5.68–3	4.49–3	1.15–2	-1.60–2
	5	-3.54–2	-1.13–2	2.67–3	1.02–2	-1.29–2		5	-3.70–2	-1.16–2	3.03–3	1.08–2	-1.38–2
	10	-2.57–2	-8.14–3	-2.89–3	6.44–3	-3.55–3		10	-2.59–2	-8.53–3	-2.88–3	6.38–3	-3.50–3
6p <sub>3/2</sub>	1	2.35–3	3.92–3	5.97–4	7.49–4	-1.35–3	6p <sub>3/2</sub>	1	2.48–3	3.99–3	6.31–4	7.29–4	-1.36–3
	3	-2.58–2	-1.07–2	5.91–3	7.21–3	-1.31–2		3	-2.60–2	-1.06–2	5.94–3	7.34–3	-1.33–2
	5	-2.33–2	-1.44–2	6.12–3	4.81–3	-1.09–2		5	-2.46–2	-1.48–2	6.41–3	5.19–3	-1.16–2
	10	-2.01–2	-1.48–2	6.02–3	3.31–3	-9.33–3		10	-1.99–2	-1.51–2	5.94–3	3.09–3	-9.03–3
<i>Z</i> = 85, At: 4f <sub>5/2</sub> <sup>6</sup> 4f <sub>7/2</sub> <sup>8</sup> 5d <sub>3/2</sub> <sup>4</sup> 5d <sub>5/2</sub> <sup>6</sup> 6s <sub>1/2</sub> <sup>2</sup> 6p <sub>1/2</sub> <sup>2</sup> 6p <sub>3/2</sub> <sup>3</sup>							<i>Z</i> = 86, Rn: 4f <sub>5/2</sub> <sup>6</sup> 4f <sub>7/2</sub> <sup>8</sup> 5d <sub>3/2</sub> <sup>4</sup> 5d <sub>5/2</sub> <sup>6</sup> 6s <sub>1/2</sub> <sup>2</sup> 6p <sub>1/2</sub> <sup>2</sup> 6p <sub>3/2</sub> <sup>4</sup>						
4s <sub>1/2</sub>	1	3.89–3	1.60–2	3.36–3	5.54–3	-8.90–3	4s <sub>1/2</sub>	1	3.59–3	1.65–2	3.58–3	5.88–3	-9.46–3
	3	-1.88–2	1.01–2	8.59–3	1.33–2	-2.19–2		3	-1.76–2	1.13–2	8.56–3	1.33–2	-2.19–2
	5	-6.02–2	-7.94–3	1.62–2	2.41–2	-4.04–2		5	-5.98–2	-6.83–3	1.64–2	2.45–2	-4.08–2
	10	-9.95–2	-3.40–2	2.08–2	3.04–2	-5.12–2		10	-1.03–1	-3.42–2	2.17–2	3.17–2	-5.35–2
4p <sub>1/2</sub>	1	5.57–5	1.21–2	1.35–4	4.83–3	-4.96–3	4p <sub>1/2</sub>	1	3.09–4	1.27–2	1.86–4	4.99–3	-5.18–3
	3	-4.25–2	-8.51–3	4.59–3	1.45–2	-1.91–2		3	-4.33–2	-8.23–3	4.73–3	1.50–2	-1.97–2
	5	-4.23–2	-1.31–2	2.68–3	1.22–2	-1.49–2		5	-4.43–2	-1.34–2	3.04–3	1.29–2	-1.60–2
	10	-2.71–2	-8.16–3	-3.47–3	6.89–3	-3.42–3		10	-2.77–2	-8.60–3	-3.45–3	6.93–3	-3.48–3
4p <sub>3/2</sub>	1	3.89–4	4.50–3	6.04–4	1.77–3	-2.37–3	4p <sub>3/2</sub>	1	6.86–4	4.72–3	5.96–4	1.73–3	-2.33–3
	3	-3.16–2	-1.33–2	6.80–3	8.66–3	-1.55–2		3	-3.22–2	-1.34–2	6.89–3	8.91–3	-1.58–2
	5	-2.64–2	-1.61–2	6.88–3	5.53–3	-1.24–2		5	-2.78–2	-1.66–2	7.21–3	5.94–3	-1.32–2
	10	-1.98–2	-1.49–2	6.13–3	3.15–3	-9.27–3		10	-1.97–2	-1.53–2	6.11–3	2.96–3	-9.08–3
4d <sub>3/2</sub>	1	-1.99–2	-6.71–3	-5.21–4	5.19–3	-4.67–3	4d <sub>3/2</sub>	1	-2.07–2	-6.90–3	-6.65–4	5.38–3	-4.71–3
	3	-6.67–3	-2.40–3	-1.00–3	1.51–3	-5.02–4		3	-7.10–3	-2.72–3	-9.04–4	1.57–3	-6.66–4
	5	-1.88–2	-1.37–4	-2.91–3	6.90–3	-3.99–3		5	-1.78–2	-1.32–4	-3.00–3	6.48–3	-3.49–3
	10	-1.30–1	-1.53–2	3.52–3	4.64–2	-4.99–2		10	-1.25–1	-1.45–2	2.99–3	4.50–2	-4.80–2

Table 1 (continued)

Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$	Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$
4d <sub>5/2</sub>	1	-1.51–2	-7.15–3	1.42–3	3.46–3	-4.88–3	4d <sub>5/2</sub>	1	-1.57–2	-7.37–3	1.36–3	3.62–3	-4.98–3
	3	2.83–3	-2.80–3	2.45–3	-1.76–3	-6.82–4		3	2.58–3	-3.09–3	2.54–3	-1.76–3	-7.80–4
	5	-6.52–3	-1.19–3	3.68–3	2.87–3	-6.54–3		5	-5.38–3	-1.14–3	3.61–3	2.42–3	-6.04–3
	10	-1.13–1	-1.90–2	1.50–2	4.07–2	-5.57–2		10	-1.09–1	-1.81–2	1.47–2	3.94–2	-5.41–2
4f <sub>5/2</sub>	1	6.14–4	1.76–3	-5.31–4	3.54–4	1.77–4	4f <sub>5/2</sub>	1	1.07–3	1.91–3	-4.96–4	2.37–4	2.59–4
	3	-4.27–2	-1.11–3	-3.41–3	1.60–2	-1.26–2		3	-4.11–2	-6.45–4	-3.42–3	1.55–2	-1.21–2
	5	-1.21–1	-1.31–2	-4.85–3	4.24–2	-3.75–2		5	-1.18–1	-1.22–2	-4.83–3	4.15–2	-3.67–2
	10	-3.60–1	-5.69–2	-1.12–2	1.19–1	-1.08–1		10	-3.56–1	-5.56–2	-1.09–2	1.18–1	-1.07–1
4f <sub>7/2</sub>	1	3.91–3	1.38–3	7.05–4	-8.75–4	1.70–4	4f <sub>7/2</sub>	1	4.45–3	1.51–3	7.66–4	-1.02–3	2.56–4
	3	-3.54–2	-2.35–3	1.37–4	1.32–2	-1.34–2		3	-3.37–2	-1.89–3	1.39–4	1.27–2	-1.29–2
	5	-1.11–1	-1.54–2	1.09–3	3.83–2	-3.94–2		5	-1.08–1	-1.45–2	1.16–3	3.75–2	-3.87–2
	10	-3.45–1	-6.27–2	-2.20–3	1.12–1	-1.10–1		10	-3.40–1	-6.14–2	-1.69–3	1.11–1	-1.09–1
5s <sub>1/2</sub>	1	2.31–3	9.35–3	1.91–3	3.20–3	-5.11–3	5s <sub>1/2</sub>	1	2.12–3	9.52–3	2.02–3	3.37–3	-5.38–3
	3	-1.36–2	8.81–3	6.63–3	1.03–2	-1.69–2		3	-1.26–2	9.76–3	6.55–3	1.02–2	-1.68–2
	5	-5.20–2	-6.59–3	1.41–2	2.10–2	-3.51–2		5	-5.13–2	-5.52–3	1.41–2	2.11–2	-3.53–2
	10	-9.40–2	-3.23–2	1.96–2	2.86–2	-4.83–2		10	-9.67–2	-3.24–2	2.04–2	2.98–2	-5.02–2
5p <sub>1/2</sub>	1	3.28–3	9.18–3	8.51–4	2.53–3	-3.38–3	5p <sub>1/2</sub>	1	3.50–3	9.54–3	9.78–4	2.61–3	-3.59–3
	3	-3.36–2	-5.63–3	4.56–3	1.21–2	-1.67–2		3	-3.38–2	-5.19–3	4.66–3	1.24–2	-1.70–2
	5	-3.89–2	-1.19–2	3.26–3	1.15–2	-1.47–2		5	-4.04–2	-1.21–2	3.62–3	1.21–2	-1.57–2
	10	-2.64–2	-8.81–3	-2.93–3	6.46–3	-3.53–3		10	-2.70–2	-9.26–3	-2.86–3	6.53–3	-3.67–3
5p <sub>3/2</sub>	1	2.34–3	4.14–3	6.51–4	8.51–4	-1.50–3	5p <sub>3/2</sub>	1	2.56–3	4.29–3	6.81–4	8.26–4	-1.51–3
	3	-2.68–2	-1.09–2	6.05–3	7.58–3	-1.36–2		3	-2.71–2	-1.09–2	6.10–3	7.74–3	-1.38–2
	5	-2.58–2	-1.53–2	6.70–3	5.54–3	-1.22–2		5	-2.70–2	-1.57–2	6.99–3	5.92–3	-1.29–2
	10	-1.98–2	-1.54–2	5.94–3	2.95–3	-8.89–3		10	-1.98–2	-1.58–2	5.95–3	2.81–3	-8.76–3
5d <sub>3/2</sub>	1	-1.28–2	-3.38–3	-1.62–4	3.76–3	-3.59–3	5d <sub>3/2</sub>	1	-1.29–2	-3.30–3	-2.54–4	3.80–3	-3.54–3
	3	-7.49–3	-3.65–3	-1.84–4	1.50–3	-1.32–3		3	-8.02–3	-3.99–3	-4.62–5	1.60–3	-1.56–3
	5	-1.64–2	-1.44–3	-2.24–3	5.55–3	-3.32–3		5	-1.56–2	-1.53–3	-2.27–3	5.16–3	-2.90–3
	10	-1.20–1	-1.50–2	3.71–3	4.26–2	-4.63–2		10	-1.15–1	-1.42–2	3.20–3	4.11–2	-4.43–2
5d <sub>5/2</sub>	1	-1.02–2	-3.98–3	1.12–3	2.72–3	-3.84–3	5d <sub>5/2</sub>	1	-1.04–2	-3.94–3	1.06–3	2.78–3	-3.84–3
	3	7.16–4	-4.01–3	2.59–3	-1.37–3	-1.22–3		3	2.62–4	-4.33–3	2.69–3	-1.30–3	-1.39–3
	5	-5.11–3	-2.32–3	3.67–3	1.85–3	-5.52–3		5	-4.15–3	-2.35–3	3.61–3	1.44–3	-5.06–3
	10	-1.04–1	-1.85–2	1.48–2	3.73–2	-5.21–2		10	-9.99–2	-1.76–2	1.45–2	3.59–2	-5.04–2
6s <sub>1/2</sub>	1	1.80–3	7.97–3	1.68–3	2.80–3	-4.48–3	6s <sub>1/2</sub>	1	1.62–3	8.07–3	1.76–3	2.93–3	-4.69–3
	3	-1.29–2	8.43–3	6.29–3	9.79–3	-1.61–2		3	-1.18–2	9.32–3	6.19–3	9.69–3	-1.59–2
	5	-5.05–2	-6.31–3	1.37–2	2.04–2	-3.41–2		5	-4.97–2	-5.27–3	1.37–2	2.05–2	-3.42–2
	10	-9.31–2	-3.20–2	1.94–2	2.83–2	-4.78–2		10	-9.57–2	-3.21–2	2.02–2	2.95–2	-4.97–2
6p <sub>1/2</sub>	1	3.53–3	8.49–3	9.68–4	2.18–3	-3.15–3	6p <sub>1/2</sub>	1	3.68–3	8.71–3	1.10–3	2.23–3	-3.34–3
	3	-3.24–2	-5.27–3	4.60–3	1.18–2	-1.64–2		3	-3.24–2	-4.76–3	4.68–3	1.20–2	-1.67–2
	5	-3.85–2	-1.17–2	3.39–3	1.14–2	-1.48–2		5	-3.99–2	-1.19–2	3.76–3	1.20–2	-1.57–2
	10	-2.64–2	-8.97–3	-2.84–3	6.40–3	-3.56–3		10	-2.70–2	-9.42–3	-2.75–3	6.47–3	-3.73–3
6p <sub>3/2</sub>	1	2.68–3	4.09–3	6.58–4	6.98–4	-1.36–3	6p <sub>3/2</sub>	1	2.86–3	4.21–3	6.90–4	6.76–4	-1.37–3
	3	-2.63–2	-1.06–2	5.98–3	7.49–3	-1.35–2		3	-2.66–2	-1.05–2	6.01–3	7.61–3	-1.36–2
	5	-2.58–2	-1.52–2	6.70–3	5.58–3	-1.23–2		5	-2.71–2	-1.56–2	7.00–3	5.98–3	-1.30–2
	10	-1.98–2	-1.55–2	5.91–3	2.92–3	-8.83–3		10	-1.99–2	-1.59–2	5.93–3	2.78–3	-8.71–3
<i>Z = 87, Fr: 7s<sub>1/2</sub></i>							<i>Z = 88, Ra: 7s<sub>1/2</sub></i>						
4s <sub>1/2</sub>	1	3.20–3	1.69–2	3.83–3	6.27–3	-1.01–2	4s <sub>1/2</sub>	1	2.86–3	1.74–2	4.07–3	6.64–3	-1.07–2
	3	-1.66–2	1.25–2	8.55–3	1.33–2	-2.19–2		3	-1.55–2	1.38–2	8.55–3	1.34–2	-2.19–2
	5	-5.93–2	-5.68–3	1.65–2	2.47–2	-4.13–2		5	-5.87–2	-4.47–3	1.67–2	2.50–2	-4.17–2
	10	-1.06–1	-3.43–2	2.26–2	3.31–2	-5.57–2		10	-1.09–1	-3.43–2	2.35–2	3.44–2	-5.79–2
4p <sub>1/2</sub>	1	4.33–4	1.33–2	2.33–4	5.19–3	-5.42–3	4p <sub>1/2</sub>	1	5.53–4	1.40–2	2.97–4	5.43–3	-5.72–3
	3	-4.41–2	-7.93–3	4.84–3	1.54–2	-2.03–2		3	-4.49–2	-7.60–3	4.97–3	1.59–2	-2.09–2
	5	-4.63–2	-1.38–2	3.40–3	1.37–2	-1.71–2		5	-4.84–2	-1.41–2	3.77–3	1.45–2	-1.82–2
	10	-2.84–2	-9.07–3	-3.39–3	7.04–3	-3.65–3		10	-2.92–2	-9.57–3	-3.30–3	7.21–3	-3.91–3
4p <sub>3/2</sub>	1	8.92–4	4.87–3	5.88–4	1.71–3	-2.30–3	4p <sub>3/2</sub>	1	1.08–3	5.05–3	5.86–4	1.70–3	-2.29–3
	3	-3.29–2	-1.35–2	6.98–3	9.14–3	-1.61–2		3	-3.36–2	-1.37–2	7.06–3	9.37–3	-1.64–2
	5	-2.92–2	-1.71–2	7.55–3	6.37–3	-1.39–2		5	-3.07–2	-1.76–2	7.88–3	6.81–3	-1.47–2
	10	-1.97–2	-1.57–2	6.14–3	2.83–3	-8.97–3		10	-1.99–2	-1.62–2	6.21–3	2.73–3	-8.94–3

(continued on next page)

Table 1 (continued)

Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$	Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$
4d <sub>3/2</sub>	1	-2.14-2	-7.11-3	-8.07-4	5.55-3	-4.74-3	4d <sub>3/2</sub>	1	-2.21-2	-7.32-3	-9.50-4	5.74-3	-4.79-3
	3	-7.56-3	-3.04-3	-8.05-4	1.65-3	-8.44-4		3	-8.10-3	-3.38-3	-7.03-4	1.75-3	-1.05-3
	5	-1.68-2	-7.58-5	-3.08-3	6.06-3	-2.98-3		5	-1.59-2	-8.16-5	-3.14-3	5.68-3	-2.54-3
	10	-1.21-1	-1.36-2	2.45-3	4.36-2	-4.60-2		10	-1.17-1	-1.28-2	1.91-3	4.22-2	-4.41-2
4d <sub>5/2</sub>	1	-1.64-2	-7.60-3	1.32-3	3.76-3	-5.08-3	4d <sub>5/2</sub>	1	-1.70-2	-7.83-3	1.27-3	3.91-3	-5.18-3
	3	2.28-3	-3.38-3	2.63-3	-1.74-3	-8.94-4		3	1.93-3	-3.69-3	2.73-3	-1.70-3	-1.03-3
	5	-4.12-3	-1.02-3	3.57-3	1.95-3	-5.53-3		5	-3.05-3	-9.76-4	3.54-3	1.54-3	-5.07-3
	10	-1.05-1	-1.72-2	1.44-2	3.81-2	-5.25-2		10	-1.01-1	-1.63-2	1.42-2	3.68-2	-5.09-2
4f <sub>5/2</sub>	1	1.44-3	2.03-3	-4.68-4	1.42-4	3.26-4	4f <sub>5/2</sub>	1	1.89-3	2.19-3	-4.34-4	3.09-5	4.03-4
	3	-3.96-2	-2.13-4	-3.43-3	1.51-2	-1.16-2		3	-3.80-2	2.42-4	-3.45-3	1.46-2	-1.12-2
	5	-1.16-1	-1.14-2	-4.87-3	4.07-2	-3.59-2		5	-1.13-1	-1.07-2	-4.89-3	4.00-2	-3.51-2
	10	-3.52-1	-5.44-2	-1.05-2	1.17-1	-1.06-1		10	-3.47-1	-5.31-2	-1.02-2	1.16-1	-1.05-1
4f <sub>7/2</sub>	1	4.89-3	1.63-3	8.16-4	-1.14-3	3.25-4	4f <sub>7/2</sub>	1	5.42-3	1.78-3	8.76-4	-1.28-3	4.05-4
	3	-3.21-2	-1.46-3	1.41-4	1.23-2	-1.24-2		3	-3.05-2	-1.01-3	1.46-4	1.18-2	-1.20-2
	5	-1.05-1	-1.38-2	1.17-3	3.67-2	-3.79-2		5	-1.02-1	-1.30-2	1.19-3	3.59-2	-3.71-2
	10	-3.36-1	-6.02-2	-1.21-3	1.10-1	-1.09-1		10	-3.32-1	-5.88-2	-7.50-4	1.09-1	-1.08-1
5s <sub>1/2</sub>	1	1.89-3	9.69-3	2.14-3	3.55-3	-5.68-3	5s <sub>1/2</sub>	1	1.69-3	9.91-3	2.26-3	3.74-3	-5.99-3
	3	-1.15-2	1.07-2	6.48-3	1.02-2	-1.67-2		3	-1.05-2	1.16-2	6.42-3	1.01-2	-1.66-2
	5	-5.04-2	-4.42-3	1.42-2	2.12-2	-3.54-2		5	-4.96-2	-3.27-3	1.42-2	2.14-2	-3.56-2
	10	-9.92-2	-3.24-2	2.12-2	3.10-2	-5.22-2		10	-1.02-1	-3.23-2	2.19-2	3.22-2	-5.41-2
5p <sub>1/2</sub>	1	3.64-3	9.86-3	1.10-3	2.71-3	-3.81-3	5p <sub>1/2</sub>	1	3.78-3	1.02-2	1.24-3	2.82-3	-4.06-3
	3	-3.39-2	-4.72-3	4.75-3	1.26-2	-1.74-2		3	-3.40-2	-4.22-3	4.83-3	1.29-2	-1.77-2
	5	-4.19-2	-1.22-2	3.97-3	1.27-2	-1.66-2		5	-4.34-2	-1.23-2	4.33-3	1.33-2	-1.76-2
	10	-2.78-2	-9.73-3	-2.75-3	6.67-3	-3.92-3		10	-2.87-2	-1.02-2	-2.60-3	6.86-3	-4.26-3
5p <sub>3/2</sub>	1	2.73-3	4.39-3	7.09-4	8.05-4	-1.51-3	5p <sub>3/2</sub>	1	2.88-3	4.49-3	7.37-4	7.92-4	-1.53-3
	3	-2.74-2	-1.08-2	6.13-3	7.87-3	-1.40-2		3	-2.77-2	-1.08-2	6.15-3	7.98-3	-1.41-2
	5	-2.82-2	-1.61-2	7.28-3	6.30-3	-1.36-2		5	-2.93-2	-1.64-2	7.57-3	6.67-3	-1.42-2
	10	-2.00-2	-1.62-2	6.00-3	2.72-3	-8.72-3		10	-2.03-2	-1.66-2	6.08-3	2.66-3	-8.75-3
5d <sub>3/2</sub>	1	-1.30-2	-3.23-3	-3.42-4	3.83-3	-3.49-3	5d <sub>3/2</sub>	1	-1.31-2	-3.17-3	-4.26-4	3.87-3	-3.44-3
	3	-8.57-3	-4.32-3	8.81-5	1.72-3	-1.81-3		3	-9.18-3	-4.66-3	2.25-4	1.85-3	-2.08-3
	5	-1.47-2	-1.59-3	-2.29-3	4.78-3	-2.49-3		5	-1.40-2	-1.70-3	-2.29-3	4.45-3	-2.16-3
	10	-1.11-1	-1.34-2	2.69-3	3.96-2	-4.23-2		10	-1.07-1	-1.27-2	2.18-3	3.82-2	-4.04-2
5d <sub>5/2</sub>	1	-1.05-2	-3.91-3	1.01-3	2.82-3	-3.82-3	5d <sub>5/2</sub>	1	-1.06-2	-3.89-3	9.61-4	2.86-3	-3.82-3
	3	-2.13-4	-4.64-3	2.79-3	-1.22-3	-1.57-3		3	-7.42-4	-4.98-3	2.89-3	-1.12-3	-1.78-3
	5	-3.15-3	-2.36-3	3.58-3	1.03-3	-4.61-3		5	-2.31-3	-2.41-3	3.55-3	6.71-4	-4.23-3
	10	-9.57-2	-1.67-2	1.42-2	3.45-2	-4.87-2		10	-9.17-2	-1.59-2	1.40-2	3.31-2	-4.71-2
6s <sub>1/2</sub>	1	1.39-3	8.16-3	1.86-3	3.08-3	-4.93-3	6s <sub>1/2</sub>	1	1.21-3	8.28-3	1.95-3	3.22-3	-5.16-3
	3	-1.08-2	1.02-2	6.11-3	9.61-3	-1.57-2		3	-9.78-3	1.11-2	6.04-3	9.55-3	-1.56-2
	5	-4.88-2	-4.19-3	1.37-2	2.06-2	-3.43-2		5	-4.79-2	-3.07-3	1.37-2	2.07-2	-3.44-2
	10	-9.82-2	-3.20-2	2.09-2	3.06-2	-5.16-2		10	-1.01-1	-3.19-2	2.17-2	3.18-2	-5.35-2
6p <sub>1/2</sub>	1	3.69-3	8.88-3	1.25-3	2.32-3	-3.57-3	6p <sub>1/2</sub>	1	3.80-3	9.14-3	1.40-3	2.42-3	-3.82-3
	3	-3.23-2	-4.21-3	4.76-3	1.22-2	-1.69-2		3	-3.22-2	-3.67-3	4.84-3	1.24-2	-1.72-2
	5	-4.13-2	-1.20-2	4.12-3	1.25-2	-1.67-2		5	-4.27-2	-1.20-2	4.48-3	1.31-2	-1.76-2
	10	-2.77-2	-9.90-3	-2.62-3	6.62-3	-4.00-3		10	-2.87-2	-1.04-2	-2.45-3	6.82-3	-4.37-3
6p <sub>3/2</sub>	1	2.87-3	4.20-3	7.32-4	6.82-4	-1.41-3	6p <sub>3/2</sub>	1	3.00-3	4.29-3	7.71-4	6.70-4	-1.44-3
	3	-2.67-2	-1.04-2	6.01-3	7.69-3	-1.37-2		3	-2.68-2	-1.03-2	6.01-3	7.79-3	-1.38-2
	5	-2.82-2	-1.60-2	7.28-3	6.33-3	-1.36-2		5	-2.93-2	-1.63-2	7.56-3	6.70-3	-1.43-2
	10	-2.01-2	-1.63-2	5.98-3	2.70-3	-8.68-3		10	-2.04-2	-1.68-2	6.08-3	2.66-3	-8.73-3
7s <sub>1/2</sub>	1	1.09-3	7.80-3	1.84-3	3.05-3	-4.89-3	7s <sub>1/2</sub>	1	9.33-4	7.90-3	1.92-3	3.17-3	-5.09-3
	3	-1.02-2	1.04-2	6.01-3	9.46-3	-1.55-2		3	-9.55-3	1.11-2	5.96-3	9.44-3	-1.54-2
	5	-4.86-2	-4.09-3	1.37-2	2.05-2	-3.42-2		5	-4.75-2	-2.96-3	1.37-2	2.06-2	-3.42-2
	10	-9.82-2	-3.20-2	2.09-2	3.07-2	-5.16-2		10	-1.00-1	-3.19-2	2.17-2	3.18-2	-5.34-2
<i>Z = 89, Ac: 6d<sub>3/2</sub><sup>1</sup>7s<sub>1/2</sub><sup>2</sup></i>							<i>Z = 90, Th: 6d<sub>3/2</sub><sup>2</sup>7s<sub>1/2</sub><sup>2</sup></i>						
4s <sub>1/2</sub>	1	2.56-3	1.80-2	4.32-3	7.04-3	-1.14-2	4s <sub>1/2</sub>	1	2.09-3	1.85-2	4.59-3	7.46-3	-1.21-2
	3	-1.43-2	1.51-2	8.55-3	1.35-2	-2.20-2		3	-1.31-2	1.64-2	8.55-3	1.35-2	-2.21-2
	5	-5.81-2	-3.17-3	1.68-2	2.53-2	-4.21-2		5	-5.73-2	-1.79-3	1.69-2	2.56-2	-4.25-2
	10	-1.11-1	-3.42-2	2.44-2	3.58-2	-6.02-2		10	-1.14-1	-3.40-2	2.53-2	3.71-2	-6.24-2

Table 1 (continued)

Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$	Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$
4p <sub>1/2</sub>	1	6.82–4	1.47–2	3.85–4	5.67–3	−6.06–3	4p <sub>1/2</sub>	1	7.60–4	1.53–2	4.78–4	5.93–3	−6.41–3
	3	−4.56–2	−7.20–3	5.08–3	1.64–2	−2.15–2		3	−4.63–2	−6.74–3	5.17–3	1.69–2	−2.20–2
	5	−5.04–2	−1.44–2	4.15–3	1.52–2	−1.94–2		5	−5.24–2	−1.46–2	4.53–3	1.60–2	−2.06–2
	10	−3.03–2	−1.01–2	−3.16–3	7.45–3	−4.28–3		10	−3.15–2	−1.07–2	−2.99–3	7.75–3	−4.76–3
4p <sub>3/2</sub>	1	1.30–3	5.25–3	5.94–4	1.70–3	−2.29–3	4p <sub>3/2</sub>	1	1.51–3	5.44–3	5.98–4	1.69–3	−2.29–3
	3	−3.43–2	−1.38–2	7.14–3	9.60–3	−1.67–2		3	−3.49–2	−1.39–2	7.19–3	9.82–3	−1.70–2
	5	−3.21–2	−1.82–2	8.23–3	7.24–3	−1.55–2		5	−3.36–2	−1.87–2	8.57–3	7.68–3	−1.62–2
	10	−2.02–2	−1.67–2	6.32–3	2.68–3	−9.00–3		10	−2.06–2	−1.72–2	6.48–3	2.66–3	−9.13–3
4d <sub>3/2</sub>	1	−2.29–2	−7.52–3	−1.10–3	5.92–3	−4.81–3	4d <sub>3/2</sub>	1	−2.36–2	−7.71–3	−1.27–3	6.08–3	−4.81–3
	3	−8.70–3	−3.74–3	−5.93–4	1.87–3	−1.27–3		3	−9.36–3	−4.12–3	−4.80–4	2.00–3	−1.52–3
	5	−1.51–2	−1.48–4	−3.19–3	5.35–3	−2.16–3		5	−1.44–2	−2.04–4	−3.22–3	5.02–3	−1.80–3
	10	−1.14–1	−1.20–2	1.36–3	4.09–2	−4.22–2		10	−1.10–1	−1.13–2	8.13–4	3.95–2	−4.03–2
4d <sub>5/2</sub>	1	−1.76–2	−8.06–3	1.21–3	4.06–3	−5.27–3	4d <sub>5/2</sub>	1	−1.82–2	−8.26–3	1.15–3	4.19–3	−5.33–3
	3	1.52–3	−4.03–3	2.84–3	−1.65–3	−1.19–3		3	1.05–3	−4.37–3	2.95–3	−1.58–3	−1.37–3
	5	−2.16–3	−9.97–4	3.51–3	1.17–3	−4.68–3		5	−1.22–3	−9.96–4	3.50–3	7.88–4	−4.28–3
	10	−9.72–2	−1.54–2	1.39–2	3.55–2	−4.94–2		10	−9.32–2	−1.45–2	1.36–2	3.42–2	−4.78–2
4f <sub>5/2</sub>	1	2.39–3	2.35–3	−3.91–4	−9.32–5	4.84–4	4f <sub>5/2</sub>	1	2.84–3	2.50–3	−3.49–4	−2.07–4	5.57–4
	3	−3.64–2	7.07–4	−3.45–3	1.41–2	−1.07–2		3	−3.47–2	1.17–3	−3.45–3	1.37–2	−1.02–2
	5	−1.10–1	−9.81–3	−4.87–3	3.92–2	−3.43–2		5	−1.07–1	−9.01–3	−4.89–3	3.83–2	−3.34–2
	10	−3.43–1	−5.17–2	−9.98–3	1.14–1	−1.04–1		10	−3.38–1	−5.04–2	−9.74–3	1.13–1	−1.03–1
4f <sub>7/2</sub>	1	5.99–3	1.94–3	9.42–4	−1.43–3	4.91–4	4f <sub>7/2</sub>	1	6.52–3	2.09–3	1.00–3	−1.57–3	5.68–4
	3	−2.88–2	−5.41–4	1.53–4	1.13–2	−1.15–2		3	−2.71–2	−7.26–5	1.61–4	1.08–2	−1.10–2
	5	−9.94–2	−1.22–2	1.24–3	3.51–2	−3.64–2		5	−9.66–2	−1.14–2	1.26–3	3.43–2	−3.56–2
	10	−3.27–1	−5.75–2	−3.18–4	1.08–1	−1.07–1		10	−3.23–1	−5.62–2	8.99–5	1.07–1	−1.07–1
5s <sub>1/2</sub>	1	1.51–3	1.01–2	2.37–3	3.92–3	−6.30–3	5s <sub>1/2</sub>	1	1.25–3	1.03–2	2.50–3	4.12–3	−6.62–3
	3	−9.46–3	1.26–2	6.36–3	1.01–2	−1.65–2		3	−8.38–3	1.36–2	6.30–3	1.01–2	−1.63–2
	5	−4.86–2	−2.06–3	1.42–2	2.15–2	−3.57–2		5	−4.75–2	−7.87–4	1.42–2	2.15–2	−3.58–2
	10	−1.04–1	−3.21–2	2.27–2	3.33–2	−5.60–2		10	−1.06–1	−3.18–2	2.34–2	3.45–2	−5.79–2
5p <sub>1/2</sub>	1	3.92–3	1.06–2	1.41–3	2.94–3	−4.35–3	5p <sub>1/2</sub>	1	4.00–3	1.09–2	1.58–3	3.07–3	−4.65–3
	3	−3.40–2	−3.65–3	4.91–3	1.31–2	−1.80–2		3	−3.39–2	−3.03–3	4.96–3	1.33–2	−1.83–2
	5	−4.48–2	−1.24–2	4.69–3	1.39–2	−1.86–2		5	−4.62–2	−1.23–2	5.05–3	1.45–2	−1.96–2
	10	−2.97–2	−1.07–2	−2.41–3	7.12–3	−4.71–3		10	−3.09–2	−1.13–2	−2.18–3	7.44–3	−5.26–3
5p <sub>3/2</sub>	1	3.05–3	4.62–3	7.75–4	7.83–4	−1.56–3	5p <sub>3/2</sub>	1	3.19–3	4.71–3	8.13–4	7.69–4	−1.58–3
	3	−2.79–2	−1.07–2	6.16–3	8.09–3	−1.43–2		3	−2.80–2	−1.06–2	6.14–3	8.18–3	−1.43–2
	5	−3.05–2	−1.68–2	7.85–3	7.04–3	−1.49–2		5	−3.16–2	−1.71–2	8.12–3	7.41–3	−1.55–2
	10	−2.06–2	−1.71–2	6.21–3	2.65–3	−8.86–3		10	−2.11–2	−1.76–2	6.38–3	2.66–3	−9.04–3
5d <sub>3/2</sub>	1	−1.31–2	−3.08–3	−5.13–4	3.90–3	−3.39–3	5d <sub>3/2</sub>	1	−1.30–2	−2.96–3	−6.04–4	3.90–3	−3.30–3
	3	−9.85–3	−5.02–3	3.67–4	2.00–3	−2.37–3		3	−1.05–2	−5.38–3	5.10–4	2.17–3	−2.68–3
	5	−1.34–2	−1.85–3	−2.27–3	4.15–3	−1.88–3		5	−1.28–2	−2.02–3	−2.24–3	3.87–3	−1.64–3
	10	−1.03–1	−1.21–2	1.68–3	3.68–2	−3.85–2		10	−9.92–2	−1.14–2	1.17–3	3.54–2	−3.65–2
5d <sub>5/2</sub>	1	−1.06–2	−3.83–3	9.07–4	2.89–3	−3.80–3	5d <sub>5/2</sub>	1	−1.06–2	−3.75–3	8.46–4	2.91–3	−3.75–3
	3	−1.33–3	−5.32–3	3.00–3	−9.99–4	−2.00–3		3	−1.95–3	−5.67–3	3.10–3	−8.67–4	−2.24–3
	5	−1.64–3	−2.53–3	3.54–3	3.53–4	−3.89–3		5	−9.70–4	−2.63–3	3.53–3	4.12–5	−3.57–3
	10	−8.77–2	−1.51–2	1.37–2	3.18–2	−4.54–2		10	−8.37–2	−1.43–2	1.34–2	3.04–2	−4.38–2
6s <sub>1/2</sub>	1	1.04–3	8.44–3	2.04–3	3.36–3	−5.40–3	6s <sub>1/2</sub>	1	8.12–4	8.56–3	2.14–3	3.53–3	−5.67–3
	3	−8.78–3	1.20–2	5.97–3	9.49–3	−1.55–2		3	−7.76–3	1.29–2	5.90–3	9.44–3	−1.53–2
	5	−4.69–2	−1.90–3	1.37–2	2.07–2	−3.45–2		5	−4.58–2	−6.68–4	1.37–2	2.08–2	−3.45–2
	10	−1.03–1	−3.17–2	2.24–2	3.29–2	−5.53–2		10	−1.05–1	−3.14–2	2.31–2	3.40–2	−5.72–2
6p <sub>1/2</sub>	1	3.92–3	9.47–3	1.59–3	2.54–3	−4.13–3	6p <sub>1/2</sub>	1	4.00–3	9.76–3	1.80–3	2.67–3	−4.47–3
	3	−3.22–2	−3.08–3	4.93–3	1.26–2	−1.76–2		3	−3.20–2	−2.43–3	5.00–3	1.28–2	−1.78–2
	5	−4.41–2	−1.21–2	4.86–3	1.38–2	−1.86–2		5	−4.55–2	−1.20–2	5.24–3	1.44–2	−1.97–2
	10	−2.98–2	−1.09–2	−2.25–3	7.10–3	−4.85–3		10	−3.10–2	−1.15–2	−2.01–3	7.43–3	−5.43–3
6p <sub>3/2</sub>	1	3.15–3	4.40–3	8.18–4	6.65–4	−1.48–3	6p <sub>3/2</sub>	1	3.27–3	4.49–3	8.70–4	6.61–4	−1.53–3
	3	−2.70–2	−1.03–2	6.02–3	7.89–3	−1.39–2		3	−2.71–2	−1.02–2	6.01–3	7.98–3	−1.40–2
	5	−3.04–2	−1.67–2	7.84–3	7.08–3	−1.49–2		5	−3.16–2	−1.70–2	8.12–3	7.45–3	−1.56–2
	10	−2.08–2	−1.73–2	6.21–3	2.65–3	−8.86–3		10	−2.13–2	−1.78–2	6.39–3	2.68–3	−9.07–3
6d <sub>3/2</sub>	1	−1.18–2	−2.39–3	−4.89–4	3.66–3	−3.17–3	6d <sub>3/2</sub>	1	−1.16–2	−2.25–3	−5.54–4	3.64–3	−3.08–3
	3	−1.02–2	−5.28–3	5.33–4	2.08–3	−2.61–3		3	−1.09–2	−5.63–3	6.79–4	2.24–3	−2.92–3

(continued on next page)

Table 1 (continued)

Shell	E	$\Delta\beta_{unp}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$	Shell	E	$\Delta\beta_{unp}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$
	5	-1.32–2	-2.13–3	-2.15–3	3.99–3	-1.84–3		5	-1.26–2	-2.32–3	-2.09–3	3.71–3	-1.62–3
	10	-1.02–1	-1.21–2	1.69–3	3.62–2	-3.79–2		10	-9.77–2	-1.14–2	1.20–3	3.48–2	-3.60–2
$7s_{1/2}$	1	7.99–4	7.97–3	1.98–3	3.27–3	-5.24–3	$7s_{1/2}$	1	6.65–4	8.10–3	2.06–3	3.39–3	-5.45–3
	3	-8.59–3	1.19–2	5.88–3	9.36–3	-1.52–2		3	-7.71–3	1.26–2	5.82–3	9.30–3	-1.51–2
	5	-4.64–2	-1.79–3	1.36–2	2.06–2	-3.42–2		5	-4.53–2	-5.79–4	1.36–2	2.06–2	-3.42–2
	10	-1.03–1	-3.16–2	2.24–2	3.29–2	-5.52–2		10	-1.05–1	-3.13–2	2.31–2	3.39–2	-5.70–2
$Z = 91$ , Pa: $5f_{5/2}^2 6d_{3/2}^1 7s_{1/2}^2$							$Z = 92$ , U: $5f_{5/2}^3 6d_{3/2}^1 7s_{1/2}^2$						
$4s_{1/2}$	1	1.27–3	1.89–2	4.96–3	8.03–3	-1.30–2	$4s_{1/2}$	1	5.45–4	1.92–2	5.29–3	8.54–3	-1.38–2
	3	-1.17–2	1.79–2	8.52–3	1.36–2	-2.21–2		3	-1.04–2	1.94–2	8.50–3	1.36–2	-2.21–2
	5	-5.62–2	-2.26–4	1.70–2	2.58–2	-4.28–2		5	-5.50–2	1.37–3	1.71–2	2.60–2	-4.31–2
	10	-1.17–1	-3.37–2	2.62–2	3.85–2	-6.46–2		10	-1.19–1	-3.33–2	2.70–2	3.98–2	-6.68–2
$4p_{1/2}$	1	9.08–4	1.62–2	6.11–4	6.23–3	-6.84–3	$4p_{1/2}$	1	9.50–4	1.69–2	7.61–4	6.54–3	-7.30–3
	3	-4.69–2	-6.15–3	5.26–3	1.74–2	-2.26–2		3	-4.74–2	-5.52–3	5.32–3	1.78–2	-2.31–2
	5	-5.46–2	-1.48–2	4.94–3	1.69–2	-2.18–2		5	-5.67–2	-1.50–2	5.33–3	1.78–2	-2.31–2
	10	-3.30–2	-1.13–2	-2.77–3	8.13–3	-5.37–3		10	-3.46–2	-1.19–2	-2.51–3	8.58–3	-6.07–3
$4p_{3/2}$	1	1.92–3	5.75–3	6.08–4	1.65–3	-2.26–3	$4p_{3/2}$	1	2.21–3	5.97–3	6.22–4	1.63–3	-2.25–3
	3	-3.55–2	-1.40–2	7.24–3	1.01–2	-1.73–2		3	-3.60–2	-1.40–2	7.26–3	1.02–2	-1.75–2
	5	-3.52–2	-1.93–2	8.93–3	8.17–3	-1.71–2		5	-3.67–2	-1.98–2	9.26–3	8.63–3	-1.79–2
	10	-2.11–2	-1.77–2	6.67–3	2.68–3	-9.35–3		10	-2.17–2	-1.83–2	6.90–3	2.73–3	-9.63–3
$4d_{3/2}$	1	-2.43–2	-7.87–3	-1.51–3	6.28–3	-4.77–3	$4d_{3/2}$	1	-2.50–2	-8.01–3	-1.73–3	6.45–3	-4.72–3
	3	-1.02–2	-4.57–3	-3.44–4	2.17–3	-1.83–3		3	-1.10–2	-5.01–3	-2.13–4	2.34–3	-2.13–3
	5	-1.36–2	-2.95–4	-3.23–3	4.68–3	-1.45–3		5	-1.30–2	-4.12–4	-3.23–3	4.38–3	-1.16–3
	10	-1.06–1	-1.05–2	2.42–4	3.81–2	-3.84–2		10	-1.02–1	-9.75–3	-3.18–4	3.68–2	-3.64–2
$4d_{5/2}$	1	-1.89–2	-8.48–3	1.03–3	4.37–3	-5.40–3	$4d_{5/2}$	1	-1.94–2	-8.64–3	9.31–4	4.50–3	-5.43–3
	3	4.50–4	-4.80–3	3.08–3	-1.48–3	-1.59–3		3	-1.58–4	-5.20–3	3.20–3	-1.38–3	-1.82–3
	5	-2.77–4	-1.03–3	3.49–3	3.96–4	-3.89–3		5	5.47–4	-1.09–3	3.49–3	4.47–5	-3.54–3
	10	-8.92–2	-1.37–2	1.33–2	3.29–2	-4.62–2		10	-8.53–2	-1.28–2	1.30–2	3.16–2	-4.46–2
$4f_{5/2}$	1	3.27–3	2.61–3	-3.03–4	-3.22–4	6.25–4	$4f_{5/2}$	1	3.71–3	2.74–3	-2.54–4	-4.38–4	6.92–4
	3	-3.30–2	1.65–3	-3.46–3	1.32–2	-9.72–3		3	-3.14–2	2.11–3	-3.46–3	1.27–2	-9.24–3
	5	-1.05–1	-8.22–3	-4.93–3	3.75–2	-3.26–2		5	-1.02–1	-7.42–3	-4.96–3	3.67–2	-3.17–2
	10	-3.34–1	-4.91–2	-9.54–3	1.12–1	-1.02–1		10	-3.29–1	-4.77–2	-9.35–3	1.11–1	-1.01–1
$4f_{7/2}$	1	7.04–3	2.19–3	1.08–3	-1.72–3	6.39–4	$4f_{7/2}$	1	7.57–3	2.32–3	1.16–3	-1.87–3	7.10–4
	3	-2.53–2	4.04–4	1.65–4	1.03–2	-1.05–2		3	-2.36–2	8.66–4	1.77–4	9.84–3	-1.00–2
	5	-9.37–2	-1.06–2	1.26–3	3.35–2	-3.48–2		5	-9.09–2	-9.76–3	1.26–3	3.27–2	-3.40–2
	10	-3.18–1	-5.49–2	4.78–4	1.05–1	-1.06–1		10	-3.14–1	-5.35–2	8.40–4	1.04–1	-1.05–1
$5s_{1/2}$	1	7.92–4	1.05–2	2.70–3	4.42–3	-7.12–3	$5s_{1/2}$	1	3.89–4	1.06–2	2.86–3	4.67–3	-7.53–3
	3	-7.17–3	1.47–2	6.23–3	1.00–2	-1.62–2		3	-6.00–3	1.58–2	6.16–3	9.96–3	-1.61–2
	5	-4.63–2	6.23–4	1.42–2	2.16–2	-3.58–2		5	-4.50–2	2.05–3	1.42–2	2.16–2	-3.58–2
	10	-1.08–1	-3.14–2	2.42–2	3.56–2	-5.98–2		10	-1.10–1	-3.09–2	2.49–2	3.68–2	-6.17–2
$5p_{1/2}$	1	4.12–3	1.13–2	1.85–3	3.25–3	-5.10–3	$5p_{1/2}$	1	4.15–3	1.17–2	2.11–3	3.43–3	-5.54–3
	3	-3.38–2	-2.29–3	5.03–3	1.36–2	-1.86–2		3	-3.35–2	-1.51–3	5.07–3	1.38–2	-1.89–2
	5	-4.77–2	-1.23–2	5.44–3	1.53–2	-2.07–2		5	-4.91–2	-1.22–2	5.82–3	1.59–2	-2.17–2
	10	-3.24–2	-1.18–2	-1.91–3	7.84–3	-5.93–3		10	-3.39–2	-1.24–2	-1.59–3	8.30–3	-6.71–3
$5p_{3/2}$	1	3.47–3	4.90–3	8.77–4	7.49–4	-1.63–3	$5p_{3/2}$	1	3.64–3	5.02–3	9.34–4	7.37–4	-1.67–3
	3	-2.82–2	-1.05–2	6.13–3	8.28–3	-1.44–2		3	-2.82–2	-1.04–2	6.09–3	8.34–3	-1.44–2
	5	-3.28–2	-1.75–2	8.42–3	7.81–3	-1.62–2		5	-3.40–2	-1.78–2	8.68–3	8.19–3	-1.69–2
	10	-2.17–2	-1.82–2	6.58–3	2.72–3	-9.30–3		10	-2.24–2	-1.87–2	6.83–3	2.81–3	-9.64–3
$5d_{3/2}$	1	-1.29–2	-2.74–3	-7.38–4	3.91–3	-3.17–3	$5d_{3/2}$	1	-1.27–2	-2.53–3	-8.46–4	3.89–3	-3.04–3
	3	-1.14–2	-5.81–3	6.73–4	2.37–3	-3.05–3		3	-1.22–2	-6.20–3	8.27–4	2.57–3	-3.40–3
	5	-1.23–2	-2.22–3	-2.18–3	3.61–3	-1.43–3		5	-1.19–2	-2.44–3	-2.10–3	3.38–3	-1.27–3
	10	-9.52–2	-1.07–2	6.50–4	3.39–2	-3.46–2		10	-9.14–2	-1.01–2	1.48–4	3.25–2	-3.27–2
$5d_{5/2}$	1	-1.05–2	-3.57–3	7.54–4	2.92–3	-3.67–3	$5d_{5/2}$	1	-1.03–2	-3.39–3	6.71–4	2.90–3	-3.57–3
	3	-2.72–3	-6.09–3	3.23–3	-7.01–4	-2.53–3		3	-3.45–3	-6.46–3	3.34–3	-5.34–4	-2.81–3
	5	-3.37–4	-2.78–3	3.54–3	-2.70–4	-3.27–3		5	1.74–4	-2.95–3	3.56–3	-5.38–4	-3.02–3
	10	-7.97–2	-1.36–2	1.31–2	2.91–2	-4.21–2		10	-7.58–2	-1.28–2	1.28–2	2.77–2	-4.05–2
$5f_{5/2}$	1	5.57–4	-2.18–4	3.14–4	-2.47–4	-6.73–5	$5f_{5/2}$	1	4.59–4	-3.31–4	3.54–4	-2.45–4	-1.09–4
	3	-2.56–2	1.77–4	-2.17–3	9.89–3	-7.73–3		3	-2.39–2	4.36–4	-2.09–3	9.33–3	-7.24–3

Table 1 (continued)

Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$	Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$
	5	-9.12–2	-8.00–3	-3.60–3	3.26–2	-2.90–2		5	-8.78–2	-7.29–3	-3.56–3	3.15–2	-2.79–2
	10	-3.15–1	-4.69–2	-7.91–3	1.06–1	-9.79–2		10	-3.10–1	-4.55–2	-7.65–3	1.04–1	-9.65–2
$6s_{1/2}$	1	4.03–4	8.63–3	2.29–3	3.75–3	-6.04–3	$6s_{1/2}$	1	5.04–5	8.69–3	2.41–3	3.94–3	-6.35–3
	3	-6.59–3	1.39–2	5.82–3	9.37–3	-1.52–2		3	-5.46–3	1.49–2	5.75–3	9.30–3	-1.50–2
	5	-4.45–2	6.98–4	1.37–2	2.08–2	-3.45–2		5	-4.32–2	2.08–3	1.36–2	2.08–2	-3.45–2
	10	-1.07–1	-3.10–2	2.39–2	3.52–2	-5.90–2		10	-1.09–1	-3.05–2	2.45–2	3.62–2	-6.08–2
$6p_{1/2}$	1	4.03–3	1.00–2	2.08–3	2.82–3	-4.91–3	$6p_{1/2}$	1	3.99–3	1.02–2	2.36–3	2.97–3	-5.32–3
	3	-3.18–2	-1.65–3	5.06–3	1.31–2	-1.81–2		3	-3.13–2	-8.37–4	5.09–3	1.32–2	-1.83–2
	5	-4.69–2	-1.20–2	5.63–3	1.51–2	-2.07–2		5	-4.81–2	-1.18–2	6.01–3	1.57–2	-2.17–2
	10	-3.25–2	-1.20–2	-1.72–3	7.85–3	-6.13–3		10	-3.40–2	-1.26–2	-1.39–3	8.31–3	-6.92–3
$6p_{3/2}$	1	3.49–3	4.63–3	9.44–4	6.48–4	-1.59–3	$6p_{3/2}$	1	3.62–3	4.72–3	1.01–3	6.45–4	-1.66–3
	3	-2.72–2	-1.00–2	5.98–3	8.06–3	-1.40–2		3	-2.72–2	-9.88–3	5.94–3	8.12–3	-1.41–2
	5	-3.28–2	-1.74–2	8.40–3	7.84–3	-1.62–2		5	-3.39–2	-1.77–2	8.67–3	8.21–3	-1.69–2
	10	-2.20–2	-1.84–2	6.60–3	2.75–3	-9.35–3		10	-2.27–2	-1.90–2	6.85–3	2.86–3	-9.71–3
$6d_{3/2}$	1	-1.13–2	-1.97–3	-6.64–4	3.59–3	-2.93–3	$6d_{3/2}$	1	-1.09–2	-1.70–3	-7.51–4	3.54–3	-2.78–3
	3	-1.17–2	-6.02–3	8.46–4	2.45–3	-3.29–3		3	-1.26–2	-6.42–3	1.01–3	2.66–3	-3.67–3
	5	-1.22–2	-2.54–3	-2.02–3	3.45–3	-1.43–3		5	-1.18–2	-2.79–3	-1.93–3	3.23–3	-1.30–3
	10	-9.36–2	-1.07–2	6.87–4	3.33–2	-3.40–2		10	-8.97–2	-1.01–2	1.91–4	3.19–2	-3.21–2
$7s_{1/2}$	1	3.94–4	8.15–3	2.16–3	3.53–3	-5.69–3	$7s_{1/2}$	1	9.18–5	8.17–3	2.25–3	3.68–3	-5.94–3
	3	-6.47–3	1.36–2	5.70–3	9.18–3	-1.49–2		3	-5.31–3	1.46–2	5.61–3	9.08–3	-1.47–2
	5	-4.38–2	7.88–4	1.35–2	2.06–2	-3.41–2		5	-4.25–2	2.14–3	1.34–2	2.05–2	-3.40–2
	10	-1.06–1	-3.08–2	2.37–2	3.50–2	-5.87–2		10	-1.08–1	-3.03–2	2.44–2	3.60–2	-6.04–2
$Z = 93, \text{Np: } 5f_{5/2}^4 6d_{3/2}^1 7s_{1/2}^2$							$Z = 94, \text{Pu: } 5f_{5/2}^6 7s_{1/2}^2$						
$4s_{1/2}$	1	-2.74–4	1.96–2	5.65–3	9.08–3	-1.47–2	$4s_{1/2}$	1	-1.32–3	2.00–2	6.08–3	9.73–3	-1.58–2
	3	-9.00–3	2.09–2	8.48–3	1.36–2	-2.21–2		3	-7.53–3	2.25–2	8.47–3	1.37–2	-2.22–2
	5	-5.38–2	3.06–3	1.71–2	2.62–2	-4.33–2		5	-5.24–2	4.88–3	1.72–2	2.63–2	-4.35–2
	10	-1.22–1	-3.27–2	2.78–2	4.11–2	-6.89–2		10	-1.24–1	-3.20–2	2.87–2	4.24–2	-7.11–2
$4p_{1/2}$	1	9.24–4	1.77–2	9.36–4	6.88–3	-7.82–3	$4p_{1/2}$	1	8.46–4	1.85–2	1.17–3	7.28–3	-8.45–3
	3	-4.77–2	-4.81–3	5.37–3	1.82–2	-2.36–2		3	-4.80–2	-3.98–3	5.41–3	1.87–2	-2.41–2
	5	-5.88–2	-1.51–2	5.73–3	1.86–2	-2.44–2		5	-6.09–2	-1.51–2	6.14–3	1.95–2	-2.57–2
	10	-3.63–2	-1.25–2	-2.20–3	9.09–3	-6.88–3		10	-3.83–2	-1.32–2	-1.85–3	9.69–3	-7.84–3
$4p_{3/2}$	1	2.49–3	6.19–3	6.42–4	1.61–3	-2.25–3	$4p_{3/2}$	1	2.84–3	6.46–3	6.76–4	1.58–3	-2.26–3
	3	-3.64–2	-1.40–2	7.25–3	1.04–2	-1.76–2		3	-3.68–2	-1.40–2	7.22–3	1.06–2	-1.78–2
	5	-3.82–2	-2.03–2	9.59–3	9.08–3	-1.87–2		5	-3.97–2	-2.08–2	9.91–3	9.56–3	-1.95–2
	10	-2.24–2	-1.89–2	7.17–3	2.82–3	-9.99–3		10	-2.32–2	-1.95–2	7.49–3	2.95–3	-1.04–2
$4d_{3/2}$	1	-2.56–2	-8.13–3	-1.96–3	6.60–3	-4.64–3	$4d_{3/2}$	1	-2.63–2	-8.22–3	-2.23–3	6.77–3	-4.54–3
	3	-1.19–2	-5.47–3	-8.20–5	2.54–3	-2.46–3		3	-1.29–2	-5.98–3	6.05–5	2.77–3	-2.83–3
	5	-1.24–2	-5.57–4	-3.20–3	4.11–3	-9.11–4		5	-1.20–2	-7.40–4	-3.16–3	3.86–3	-7.04–4
	10	-9.80–2	-9.03–3	-8.72–4	3.54–2	-3.45–2		10	-9.42–2	-8.32–3	-1.43–3	3.41–2	-3.26–2
$4d_{5/2}$	1	-1.99–2	-8.79–3	8.19–4	4.62–3	-5.44–3	$4d_{5/2}$	1	-2.05–2	-8.93–3	6.77–4	4.76–3	-5.44–3
	3	-8.59–4	-5.63–3	3.33–3	-1.24–3	-2.08–3		3	-1.65–3	-6.11–3	3.47–3	-1.09–3	-2.38–3
	5	1.29–3	-1.17–3	3.51–3	-2.83–4	-3.22–3		5	1.98–3	-1.30–3	3.54–3	-6.01–4	-2.94–3
	10	-8.14–2	-1.20–2	1.27–2	3.03–2	-4.30–2		10	-7.75–2	-1.12–2	1.24–2	2.90–2	-4.14–2
$4f_{5/2}$	1	4.14–3	2.86–3	-2.03–4	-5.51–4	7.54–4	$4f_{5/2}$	1	4.59–3	2.98–3	-1.46–4	-6.70–4	8.17–4
	3	-2.97–2	2.58–3	-3.45–3	1.22–2	-8.76–3		3	-2.80–2	3.05–3	-3.45–3	1.17–2	-8.29–3
	5	-9.88–2	-6.63–3	-4.99–3	3.59–2	-3.09–2		5	-9.60–2	-5.85–3	-5.03–3	3.51–2	-3.00–2
	10	-3.24–1	-4.64–2	-9.19–3	1.09–1	-1.00–1		10	-3.20–1	-4.50–2	-9.07–3	1.08–1	-9.89–2
$4f_{7/2}$	1	8.09–3	2.44–3	1.23–3	-2.01–3	7.77–4	$4f_{7/2}$	1	8.63–3	2.55–3	1.32–3	-2.17–3	8.41–4
	3	-2.19–2	1.34–3	1.84–4	9.33–3	-9.52–3		3	-2.02–2	1.80–3	1.96–4	8.82–3	-9.02–3
	5	-8.80–2	-8.97–3	1.26–3	3.19–2	-3.31–2		5	-8.52–2	-8.18–3	1.26–3	3.11–2	-3.23–2
	10	-3.09–1	-5.21–2	1.18–3	1.03–1	-1.04–1		10	-3.04–1	-5.08–2	1.49–3	1.02–1	-1.03–1
$5s_{1/2}$	1	-6.27–5	1.08–2	3.03–3	4.93–3	-7.97–3	$5s_{1/2}$	1	-6.35–4	1.09–2	3.24–3	5.25–3	-8.49–3
	3	-4.82–3	1.69–2	6.10–3	9.91–3	-1.60–2		3	-3.57–3	1.81–2	6.04–3	9.87–3	-1.59–2
	5	-4.35–2	3.55–3	1.42–2	2.17–2	-3.58–2		5	-4.20–2	5.15–3	1.41–2	2.17–2	-3.58–2
	10	-1.12–1	-3.03–2	2.56–2	3.79–2	-6.35–2		10	-1.14–1	-2.95–2	2.63–2	3.90–2	-6.53–2
$5p_{1/2}$	1	4.12–3	1.20–2	2.40–3	3.62–3	-6.02–3	$5p_{1/2}$	1	4.04–3	1.23–2	2.77–3	3.87–3	-6.63–3
	3	-3.31–2	-6.57–4	5.09–3	1.40–2	-1.91–2		3	-3.26–2	3.10–4	5.11–3	1.42–2	-1.93–2

(continued on next page)

Table 1 (continued)

Shell	E	$\Delta\beta_{unp}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$	Shell	E	$\Delta\beta_{unp}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$
	5	-5.04–2	-1.21–2	6.19–3	1.66–2	-2.28–2		5	-5.18–2	-1.18–2	6.57–3	1.73–2	-2.39–2
	10	-3.56–2	-1.29–2	-1.24–3	8.82–3	-7.58–3		10	-3.75–2	-1.35–2	-8.36–4	9.42–3	-8.59–3
5p <sub>3/2</sub>	1	3.80–3	5.12–3	9.98–4	7.31–4	-1.73–3	5p <sub>3/2</sub>	1	3.98–3	5.27–3	1.09–3	7.32–4	-1.82–3
	3	-2.82–2	-1.02–2	6.03–3	8.39–3	-1.44–2		3	-2.81–2	-1.00–2	5.96–3	8.44–3	-1.44–2
	5	-3.51–2	-1.81–2	8.93–3	8.55–3	-1.75–2		5	-3.62–2	-1.85–2	9.19–3	8.94–3	-1.81–2
	10	-2.31–2	-1.93–2	7.11–3	2.94–3	-1.00–2		10	-2.40–2	-1.99–2	7.43–3	3.11–3	-1.05–2
5d <sub>3/2</sub>	1	-1.24–2	-2.29–3	-9.53–4	3.85–3	-2.90–3	5d <sub>3/2</sub>	1	-1.20–2	-1.98–3	-1.07–3	3.81–3	-2.73–3
	3	-1.31–2	-6.61–3	9.78–4	2.80–3	-3.77–3		3	-1.41–2	-7.05–3	1.14–3	3.04–3	-4.18–3
	5	-1.16–2	-2.69–3	-2.01–3	3.18–3	-1.17–3		5	-1.14–2	-2.98–3	-1.89–3	3.01–3	-1.11–3
	10	-8.76–2	-9.53–3	-3.48–4	3.12–2	-3.08–2		10	-8.39–2	-8.96–3	-8.46–4	2.98–2	-2.89–2
5d <sub>5/2</sub>	1	-1.01–2	-3.19–3	5.89–4	2.87–3	-3.46–3	5d <sub>5/2</sub>	1	-9.78–3	-2.94–3	4.93–4	2.84–3	-3.33–3
	3	-4.28–3	-6.87–3	3.46–3	-3.43–4	-3.12–3		3	-5.18–3	-7.31–3	3.59–3	-1.31–4	-3.46–3
	5	5.93–4	-3.15–3	3.59–3	-7.78–4	-2.81–3		5	9.37–4	-3.38–3	3.63–3	-1.00–3	-2.63–3
	10	-7.20–2	-1.21–2	1.25–2	2.64–2	-3.89–2		10	-6.81–2	-1.15–2	1.22–2	2.51–2	-3.73–2
5f <sub>5/2</sub>	1	3.13–4	-4.57–4	3.91–4	-2.30–4	-1.62–4	5f <sub>5/2</sub>	1	1.18–4	-6.05–4	4.31–4	-2.03–4	-2.28–4
	3	-2.23–2	6.81–4	-2.02–3	8.79–3	-6.77–3		3	-2.07–2	9.09–4	-1.95–3	8.27–3	-6.31–3
	5	-8.45–2	-6.61–3	-3.52–3	3.05–2	-2.69–2		5	-8.13–2	-5.95–3	-3.49–3	2.94–2	-2.59–2
	10	-3.04–1	-4.41–2	-7.41–3	1.02–1	-9.50–2		10	-2.98–1	-4.27–2	-7.21–3	1.01–1	-9.36–2
6s <sub>1/2</sub>	1	-3.36–4	8.69–3	2.53–3	4.12–3	-6.65–3	6s <sub>1/2</sub>	1	-8.16–4	8.70–3	2.68–3	4.34–3	-7.02–3
	3	-4.32–3	1.59–2	5.67–3	9.22–3	-1.49–2		3	-3.09–3	1.70–2	5.59–3	9.16–3	-1.47–2
	5	-4.17–2	3.52–3	1.36–2	2.08–2	-3.44–2		5	-4.01–2	5.05–3	1.35–2	2.08–2	-3.43–2
	10	-1.10–1	-2.98–2	2.52–2	3.73–2	-6.25–2		10	-1.12–1	-2.90–2	2.59–2	3.83–2	-6.42–2
6p <sub>1/2</sub>	1	3.91–3	1.04–2	2.66–3	3.13–3	-5.79–3	6p <sub>1/2</sub>	1	3.73–3	1.05–2	3.02–3	3.32–3	-6.34–3
	3	-3.08–2	4.69–5	5.11–3	1.34–2	-1.85–2		3	-3.01–2	1.06–3	5.11–3	1.35–2	-1.86–2
	5	-4.94–2	-1.16–2	6.39–3	1.64–2	-2.28–2		5	-5.05–2	-1.13–2	6.76–3	1.70–2	-2.38–2
	10	-3.58–2	-1.31–2	-1.01–3	8.85–3	-7.83–3		10	-3.76–2	-1.37–2	-6.01–4	9.45–3	-8.85–3
6p <sub>3/2</sub>	1	3.73–3	4.80–3	1.09–3	6.45–4	-1.73–3	6p <sub>3/2</sub>	1	3.85–3	4.89–3	1.18–3	6.53–4	-1.83–3
	3	-2.71–2	-9.69–3	5.88–3	8.15–3	-1.40–2		3	-2.70–2	-9.45–3	5.79–3	8.17–3	-1.40–2
	5	-3.49–2	-1.80–2	8.91–3	8.57–3	-1.75–2		5	-3.61–2	-1.83–2	9.16–3	8.97–3	-1.81–2
	10	-2.35–2	-1.95–2	7.14–3	3.00–3	-1.01–2		10	-2.43–2	-2.01–2	7.47–3	3.17–3	-1.06–2
6d <sub>3/2</sub>	1	-1.04–2	-1.38–3	-8.35–4	3.45–3	-2.61–3	7s <sub>1/2</sub>	1	-8.93–4	7.91–3	2.49–3	4.02–3	-6.50–3
	3	-1.35–2	-6.85–3	1.18–3	2.90–3	-4.08–3		3	-2.63–3	1.67–2	5.38–3	8.83–3	-1.42–2
	5	-1.16–2	-3.05–3	-1.82–3	3.04–3	-1.22–3		5	-3.94–2	5.03–3	1.33–2	2.04–2	-3.37–2
	10	-8.59–2	-9.59–3	-2.97–4	3.05–2	-3.02–2		10	-1.11–1	-2.87–2	2.57–2	3.81–2	-6.37–2
7s <sub>1/2</sub>	1	-3.15–4	8.09–3	2.36–3	3.83–3	-6.19–3							
	3	-3.93–3	1.57–2	5.49–3	8.94–3	-1.44–2							
	5	-4.10–2	3.53–3	1.34–2	2.05–2	-3.38–2							
	10	-1.10–1	-2.96–2	2.50–2	3.71–2	-6.21–2							
$Z = 95, \text{Am: } 5f_{5/2}^6 5f_{7/2}^1 7s_{1/2}^2$							$Z = 96, \text{Cm: } 5f_{5/2}^6 5f_{7/2}^1 6d_{3/2}^1 7s_{1/2}^2$						
4s <sub>1/2</sub>	1	-2.38–3	2.03–2	6.50–3	1.04–2	-1.69–2	4s <sub>1/2</sub>	1	-3.34–3	2.06–2	6.89–3	1.09–2	-1.78–2
	3	-6.15–3	2.40–2	8.48–3	1.38–2	-2.22–2		3	-4.88–3	2.55–2	8.49–3	1.39–2	-2.24–2
	5	-5.08–2	6.74–3	1.72–2	2.65–2	-4.37–2		5	-4.93–2	8.62–3	1.72–2	2.66–2	-4.38–2
	10	-1.26–1	-3.12–2	2.94–2	4.37–2	-7.31–2		10	-1.27–1	-3.02–2	3.02–2	4.49–2	-7.51–2
4p <sub>1/2</sub>	1	6.53–4	1.92–2	1.40–3	7.70–3	-9.10–3	4p <sub>1/2</sub>	1	3.43–4	1.99–2	1.63–3	8.15–3	-9.77–3
	3	-4.82–2	-3.11–3	5.43–3	1.91–2	-2.46–2		3	-4.84–2	-2.21–3	5.44–3	1.95–2	-2.50–2
	5	-6.29–2	-1.51–2	6.53–3	2.04–2	-2.70–2		5	-6.48–2	-1.50–2	6.90–3	2.13–2	-2.82–2
	10	-4.04–2	-1.38–2	-1.47–3	1.03–2	-8.87–3		10	-4.26–2	-1.45–2	-1.04–3	1.10–2	-1.00–2
4p <sub>3/2</sub>	1	3.10–3	6.64–3	7.10–4	1.56–3	-2.27–3	4p <sub>3/2</sub>	1	3.23–3	6.76–3	7.32–4	1.56–3	-2.29–3
	3	-3.71–2	-1.40–2	7.17–3	1.07–2	-1.79–2		3	-3.73–2	-1.39–2	7.11–3	1.08–2	-1.79–2
	5	-4.11–2	-2.12–2	1.02–2	1.00–2	-2.02–2		5	-4.24–2	-2.16–2	1.05–2	1.04–2	-2.09–2
	10	-2.40–2	-2.02–2	7.83–3	3.11–3	-1.09–2		10	-2.50–2	-2.08–2	8.20–3	3.30–3	-1.15–2
4d <sub>3/2</sub>	1	-2.68–2	-8.30–3	-2.48–3	6.90–3	-4.41–3	4d <sub>3/2</sub>	1	-2.72–2	-8.37–3	-2.70–3	7.00–3	-4.29–3
	3	-1.39–2	-6.47–3	1.93–4	3.01–3	-3.20–3		3	-1.49–2	-6.95–3	3.14–4	3.24–3	-3.55–3
	5	-1.16–2	-9.43–4	-3.10–3	3.65–3	-5.49–4		5	-1.13–2	-1.16–3	-3.03–3	3.47–3	-4.43–4
	10	-9.05–2	-7.67–3	-1.97–3	3.28–2	-3.08–2		10	-8.70–2	-7.06–3	-2.49–3	3.15–2	-2.90–2
4d <sub>5/2</sub>	1	-2.09–2	-9.04–3	5.51–4	4.86–3	-5.41–3	4d <sub>5/2</sub>	1	-2.13–2	-9.14–3	4.41–4	4.93–3	-5.37–3
	3	-2.46–3	-6.58–3	3.60–3	-9.28–4	-2.67–3		3	-3.26–3	-7.02–3	3.72–3	-7.59–4	-2.96–3

Table 1 (continued)

Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$	Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$	
	5	2.55–3	−1.44–3	3.57–3	−8.79–4	−2.70–3		5	3.02–3	−1.59–3	3.62–3	−1.12–3	−2.50–3	
	10	−7.37–2	−1.04–2	1.21–2	2.77–2	−3.99–2		10	−7.01–2	−9.72–3	1.19–2	2.65–2	−3.84–2	
$4f_{5/2}$	1	5.01–3	3.10–3	−9.03–5	−7.81–4	8.72–4	$4f_{5/2}$	1	5.37–3	3.20–3	−4.20–5	−8.75–4	9.17–4	
	3	−2.64–2	3.50–3	−3.44–3	1.13–2	−7.82–3		3	−2.47–2	3.95–3	−3.42–3	1.08–2	−7.37–3	
	5	−9.32–2	−5.06–3	−5.06–3	3.42–2	−2.92–2		5	−9.04–2	−4.29–3	−5.08–3	3.34–2	−2.83–2	
	10	−3.15–1	−4.37–2	−8.94–3	1.07–1	−9.77–2		10	−3.10–1	−4.23–2	−8.83–3	1.05–1	−9.64–2	
$4f_{7/2}$	1	9.14–3	2.66–3	1.41–3	−2.31–3	9.01–4	$4f_{7/2}$	1	9.60–3	2.78–3	1.48–3	−2.43–3	9.52–4	
	3	−1.84–2	2.27–3	2.10–4	8.32–3	−8.53–3		3	−1.68–2	2.72–3	2.24–4	7.86–3	−8.08–3	
	5	−8.23–2	−7.39–3	1.25–3	3.02–2	−3.15–2		5	−7.96–2	−6.61–3	1.24–3	2.94–2	−3.07–2	
	10	−3.00–1	−4.94–2	1.79–3	1.00–1	−1.02–1		10	−2.95–1	−4.81–2	2.07–3	9.92–2	−1.01–1	
$5s_{1/2}$	1	−1.20–3	1.09–2	3.43–3	5.54–3	−8.97–3	$5s_{1/2}$	1	−1.71–3	1.09–2	3.60–3	5.78–3	−9.38–3	
	3	−2.39–3	1.92–2	5.98–3	9.84–3	−1.58–2		3	−1.30–3	2.03–2	5.94–3	9.82–3	−1.58–2	
	5	−4.04–2	6.76–3	1.40–2	2.17–2	−3.57–2		5	−3.87–2	8.37–3	1.40–2	2.16–2	−3.56–2	
	10	−1.15–1	−2.86–2	2.69–2	4.00–2	−6.70–2		10	−1.16–1	−2.76–2	2.75–2	4.10–2	−6.86–2	
$5p_{1/2}$	1	3.89–3	1.26–2	3.13–3	4.11–3	−7.24–3	$5p_{1/2}$	1	3.66–3	1.28–2	3.48–3	4.36–3	−7.84–3	
	3	−3.21–2	1.31–3	5.11–3	1.44–2	−1.95–2		3	−3.15–2	2.32–3	5.10–3	1.45–2	−1.96–2	
	5	−5.30–2	−1.15–2	6.93–3	1.80–2	−2.49–2		5	−5.41–2	−1.12–2	7.28–3	1.86–2	−2.59–2	
	10	−3.95–2	−1.41–2	−4.01–4	1.01–2	−9.67–3		10	−4.15–2	−1.46–2	6.60–5	1.08–2	−1.08–2	
$5p_{3/2}$	1	4.10–3	5.35–3	1.16–3	7.34–4	−1.90–3	$5p_{3/2}$	1	4.12–3	5.38–3	1.22–3	7.49–4	−1.97–3	
	3	−2.80–2	−9.82–3	5.87–3	8.45–3	−1.43–2		3	−2.78–2	−9.60–3	5.77–3	8.43–3	−1.42–2	
	5	−3.72–2	−1.87–2	9.42–3	9.29–3	−1.87–2		5	−3.82–2	−1.90–2	9.62–3	9.60–3	−1.92–2	
	10	−2.49–2	−2.05–2	7.77–3	3.30–3	−1.11–2		10	−2.59–2	−2.11–2	8.14–3	3.52–3	−1.17–2	
$5d_{3/2}$	1	−1.16–2	−1.70–3	−1.17–3	3.75–3	−2.58–3	$5d_{3/2}$	1	−1.13–2	−1.46–3	−1.24–3	3.67–3	−2.43–3	
	3	−1.50–2	−7.46–3	1.28–3	3.29–3	−4.57–3		3	−1.59–2	−7.84–3	1.41–3	3.52–3	−4.94–3	
	5	−1.13–2	−3.28–3	−1.76–3	2.87–3	−1.11–3		5	−1.13–2	−3.59–3	−1.62–3	2.77–3	−1.15–3	
	10	−8.03–2	−8.45–3	−1.32–3	2.85–2	−2.72–2		10	−7.69–2	−7.98–3	−1.76–3	2.72–2	−2.54–2	
$5d_{5/2}$	1	−9.46–3	−2.70–3	4.13–4	2.79–3	−3.20–3	$5d_{5/2}$	1	−9.10–3	−2.49–3	3.46–4	2.72–3	−3.06–3	
	3	−6.07–3	−7.72–3	3.71–3	8.27–5	−3.80–3		3	−6.92–3	−8.09–3	3.81–3	2.94–4	−4.11–3	
	5	1.17–3	−3.63–3	3.69–3	−1.18–3	−2.51–3		5	1.30–3	−3.89–3	3.75–3	−1.33–3	−2.42–3	
	10	−6.45–2	−1.08–2	1.19–2	2.38–2	−3.58–2		10	−6.10–2	−1.02–2	1.16–2	2.26–2	−3.43–2	
$5f_{5/2}$	1	−1.30–4	−7.56–4	4.59–4	−1.59–4	−3.00–4	$5f_{5/2}$	1	−3.95–4	−8.98–4	4.77–4	−1.06–4	−3.71–4	
	3	−1.92–2	1.12–3	−1.88–3	7.76–3	−5.88–3		3	−1.78–2	1.31–3	−1.80–3	7.27–3	−5.47–3	
	5	−7.84–2	−5.43–3	−3.49–3	2.85–2	−2.50–2		5	−7.53–2	−4.81–3	−3.44–3	2.75–2	−2.41–2	
	10	−2.93–1	−4.14–2	−7.01–3	9.91–2	−9.21–2		10	−2.87–1	−4.00–2	−6.80–3	9.74–2	−9.06–2	
$5f_{7/2}$	1	2.86–3	−1.02–3	1.49–3	−1.25–3	−2.36–4	$5f_{7/2}$	1	2.60–3	−1.16–3	1.51–3	−1.20–3	−3.05–4	
	3	−1.22–2	1.27–4	1.25–3	5.16–3	−6.41–3		3	−1.08–2	3.20–4	1.29–3	4.69–3	−5.98–3	
	5	−6.84–2	−7.51–3	2.37–3	2.48–2	−2.72–2		5	−6.53–2	−6.87–3	2.40–3	2.38–2	−2.62–2	
	10	−2.78–1	−4.69–2	3.56–3	9.32–2	−9.68–2		10	−2.73–1	−4.55–2	3.90–3	9.16–2	−9.55–2	
$6s_{1/2}$	1	−1.27–3	8.65–3	2.81–3	4.53–3	−7.34–3	$6s_{1/2}$	1	−1.69–3	8.60–3	2.92–3	4.70–3	−7.62–3	
	3	−1.95–3	1.80–2	5.52–3	9.09–3	−1.46–2		3	−9.16–4	1.90–2	5.47–3	9.05–3	−1.45–2	
	5	−3.85–2	6.59–3	1.34–2	2.07–2	−3.41–2		5	−3.69–2	8.13–3	1.33–2	2.07–2	−3.40–2	
	10	−1.13–1	−2.81–2	2.65–2	3.93–2	−6.58–2		10	−1.14–1	−2.70–2	2.70–2	4.03–2	−6.73–2	
$6p_{1/2}$	1	3.52–3	1.06–2	3.38–3	3.50–3	−6.88–3	$6p_{1/2}$	1	3.25–3	1.06–2	3.71–3	3.70–3	−7.41–3	
	3	−2.94–2	2.10–3	5.11–3	1.36–2	−1.87–2		3	−2.86–2	3.15–3	5.10–3	1.37–2	−1.88–2	
	5	−5.17–2	−1.10–2	7.13–3	1.77–2	−2.48–2		5	−5.27–2	−1.06–2	7.48–3	1.83–2	−2.58–2	
	10	−3.96–2	−1.42–2	−1.49–4	1.01–2	−9.96–3		10	−4.16–2	−1.48–2	3.37–4	1.08–2	−1.11–2	
$6p_{3/2}$	1	3.92–3	4.94–3	1.26–3	6.62–4	−1.93–3	$6p_{3/2}$	1	3.89–3	4.94–3	1.33–3	6.83–4	−2.01–3	
	3	−2.68–2	−9.20–3	5.70–3	8.17–3	−1.39–2		3	−2.65–2	−8.95–3	5.59–3	8.14–3	−1.37–2	
	5	−3.71–2	−1.85–2	9.38–3	9.31–3	−1.87–2		5	−3.80–2	−1.87–2	9.58–3	9.62–3	−1.92–2	
	10	−2.53–2	−2.08–2	7.82–3	3.37–3	−1.12–2		10	−2.63–2	−2.14–2	8.20–3	3.60–3	−1.18–2	
$7s_{1/2}$	1	−1.37–3	7.75–3	2.58–3	4.16–3	−6.75–3	$6d_{3/2}$	1	−8.71–3	−3.57–4	−1.03–3	3.13–3	−2.10–3	
	3	−1.77–3	1.76–2	5.34–3	8.80–3	−1.41–2		3	−1.63–2	−8.03–3	1.61–3	3.64–3	−5.26–3	
	5	−3.77–2	6.56–3	1.32–2	2.03–2	−3.35–2		5	−1.14–2	−4.02–3	−1.39–3	2.68–3	−1.29–3	
	10	−1.12–1	−2.78–2	2.63–2	3.90–2	−6.53–2		10	−7.52–2	−8.10–3	−1.68–3	2.65–2	−2.48–2	
							$7s_{1/2}$	1	−1.68–3	7.70–3	2.67–3	4.29–3	−6.95–3	
								3	−6.93–4	1.85–2	5.28–3	8.74–3	−1.40–2	
								5	−3.61–2	8.06–3	1.31–2	2.03–2	−3.33–2	
								10	−1.13–1	−2.67–2	2.68–2	3.99–2	−6.67–2	

(continued on next page)

Table 1 (continued)

Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$	Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$
$Z = 97$ , Bk: $5f_{5/2}^6 5f_{7/2}^2 6d_{3/2}^1 7s_{1/2}^2$							$Z = 98$ , Cf: $5f_{5/2}^6 5f_{7/2}^4 7s_{1/2}^2$						
4s <sub>1/2</sub>	1	-4.58-3	2.08-2	7.35-3	1.16-2	-1.90-2	4s <sub>1/2</sub>	1	-6.21-3	2.10-2	7.92-3	1.25-2	-2.04-2
	3	-3.52-3	2.71-2	8.51-3	1.40-2	-2.25-2		3	-2.09-3	2.89-2	8.56-3	1.41-2	-2.26-2
	5	-4.75-2	1.06-2	1.72-2	2.67-2	-4.40-2		5	-4.57-2	1.28-2	1.72-2	2.68-2	-4.41-2
	10	-1.29-1	-2.91-2	3.09-2	4.61-2	-7.71-2		10	-1.30-1	-2.78-2	3.17-2	4.74-2	-7.91-2
4p <sub>1/2</sub>	1	-5.31-5	2.07-2	1.93-3	8.68-3	-1.06-2	4p <sub>1/2</sub>	1	-6.04-4	2.15-2	2.31-3	9.32-3	-1.16-2
	3	-4.85-2	-1.19-3	5.44-3	2.00-2	-2.54-2		3	-4.85-2	2.87-6	5.43-3	2.05-2	-2.59-2
	5	-6.70-2	-1.49-2	7.29-3	2.23-2	-2.96-2		5	-6.91-2	-1.47-2	7.69-3	2.33-2	-3.10-2
	10	-4.50-2	-1.51-2	-5.75-4	1.18-2	-1.13-2		10	-4.77-2	-1.58-2	-5.65-5	1.27-2	-1.27-2
4p <sub>3/2</sub>	1	3.43-3	6.94-3	7.73-4	1.56-3	-2.33-3	4p <sub>3/2</sub>	1	3.69-3	7.16-3	8.36-4	1.55-3	-2.39-3
	3	-3.75-2	-1.38-2	7.03-3	1.09-2	-1.79-2		3	-3.76-2	-1.37-2	6.93-3	1.10-2	-1.79-2
	5	-4.39-2	-2.21-2	1.07-2	1.09-2	-2.16-2		5	-4.54-2	-2.26-2	1.10-2	1.13-2	-2.23-2
	10	-2.60-2	-2.15-2	8.61-3	3.53-3	-1.21-2		10	-2.72-2	-2.23-2	9.07-3	3.79-3	-1.29-2
4d <sub>3/2</sub>	1	-2.76-2	-8.40-3	-2.97-3	7.09-3	-4.13-3	4d <sub>3/2</sub>	1	-2.80-2	-8.39-3	-3.28-3	7.20-3	-3.92-3
	3	-1.60-2	-7.47-3	4.41-4	3.50-3	-3.94-3		3	-1.73-2	-8.05-3	5.71-4	3.81-3	-4.38-3
	5	-1.11-2	-1.42-3	-2.94-3	3.30-3	-3.68-4		5	-1.10-2	-1.72-3	-2.82-3	3.17-3	-3.48-4
	10	-8.35-2	-6.46-3	-3.00-3	3.02-2	-2.72-2		10	-8.00-2	-5.88-3	-3.51-3	2.90-2	-2.55-2
4d <sub>5/2</sub>	1	-2.15-2	-9.19-3	3.02-4	5.00-3	-5.30-3	4d <sub>5/2</sub>	1	-2.18-2	-9.21-3	1.28-4	5.08-3	-5.20-3
	3	-4.17-3	-7.51-3	3.85-3	-5.64-4	-3.29-3		3	-5.22-3	-8.06-3	4.00-3	-3.35-4	-3.66-3
	5	3.46-3	-1.78-3	3.67-3	-1.36-3	-2.31-3		5	3.79-3	-2.01-3	3.75-3	-1.57-3	-2.17-3
	10	-6.65-2	-9.02-3	1.16-2	2.53-2	-3.69-2		10	-6.28-2	-8.33-3	1.14-2	2.41-2	-3.54-2
4f <sub>5/2</sub>	1	5.78-3	3.32-3	1.40-5	-9.81-4	9.67-4	4f <sub>5/2</sub>	1	6.21-3	3.43-3	7.89-5	-1.09-3	1.01-3
	3	-2.32-2	4.41-3	-3.42-3	1.04-2	-6.94-3		3	-2.15-2	4.91-3	-3.41-3	9.89-3	-6.48-3
	5	-8.82-2	-3.70-3	-5.17-3	3.28-2	-2.76-2		5	-8.55-2	-2.92-3	-5.21-3	3.20-2	-2.68-2
	10	-3.05-1	-4.10-2	-8.74-3	1.04-1	-9.53-2		10	-3.01-1	-3.97-2	-8.68-3	1.03-1	-9.41-2
4f <sub>7/2</sub>	1	1.01-2	2.87-3	1.57-3	-2.57-3	1.00-3	4f <sub>7/2</sub>	1	1.06-2	2.98-3	1.68-3	-2.73-3	1.05-3
	3	-1.51-2	3.18-3	2.41-4	7.37-3	-7.61-3		3	-1.33-2	3.68-3	2.63-4	6.86-3	-7.13-3
	5	-7.73-2	-6.01-3	1.17-3	2.87-2	-2.99-2		5	-7.46-2	-5.23-3	1.16-3	2.80-2	-2.91-2
	10	-2.90-1	-4.67-2	2.33-3	9.79-2	-1.00-1		10	-2.86-1	-4.54-2	2.58-3	9.67-2	-9.93-2
5s <sub>1/2</sub>	1	-2.37-3	1.10-2	3.81-3	6.09-3	-9.90-3	5s <sub>1/2</sub>	1	-3.20-3	1.09-2	4.05-3	6.45-3	-1.05-2
	3	-1.60-4	2.14-2	5.91-3	9.81-3	-1.57-2		3	1.04-3	2.26-2	5.87-3	9.80-3	-1.57-2
	5	-3.70-2	1.01-2	1.39-2	2.16-2	-3.55-2		5	-3.50-2	1.19-2	1.38-2	2.15-2	-3.53-2
	10	-1.17-1	-2.64-2	2.81-2	4.20-2	-7.01-2		10	-1.18-1	-2.51-2	2.87-2	4.30-2	-7.17-2
5p <sub>1/2</sub>	1	3.36-3	1.31-2	3.92-3	4.67-3	-8.59-3	5p <sub>1/2</sub>	1	2.96-3	1.33-2	4.48-3	5.04-3	-9.52-3
	3	-3.08-2	3.46-3	5.09-3	1.47-2	-1.98-2		3	-2.99-2	4.77-3	5.07-3	1.49-2	-2.00-2
	5	-5.53-2	-1.08-2	7.63-3	1.94-2	-2.70-2		5	-5.65-2	-1.02-2	8.00-3	2.01-2	-2.81-2
	10	-4.37-2	-1.52-2	5.80-4	1.15-2	-1.21-2		10	-4.61-2	-1.57-2	1.14-3	1.24-2	-1.35-2
5p <sub>3/2</sub>	1	4.17-3	5.44-3	1.31-3	7.68-4	-2.08-3	5p <sub>3/2</sub>	1	4.24-3	5.51-3	1.42-3	7.93-4	-2.21-3
	3	-2.75-2	-9.34-3	5.66-3	8.42-3	-1.41-2		3	-2.72-2	-9.04-3	5.53-3	8.39-3	-1.39-2
	5	-3.92-2	-1.93-2	9.81-3	9.96-3	-1.98-2		5	-4.02-2	-1.95-2	1.00-2	1.03-2	-2.03-2
	10	-2.69-2	-2.18-2	8.55-3	3.77-3	-1.23-2		10	-2.81-2	-2.25-2	9.00-3	4.06-3	-1.31-2
5d <sub>3/2</sub>	1	-1.08-2	-1.15-3	-1.32-3	3.59-3	-2.26-3	5d <sub>3/2</sub>	1	-1.02-2	-7.43-4	-1.41-3	3.49-3	-2.08-3
	3	-1.69-2	-8.24-3	1.54-3	3.78-3	-5.33-3		3	-1.81-2	-8.69-3	1.67-3	4.08-3	-5.76-3
	5	-1.14-2	-3.94-3	-1.46-3	2.69-3	-1.23-3		5	-1.16-2	-4.33-3	-1.28-3	2.65-3	-1.37-3
	10	-7.35-2	-7.52-3	-2.20-3	2.59-2	-2.37-2		10	-7.01-2	-7.09-3	-2.63-3	2.47-2	-2.21-2
5d <sub>5/2</sub>	1	-8.69-3	-2.22-3	2.71-4	2.64-3	-2.91-3	5d <sub>5/2</sub>	1	-8.16-3	-1.87-3	1.87-4	2.56-3	-2.74-3
	3	-7.86-3	-8.50-3	3.93-3	5.29-4	-4.46-3		3	-8.93-3	-8.97-3	4.06-3	7.98-4	-4.86-3
	5	1.36-3	-4.19-3	3.82-3	-1.46-3	-2.36-3		5	1.33-3	-4.53-3	3.91-3	-1.57-3	-2.35-3
	10	-5.75-2	-9.66-3	1.14-2	2.14-2	-3.28-2		10	-5.41-2	-9.11-3	1.11-2	2.02-2	-3.13-2
5f <sub>5/2</sub>	1	-7.16-4	-1.06-3	4.96-4	-3.99-5	-4.56-4	5f <sub>5/2</sub>	1	-1.11-3	-1.26-3	5.14-4	4.31-5	-5.57-4
	3	-1.64-2	1.49-3	-1.72-3	6.80-3	-5.07-3		3	-1.49-2	1.67-3	-1.65-3	6.32-3	-4.67-3
	5	-7.22-2	-4.21-3	-3.39-3	2.65-2	-2.31-2		5	-6.92-2	-3.62-3	-3.35-3	2.56-2	-2.22-2
	10	-2.81-1	-3.86-2	-6.64-3	9.58-2	-8.91-2		10	-2.76-1	-3.73-2	-6.49-3	9.41-2	-8.76-2
5f <sub>7/2</sub>	1	2.30-3	-1.32-3	1.53-3	-1.14-3	-3.87-4	5f <sub>7/2</sub>	1	1.95-3	-1.51-3	1.56-3	-1.07-3	-4.86-4
	3	-9.35-3	5.18-4	1.33-3	4.21-3	-5.54-3		3	-7.89-3	7.22-4	1.38-3	3.72-3	-5.10-3
	5	-6.22-2	-6.24-3	2.42-3	2.29-2	-2.53-2		5	-5.92-2	-5.62-3	2.44-3	2.19-2	-2.44-2
	10	-2.67-1	-4.41-2	4.22-3	9.01-2	-9.43-2		10	-2.62-1	-4.27-2	4.53-3	8.85-2	-9.30-2

Table 1 (continued)

Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$	Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$
6s <sub>1/2</sub>	1	-2.20-3	8.51-3	3.06-3	4.90-3	-7.95-3	6s <sub>1/2</sub>	1	-2.84-3	8.38-3	3.22-3	5.13-3	-8.35-3
	3	1.90-4	2.00-2	5.42-3	9.01-3	-1.44-2		3	1.35-3	2.11-2	5.37-3	8.98-3	-1.44-2
	5	-3.51-2	9.77-3	1.32-2	2.06-2	-3.38-2		5	-3.32-2	1.15-2	1.31-2	2.05-2	-3.36-2
	10	-1.15-1	-2.58-2	2.76-2	4.12-2	-6.88-2		10	-1.16-1	-2.45-2	2.81-2	4.21-2	-7.02-2
6p <sub>1/2</sub>	1	2.92-3	1.07-2	4.13-3	3.92-3	-8.05-3	6p <sub>1/2</sub>	1	2.48-3	1.06-2	4.61-3	4.16-3	-8.77-3
	3	-2.77-2	4.34-3	5.08-3	1.38-2	-1.89-2		3	-2.66-2	5.67-3	5.04-3	1.39-2	-1.90-2
	5	-5.36-2	-1.01-2	7.83-3	1.90-2	-2.68-2		5	-5.44-2	-9.47-3	8.18-3	1.96-2	-2.78-2
	10	-4.38-2	-1.53-2	8.67-4	1.16-2	-1.25-2		10	-4.62-2	-1.58-2	1.45-3	1.24-2	-1.39-2
6p <sub>3/2</sub>	1	3.88-3	4.94-3	1.41-3	7.06-4	-2.12-3	6p <sub>3/2</sub>	1	3.87-3	4.95-3	1.52-3	7.35-4	-2.26-3
	3	-2.61-2	-8.65-3	5.47-3	8.09-3	-1.36-2		3	-2.57-2	-8.29-3	5.33-3	8.03-3	-1.34-2
	5	-3.89-2	-1.89-2	9.76-3	9.93-3	-1.97-2		5	-3.98-2	-1.91-2	9.93-3	1.03-2	-2.02-2
	10	-2.74-2	-2.20-2	8.61-3	3.86-3	-1.25-2		10	-2.85-2	-2.27-2	9.06-3	4.16-3	-1.32-2
6d <sub>3/2</sub>	1	-8.08-3	-3.66-6	-1.08-3	3.02-3	-1.94-3	7s <sub>1/2</sub>	1	-2.82-3	7.26-3	2.89-3	4.61-3	-7.50-3
	3	-1.73-2	-8.39-3	1.74-3	3.90-3	-5.64-3		3	1.49-3	2.05-2	5.16-3	8.63-3	-1.38-2
	5	-1.15-2	-4.39-3	-1.21-3	2.62-3	-1.41-3		5	-3.23-2	1.14-2	1.28-2	2.00-2	-3.29-2
	10	-7.18-2	-7.68-3	-2.11-3	2.52-2	-2.31-2		10	-1.14-1	-2.42-2	2.79-2	4.17-2	-6.96-2
7s <sub>1/2</sub>	1	-2.18-3	7.51-3	2.77-3	4.43-3	-7.20-3							
	3	2.50-4	1.94-2	5.24-3	8.71-3	-1.39-2							
	5	-3.43-2	9.67-3	1.29-2	2.02-2	-3.31-2							
	10	-1.14-1	-2.55-2	2.73-2	4.08-2	-6.82-2							
<i>Z</i> = 99, Es: 5f <sub>5/2</sub> <sup>6</sup> 5f <sub>7/2</sub> <sup>5</sup> 7s <sub>1/2</sub> <sup>2</sup>							<i>Z</i> = 100, Fm: 5f <sub>5/2</sub> <sup>6</sup> 5f <sub>7/2</sub> <sup>6</sup> 7s <sub>1/2</sub> <sup>2</sup>						
4s <sub>1/2</sub>	1	-7.75-3	2.11-2	8.45-3	1.32-2	-2.17-2	4s <sub>1/2</sub>	1	-9.41-3	2.12-2	9.01-3	1.40-2	-2.30-2
	3	-7.90-4	3.05-2	8.62-3	1.42-2	-2.29-2		3	4.59-4	3.21-2	8.70-3	1.44-2	-2.31-2
	5	-4.37-2	1.50-2	1.72-2	2.69-2	-4.42-2		5	-4.17-2	1.73-2	1.72-2	2.70-2	-4.43-2
	10	-1.32-1	-2.64-2	3.24-2	4.85-2	-8.10-2		10	-1.32-1	-2.48-2	3.31-2	4.97-2	-8.28-2
4p <sub>1/2</sub>	1	-1.28-3	2.23-2	2.69-3	9.97-3	-1.27-2	4p <sub>1/2</sub>	1	-2.11-3	2.31-2	3.13-3	1.07-2	-1.38-2
	3	-4.84-2	1.22-3	5.40-3	2.09-2	-2.63-2		3	-4.83-2	2.55-3	5.37-3	2.14-2	-2.68-2
	5	-7.10-2	-1.43-2	8.06-3	2.43-2	-3.23-2		5	-7.30-2	-1.40-2	8.44-3	2.53-2	-3.37-2
	10	-5.04-2	-1.65-2	4.96-4	1.37-2	-1.42-2		10	-5.34-2	-1.72-2	1.09-3	1.47-2	-1.58-2
4p <sub>3/2</sub>	1	3.84-3	7.31-3	8.89-4	1.57-3	-2.46-3	4p <sub>3/2</sub>	1	3.97-3	7.47-3	9.50-4	1.59-3	-2.54-3
	3	-3.77-2	-1.36-2	6.81-3	1.10-2	-1.78-2		3	-3.78-2	-1.34-2	6.69-3	1.11-2	-1.78-2
	5	-4.67-2	-2.30-2	1.13-2	1.17-2	-2.30-2		5	-4.80-2	-2.34-2	1.15-2	1.21-2	-2.36-2
	10	-2.84-2	-2.30-2	9.55-3	4.08-3	-1.36-2		10	-2.97-2	-2.37-2	1.01-2	4.40-3	-1.45-2
4d <sub>3/2</sub>	1	-2.83-2	-8.36-3	-3.55-3	7.27-3	-3.72-3	4d <sub>3/2</sub>	1	-2.85-2	-8.30-3	-3.82-3	7.31-3	-3.49-3
	3	-1.85-2	-8.60-3	6.86-4	4.10-3	-4.79-3		3	-1.98-2	-9.16-3	7.94-4	4.41-3	-5.20-3
	5	-1.10-2	-2.03-3	-2.69-3	3.06-3	-3.73-4		5	-1.11-2	-2.37-3	-2.55-3	2.99-3	-4.41-4
	10	-7.67-2	-5.34-3	-3.98-3	2.77-2	-2.38-2		10	-7.34-2	-4.83-3	-4.44-3	2.65-2	-2.21-2
4d <sub>5/2</sub>	1	-2.21-2	-9.26-3	-2.25-5	5.14-3	-5.11-3	4d <sub>5/2</sub>	1	-2.23-2	-9.28-3	-1.78-4	5.18-3	-5.00-3
	3	-6.25-3	-8.60-3	4.14-3	-1.09-4	-4.03-3		3	-7.33-3	-9.14-3	4.28-3	1.31-4	-4.41-3
	5	4.03-3	-2.27-3	3.83-3	-1.75-3	-2.08-3		5	4.19-3	-2.55-3	3.92-3	-1.91-3	-2.02-3
	10	-5.94-2	-7.69-3	1.11-2	2.29-2	-3.40-2		10	-5.60-2	-7.08-3	1.09-2	2.18-2	-3.27-2
4f <sub>5/2</sub>	1	6.58-3	3.53-3	1.38-4	-1.19-3	1.05-3	4f <sub>5/2</sub>	1	6.94-3	3.63-3	1.98-4	-1.29-3	1.09-3
	3	-1.99-2	5.37-3	-3.39-3	9.45-3	-6.05-3		3	-1.84-2	5.83-3	-3.37-3	9.01-3	-5.63-3
	5	-8.29-2	-2.15-3	-5.24-3	3.12-2	-2.60-2		5	-8.02-2	-1.39-3	-5.26-3	3.05-2	-2.52-2
	10	-2.96-1	-3.83-2	-8.62-3	1.01-1	-9.28-2		10	-2.92-1	-3.70-2	-8.58-3	1.00-1	-9.16-2
4f <sub>7/2</sub>	1	1.11-2	3.07-3	1.78-3	-2.87-3	1.09-3	4f <sub>7/2</sub>	1	1.16-2	3.16-3	1.88-3	-3.01-3	1.13-3
	3	-1.17-2	4.15-3	2.83-4	6.39-3	-6.68-3		3	-1.00-2	4.61-3	3.07-4	5.92-3	-6.23-3
	5	-7.19-2	-4.46-3	1.15-3	2.72-2	-2.83-2		5	-6.92-2	-3.69-3	1.13-3	2.64-2	-2.76-2
	10	-2.81-1	-4.41-2	2.81-3	9.55-2	-9.83-2		10	-2.77-1	-4.28-2	3.03-3	9.43-2	-9.73-2
5s <sub>1/2</sub>	1	-3.96-3	1.08-2	4.26-3	6.75-3	-1.10-2	5s <sub>1/2</sub>	1	-4.77-3	1.06-2	4.47-3	7.05-3	-1.15-2
	3	2.12-3	2.37-2	5.86-3	9.81-3	-1.57-2		3	3.15-3	2.48-2	5.85-3	9.83-3	-1.57-2
	5	-3.31-2	1.37-2	1.37-2	2.15-2	-3.51-2		5	-3.11-2	1.56-2	1.36-2	2.14-2	-3.49-2
	10	-1.19-1	-2.36-2	2.93-2	4.39-2	-7.31-2		10	-1.19-1	-2.19-2	2.98-2	4.47-2	-7.45-2
5p <sub>1/2</sub>	1	2.48-3	1.35-2	5.01-3	5.40-3	-1.04-2	5p <sub>1/2</sub>	1	1.91-3	1.36-2	5.59-3	5.80-3	-1.14-2
	3	-2.90-2	6.09-3	5.04-3	1.51-2	-2.01-2		3	-2.80-2	7.50-3	5.01-3	1.52-2	-2.02-2
	5	-5.74-2	-9.61-3	8.34-3	2.08-2	-2.91-2		5	-5.83-2	-8.89-3	8.67-3	2.15-2	-3.02-2
	10	-4.86-2	-1.62-2	1.74-3	1.33-2	-1.50-2		10	-5.12-2	-1.67-2	2.37-3	1.43-2	-1.66-2

(continued on next page)

Table 1 (continued)

Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$	Shell	<i>E</i>	$\Delta\beta_{\text{unp}}$	$\Delta\beta_{lp}$	$\eta$	$\mu$	$\xi$
5p <sub>3/2</sub>	1	4.25–3	5.56–3	1.52–3	8.29–4	−2.35–3	5p <sub>3/2</sub>	1	4.22–3	5.59–3	1.62–3	8.72–4	−2.49–3
	3	−2.69–2	−8.74–3	5.40–3	8.35–3	−1.37–2		3	−2.65–2	−8.42–3	5.25–3	8.29–3	−1.35–2
	5	−4.11–2	−1.97–2	1.02–2	1.06–2	−2.08–2		5	−4.20–2	−1.99–2	1.03–2	1.09–2	−2.12–2
	10	−2.93–2	−2.31–2	9.47–3	4.36–3	−1.38–2		10	−3.06–2	−2.38–2	9.96–3	4.69–3	−1.47–2
5d <sub>3/2</sub>	1	−9.65–3	−3.96–4	−1.47–3	3.41–3	−1.93–3	5d <sub>3/2</sub>	1	−9.10–3	−3.27–5	−1.53–3	3.32–3	−1.79–3
	3	−1.92–2	−9.12–3	1.79–3	4.37–3	−6.17–3		3	−2.03–2	−9.54–3	1.90–3	4.67–3	−6.57–3
	5	−1.19–2	−4.73–3	−1.08–3	2.63–3	−1.55–3		5	−1.22–2	−5.16–3	−8.78–4	2.65–3	−1.77–3
	10	−6.70–2	−6.70–3	−3.03–3	2.35–2	−2.05–2		10	−6.40–2	−6.36–3	−3.40–3	2.24–2	−1.90–2
5d <sub>5/2</sub>	1	−7.65–3	−1.56–3	1.20–4	2.46–3	−2.58–3	5d <sub>5/2</sub>	1	−7.10–3	−1.24–3	6.06–5	2.35–3	−2.42–3
	3	−9.93–3	−9.38–3	4.17–3	1.05–3	−5.22–3		3	−1.10–2	−9.80–3	4.28–3	1.32–3	−5.60–3
	5	1.21–3	−4.88–3	4.01–3	−1.64–3	−2.37–3		5	1.01–3	−5.26–3	4.12–3	−1.68–3	−2.43–3
	10	−5.08–2	−8.60–3	1.09–2	1.90–2	−3.00–2		10	−4.76–2	−8.14–3	1.07–2	1.79–2	−2.86–2
5f <sub>5/2</sub>	1	−1.51–3	−1.44–3	5.22–4	1.33–4	−6.55–4	5f <sub>5/2</sub>	1	−1.95–3	−1.63–3	5.23–4	2.34–4	−7.57–4
	3	−1.36–2	1.82–3	−1.57–3	5.87–3	−4.30–3		3	−1.24–2	1.95–3	−1.50–3	5.44–3	−3.95–3
	5	−6.63–2	−3.06–3	−3.30–3	2.46–2	−2.13–2		5	−6.34–2	−2.51–3	−3.24–3	2.37–2	−2.05–2
	10	−2.70–1	−3.59–2	−6.35–3	9.24–2	−8.61–2		10	−2.65–1	−3.46–2	−6.22–3	9.08–2	−8.46–2
5f <sub>7/2</sub>	1	1.58–3	−1.68–3	1.57–3	−9.90–4	−5.82–4	5f <sub>7/2</sub>	1	1.16–3	−1.87–3	1.58–3	−8.97–4	−6.83–4
	3	−6.58–3	8.91–4	1.42–3	3.27–3	−4.69–3		3	−5.31–3	1.04–3	1.46–3	2.83–3	−4.29–3
	5	−5.63–2	−5.04–3	2.46–3	2.10–2	−2.35–2		5	−5.34–2	−4.47–3	2.48–3	2.01–2	−2.26–2
	10	−2.56–1	−4.13–2	4.81–3	8.69–2	−9.17–2		10	−2.51–1	−4.00–2	5.08–3	8.53–2	−9.04–2
6s <sub>1/2</sub>	1	−3.40–3	8.17–3	3.33–3	5.29–3	−8.63–3	6s <sub>1/2</sub>	1	−3.97–3	7.93–3	3.44–3	5.45–3	−8.89–3
	3	2.38–3	2.21–2	5.33–3	8.95–3	−1.43–2		3	3.37–3	2.30–2	5.31–3	8.93–3	−1.42–2
	5	−3.12–2	1.32–2	1.30–2	2.04–2	−3.34–2		5	−2.92–2	1.50–2	1.28–2	2.03–2	−3.31–2
	10	−1.16–1	−2.30–2	2.86–2	4.29–2	−7.16–2		10	−1.16–1	−2.13–2	2.91–2	4.37–2	−7.28–2
6p <sub>1/2</sub>	1	2.00–3	1.04–2	5.06–3	4.39–3	−9.44–3	6p <sub>1/2</sub>	1	1.51–3	1.05–2	5.63–3	4.71–3	−1.03–2
	3	−2.55–2	7.01–3	4.99–3	1.40–2	−1.90–2		3	−2.44–2	8.49–3	4.98–3	1.41–2	−1.91–2
	5	−5.52–2	−8.78–3	8.51–3	2.03–2	−2.88–2		5	−5.60–2	−8.01–3	8.86–3	2.10–2	−2.98–2
	10	−4.85–2	−1.62–2	2.06–3	1.33–2	−1.54–2		10	−5.11–2	−1.67–2	2.71–3	1.43–2	−1.70–2
6p <sub>3/2</sub>	1	3.79–3	4.91–3	1.61–3	7.70–4	−2.38–3	6p <sub>3/2</sub>	1	3.69–3	4.87–3	1.70–3	8.10–4	−2.51–3
	3	−2.52–2	−7.94–3	5.18–3	7.95–3	−1.31–2		3	−2.47–2	−7.56–3	5.02–3	7.86–3	−1.29–2
	5	−4.06–2	−1.93–2	1.01–2	1.05–2	−2.06–2		5	−4.13–2	−1.94–2	1.02–2	1.08–2	−2.10–2
	10	−2.97–2	−2.33–2	9.53–3	4.47–3	−1.40–2		10	−3.10–2	−2.40–2	1.00–2	4.81–3	−1.48–2
7s <sub>1/2</sub>	1	−3.29–3	7.12–3	3.00–3	4.76–3	−7.76–3	7s <sub>1/2</sub>	1	−3.80–3	6.94–3	3.10–3	4.92–3	−8.02–3
	3	2.64–3	2.15–2	5.11–3	8.57–3	−1.37–2		3	3.80–3	2.26–2	5.06–3	8.53–3	−1.36–2
	5	−3.04–2	1.31–2	1.27–2	1.99–2	−3.26–2		5	−2.85–2	1.48–2	1.26–2	1.98–2	−3.24–2
	10	−1.15–1	−2.27–2	2.83–2	4.25–2	−7.09–2		10	−1.15–1	−2.11–2	2.88–2	4.33–2	−7.21–2

Table 2

Subshell photoionization cross section and angular distribution parameters of the zero and first orders for photoelectron energy  $E = 10$  keV. See page 252 for Explanation of Tables

Z	Shell	$\sigma$	$\beta$	$\gamma$	$\delta$
1	1s <sub>1/2</sub>	9.083–6	1.960+0	2.322+0	5.716–5
2	1s <sub>1/2</sub>	1.913–4	1.959+0	2.302+0	6.133–5
3	1s <sub>1/2</sub>	1.495–3	1.961+0	2.312+0	6.368–5
	2s <sub>1/2</sub>	4.488–5	1.960+0	2.312+0	6.618–5
4	1s <sub>1/2</sub>	5.755–3	1.961+0	2.302+0	6.741–5
	2s <sub>1/2</sub>	2.356–4	1.961+0	2.302+0	6.492–5
5	1s <sub>1/2</sub>	1.577–2	1.961+0	2.293+0	7.146–5
	2s <sub>1/2</sub>	8.198–4	1.962+0	2.287+0	6.443–5
	2p <sub>1/2</sub>	2.424–6	3.623–2	7.881–1	3.690–1
6	1s <sub>1/2</sub>	3.493–2	1.961+0	2.280+0	7.620–5
	2s <sub>1/2</sub>	2.025–3	1.962+0	2.268+0	6.547–5
	2p <sub>1/2</sub>	1.031–5	5.031–2	8.007–1	3.633–1
7	1s <sub>1/2</sub>	6.682–2	1.961+0	2.268+0	8.100–5
	2s <sub>1/2</sub>	4.154–3	1.963+0	2.247+0	6.616–5
	2p <sub>1/2</sub>	3.202–5	6.716–2	8.089–1	3.590–1
	2p <sub>3/2</sub>	6.258–5	4.686–2	7.819–1	3.667–1
8	1s <sub>1/2</sub>	1.148–1	1.961+0	2.256+0	8.597–5
	2s <sub>1/2</sub>	7.542–3	1.963+0	2.227+0	6.686–5
	2p <sub>1/2</sub>	8.153–5	8.339–2	8.192–1	3.542–1
	2p <sub>3/2</sub>	1.589–4	6.229–2	7.912–1	3.616–1
9	1s <sub>1/2</sub>	1.820–1	1.961+0	2.247+0	9.097–5
	2s <sub>1/2</sub>	1.255–2	1.964+0	2.207+0	6.670–5
	2p <sub>1/2</sub>	1.813–4	1.067–1	8.515–1	3.481–1
	2p <sub>3/2</sub>	3.521–4	8.497–2	8.232–1	3.554–1
10	1s <sub>1/2</sub>	2.705–1	1.961+0	2.237+0	9.552–5
	2s <sub>1/2</sub>	1.956–2	1.965+0	2.183+0	6.667–5
	2p <sub>1/2</sub>	3.648–4	1.380–1	8.902–1	3.409–1
	2p <sub>3/2</sub>	7.065–4	1.158–1	8.613–1	3.481–1
11	1s <sub>1/2</sub>	3.803–1	1.961+0	2.228+0	9.988–5
	2s <sub>1/2</sub>	3.052–2	1.965+0	2.157+0	6.663–5
	2p <sub>1/2</sub>	7.602–4	1.725–1	9.269–1	3.334–1
	2p <sub>3/2</sub>	1.469–3	1.499–1	8.979–1	3.407–1
	3s <sub>1/2</sub>	9.546–4	1.965+0	2.156+0	6.352–5
12	1s <sub>1/2</sub>	5.116–1	1.961+0	2.218+0	1.037–4
	2s <sub>1/2</sub>	4.531–2	1.966+0	2.130+0	6.650–5
	2p <sub>1/2</sub>	1.431–3	2.073–1	9.600–1	3.258–1
	2p <sub>3/2</sub>	2.760–3	1.844–1	9.310–1	3.331–1
	3s <sub>1/2</sub>	2.336–3	1.966+0	2.127+0	6.367–5
13	1s <sub>1/2</sub>	6.631–1	1.961+0	2.207+0	1.072–4
	2s <sub>1/2</sub>	6.444–2	1.967+0	2.102+0	6.627–5
	2p <sub>1/2</sub>	2.505–3	2.416–1	9.898–1	3.182–1
	2p <sub>3/2</sub>	4.817–3	2.184–1	9.610–1	3.256–1
	3s <sub>1/2</sub>	4.781–3	1.967+0	2.096+0	6.307–5
	3p <sub>1/2</sub>	1.023–4	2.391–1	9.863–1	3.176–1
14	1s <sub>1/2</sub>	8.328–1	1.961+0	2.196+0	1.103–4
	2s <sub>1/2</sub>	8.836–2	1.968+0	2.072+0	6.590–5
	2p <sub>1/2</sub>	4.130–3	2.753–1	1.019+0	3.106–1
	2p <sub>3/2</sub>	7.918–3	2.520–1	9.902–1	3.180–1
	3s <sub>1/2</sub>	7.836–3	1.968+0	2.065+0	6.231–5
	3p <sub>1/2</sub>	2.392–4	2.720–1	1.014+0	3.096–1
15	2s <sub>1/2</sub>	1.174–1	1.969+0	2.043+0	6.535–5
	2p <sub>1/2</sub>	6.481–3	3.086–1	1.048+0	3.030–1
	2p <sub>3/2</sub>	1.239–2	2.854–1	1.020+0	3.103–1
	3s <sub>1/2</sub>	1.170–2	1.969+0	2.032+0	6.177–5
	3p <sub>1/2</sub>	4.615–4	3.049–1	1.041+0	3.013–1
	3p <sub>3/2</sub>	8.808–4	2.815–1	1.013+0	3.083–1

Table 2 (continued)

Z	Shell	$\sigma$	$\beta$	$\gamma$	$\delta$
16	2s <sub>1/2</sub>	1.520–1	1.969+0	2.012+0	6.458–5
	2p <sub>1/2</sub>	9.762–3	3.422–1	1.078+0	2.953–1
	2p <sub>3/2</sub>	1.861–2	3.192–1	1.051+0	3.024–1
	3s <sub>1/2</sub>	1.649–2	1.970+0	1.999+0	6.051–5
	3p <sub>1/2</sub>	8.004–4	3.377–1	1.070+0	2.930–1
	3p <sub>3/2</sub>	1.523–3	3.145–1	1.042+0	2.997–1
17	2s <sub>1/2</sub>	1.922–1	1.970+0	1.980+0	6.357–5
	2p <sub>1/2</sub>	1.420–2	3.763–1	1.110+0	2.875–1
	2p <sub>3/2</sub>	2.698–2	3.535–1	1.084+0	2.945–1
	3s <sub>1/2</sub>	2.229–2	1.971+0	1.965+0	5.889–5
	3p <sub>1/2</sub>	1.293–3	3.712–1	1.099+0	2.845–1
	3p <sub>3/2</sub>	2.452–3	3.483–1	1.072+0	2.912–1
18	2s <sub>1/2</sub>	2.384–1	1.971+0	1.948+0	6.229–5
	2p <sub>1/2</sub>	2.004–2	4.110–1	1.143+0	2.798–1
	2p <sub>3/2</sub>	3.796–2	3.887–1	1.117+0	2.866–1
	3s <sub>1/2</sub>	2.918–2	1.972+0	1.929+0	5.735–5
	3p <sub>1/2</sub>	1.983–3	4.054–1	1.129+0	2.762–1
	3p <sub>3/2</sub>	3.746–3	3.829–1	1.104+0	2.826–1
19	2s <sub>1/2</sub>	2.901–1	1.972+0	1.914+0	6.095–5
	2p <sub>1/2</sub>	2.750–2	4.457–1	1.175+0	2.720–1
	2p <sub>3/2</sub>	5.193–2	4.240–1	1.151+0	2.787–1
	3s <sub>1/2</sub>	3.898–2	1.973+0	1.892+0	5.569–5
	3p <sub>1/2</sub>	3.229–3	4.396–1	1.159+0	2.675–1
	3p <sub>3/2</sub>	6.091–3	4.176–1	1.135+0	2.738–1
20	2s <sub>1/2</sub>	3.477–1	1.973+0	1.879+0	5.934–5
	2p <sub>1/2</sub>	3.688–2	4.804–1	1.208+0	2.644–1
	2p <sub>3/2</sub>	6.942–2	4.595–1	1.185+0	2.708–1
	3s <sub>1/2</sub>	5.069–2	1.974+0	1.853+0	5.366–5
	3p <sub>1/2</sub>	4.900–3	4.740–1	1.189+0	2.591–1
	3p <sub>3/2</sub>	9.223–3	4.527–1	1.166+0	2.651–1
21	2s <sub>1/2</sub>	4.116–1	1.974+0	1.843+0	5.723–5
	2p <sub>1/2</sub>	4.861–2	5.156–1	1.241+0	2.568–1
	2p <sub>3/2</sub>	9.121–2	4.956–1	1.220+0	2.629–1
	3s <sub>1/2</sub>	6.248–2	1.975+0	1.814+0	5.116–5
	3p <sub>1/2</sub>	6.817–3	5.090–1	1.218+0	2.506–1
	3p <sub>3/2</sub>	1.279–2	4.885–1	1.197+0	2.564–1
22	2s <sub>1/2</sub>	4.813–1	1.975+0	1.806+0	5.476–5
	2p <sub>1/2</sub>	6.291–2	5.507–1	1.273+0	2.492–1
	2p <sub>3/2</sub>	1.177–1	5.316–1	1.254+0	2.552–1
	3s <sub>1/2</sub>	7.552–2	1.977+0	1.773+0	4.838–5
	3d <sub>3/2</sub>	7.014–5	2.122–1	7.377–1	5.461–1
	4s <sub>1/2</sub>	4.843–3	1.976+0	1.812+0	5.003–5
23	2s <sub>1/2</sub>	5.565–1	1.976+0	1.767+0	5.189–5
	2p <sub>1/2</sub>	8.007–2	5.854–1	1.303+0	2.419–1
	2p <sub>3/2</sub>	1.493–1	5.675–1	1.286+0	2.475–1
	3s <sub>1/2</sub>	8.986–2	1.978+0	1.732+0	4.544–5
	3p <sub>1/2</sub>	1.215–2	5.784–1	1.271+0	2.342–1
	3p <sub>3/2</sub>	2.263–2	5.601–1	1.253+0	2.394–1
24	2s <sub>1/2</sub>	6.378–1	1.977+0	1.729+0	4.843–5
	2p <sub>1/2</sub>	1.006–1	6.199–1	1.333+0	2.347–1
	2p <sub>3/2</sub>	1.869–1	6.034–1	1.318+0	2.401–1
	3s <sub>1/2</sub>	1.041–1	1.979+0	1.691+0	4.177–5
	3p <sub>1/2</sub>	1.540–2	6.127–1	1.296+0	2.262–1
	3p <sub>3/2</sub>	2.815–1	3.083–1		

(continued on next page)

Table 2 (continued)

Z	Shell	$\sigma$	$\beta$	$\gamma$	$\delta$
25	3p <sub>3/2</sub>	2.855–2	5.957–1	1.281+0	2.311–1
	3d <sub>3/2</sub>	2.679–4	2.523–1	8.258–1	5.165–1
	3d <sub>5/2</sub>	3.838–4	2.672–1	8.444–1	5.224–1
	4s <sub>1/2</sub>	5.713–3	1.979+0	1.687+0	4.063–5
	2s <sub>1/2</sub>	7.224–1	1.978+0	1.689+0	4.479–5
	2p <sub>1/2</sub>	1.241–1	6.532–1	1.360+0	2.278–1
	2p <sub>3/2</sub>	2.299–1	6.381–1	1.347+0	2.328–1
	3s <sub>1/2</sub>	1.226–1	1.980+0	1.648+0	3.809–5
26	3p <sub>1/2</sub>	2.002–2	6.459–1	1.319+0	2.183–1
	3p <sub>3/2</sub>	3.700–2	6.303–1	1.306+0	2.229–1
	3d <sub>3/2</sub>	4.603–4	2.628–1	8.503–1	5.076–1
	3d <sub>5/2</sub>	6.595–4	2.770–1	8.682–1	5.139–1
	4s <sub>1/2</sub>	8.580–3	1.980+0	1.644+0	3.649–5
	2s <sub>1/2</sub>	8.125–1	1.979+0	1.649+0	4.044–5
	2p <sub>1/2</sub>	1.515–1	6.861–1	1.386+0	2.210–1
	2p <sub>3/2</sub>	2.798–1	6.725–1	1.376+0	2.258–1
27	3s <sub>1/2</sub>	1.410–1	1.981+0	1.605+0	3.378–5
	3p <sub>1/2</sub>	2.512–2	6.790–1	1.342+0	2.106–1
	3p <sub>3/2</sub>	4.624–2	6.649–1	1.331+0	2.148–1
	3d <sub>3/2</sub>	6.707–4	2.737–1	8.789–1	4.991–1
	3d <sub>5/2</sub>	9.587–4	2.870–1	8.959–1	5.057–1
	4s <sub>1/2</sub>	9.570–3	1.981+0	1.600+0	3.270–5
	2s <sub>1/2</sub>	9.067–1	1.980+0	1.608+0	3.542–5
	2p <sub>1/2</sub>	1.829–1	7.181–1	1.411+0	2.145–1
28	2p <sub>3/2</sub>	3.367–1	7.062–1	1.403+0	2.189–1
	3s <sub>1/2</sub>	1.609–1	1.982+0	1.560+0	2.895–5
	3p <sub>1/2</sub>	3.111–2	7.115–1	1.364+0	2.030–1
	3p <sub>3/2</sub>	5.704–2	6.990–1	1.355+0	2.069–1
	3d <sub>3/2</sub>	9.541–4	2.857–1	9.103–1	4.908–1
	3d <sub>5/2</sub>	1.360–3	2.980–1	9.265–1	4.976–1
	4s <sub>1/2</sub>	1.059–2	1.983+0	1.555+0	2.807–5
	2s <sub>1/2</sub>	1.005+0	1.981+0	1.567+0	2.966–5
29	2p <sub>1/2</sub>	2.185–1	7.493–1	1.434+0	2.081–1
	2p <sub>3/2</sub>	4.009–1	7.392–1	1.430+0	2.122–1
	3s <sub>1/2</sub>	1.821–1	1.983+0	1.515+0	2.351–5
	3p <sub>1/2</sub>	3.808–2	7.433–1	1.383+0	1.955–1
	3p <sub>3/2</sub>	6.956–2	7.327–1	1.378+0	1.991–1
	3d <sub>3/2</sub>	1.329–3	2.991–1	9.440–1	4.823–1
	3d <sub>5/2</sub>	1.891–3	3.104–1	9.593–1	4.895–1
	4s <sub>1/2</sub>	1.163–2	1.984+0	1.509+0	2.211–5
30	2s <sub>1/2</sub>	1.108+0	1.982+0	1.525+0	2.285–5
	2p <sub>1/2</sub>	2.591–1	7.800–1	1.458+0	2.020–1
	2p <sub>3/2</sub>	4.738–1	7.718–1	1.456+0	2.058–1
	3s <sub>1/2</sub>	2.029–1	1.984+0	1.469+0	1.727–5
	3p <sub>1/2</sub>	4.555–2	7.750–1	1.402+0	1.882–1
	3p <sub>3/2</sub>	8.280–2	7.663–1	1.400+0	1.915–1
	3d <sub>3/2</sub>	1.680–3	3.144–1	9.793–1	4.737–1
	3d <sub>5/2</sub>	2.378–3	3.246–1	9.934–1	4.812–1
31	4s <sub>1/2</sub>	9.584–3	1.985+0	1.462+0	1.646–5
	2s <sub>1/2</sub>	1.210+0	1.983+0	1.483+0	1.550–5
	2p <sub>1/2</sub>	3.030–1	8.090–1	1.479+0	1.962–1
	2p <sub>3/2</sub>	5.524–1	8.029–1	1.480+0	1.996–1
	3s <sub>1/2</sub>	2.286–1	1.986+0	1.422+0	1.064–5
	3p <sub>1/2</sub>	5.535–2	8.051–1	1.418+0	1.812–1
	3p <sub>3/2</sub>	1.003–1	7.984–1	1.418+0	1.841–1
	3d <sub>3/2</sub>	2.449–3	3.301–1	1.013+0	
32	3d <sub>5/2</sub>	3.466–3	3.392–1	1.026+0	4.728–1
	4s <sub>1/2</sub>	1.379–2	1.986+0	1.415+0	9.382–6
	2s <sub>1/2</sub>	1.314+0	1.984+0	1.441+0	7.189–6
	2p <sub>1/2</sub>	3.511–1	8.370–1	1.498+0	1.906–1
	2p <sub>3/2</sub>	6.380–1	8.330–1	1.503+0	1.936–1
	3s <sub>1/2</sub>	2.563–1	1.987+0	1.376+0	3.279–6

Table 2 (continued)

Z	Shell	$\sigma$	$\beta$	$\gamma$	$\delta$
32	3p <sub>1/2</sub>	6.674–2	8.343–1	1.431+0	1.744–1
	3p <sub>3/2</sub>	1.205–1	8.297–1	1.435+0	1.770–1
	3d <sub>3/2</sub>	3.477–3	3.466–1	1.045+0	4.563–1
	3d <sub>5/2</sub>	4.918–3	3.545–1	1.057+0	4.646–1
	4s <sub>1/2</sub>	2.027–2	1.987+0	1.367+0	2.372–6
	4p <sub>1/2</sub>	2.379–3	8.352–1	1.427+0	1.728–1
	2s <sub>1/2</sub>	1.419+0	1.985+0	1.399+0	–2.252–6
	2p <sub>1/2</sub>	4.034–1	8.640–1	1.517+0	1.852–1
33	2p <sub>3/2</sub>	7.308–1	8.622–1	1.525+0	1.879–1
	3s <sub>1/2</sub>	2.863–1	1.988+0	1.330+0	–4.911–6
	3p <sub>1/2</sub>	7.991–2	8.627–1	1.443+0	1.679–1
	3p <sub>3/2</sub>	1.439–1	8.603–1	1.450+0	1.701–1
	3d <sub>3/2</sub>	4.815–3	3.636–1	1.076+0	4.478–1
	3d <sub>5/2</sub>	6.804–3	3.702–1	1.087+0	4.565–1
	4s <sub>1/2</sub>	2.645–2	1.988+0	1.320+0	–5.157–6
	4p <sub>1/2</sub>	4.083–3	8.636–1	1.437+0	1.660–1
34	2s <sub>1/2</sub>	1.524+0	1.986+0	1.356+0	–1.295–5
	2p <sub>1/2</sub>	4.601–1	8.903–1	1.533+0	1.802–1
	2p <sub>3/2</sub>	8.308–1	8.908–1	1.545+0	1.825–1
	3s <sub>1/2</sub>	3.183–1	1.989+0	1.283+0	–1.401–5
	3p <sub>1/2</sub>	9.497–2	8.905–1	1.453+0	1.616–1
	3p <sub>3/2</sub>	1.706–1	8.904–1	1.463+0	1.635–1
	3d <sub>3/2</sub>	6.528–3	3.810–1	1.106+0	4.392–1
	3d <sub>5/2</sub>	9.215–3	3.863–1	1.115+0	4.484–1
35	4s <sub>1/2</sub>	3.306–2	1.989+0	1.272+0	–1.445–5
	4p <sub>1/2</sub>	6.107–3	8.914–1	1.446+0	1.594–1
	4p <sub>3/2</sub>	1.077–2	8.913–1	1.456+0	1.612–1
	2s <sub>1/2</sub>	1.629+0	1.987+0	1.314+0	–2.498–5
	2p <sub>1/2</sub>	5.209–1	9.154–1	1.549+0	1.753–1
	2p <sub>3/2</sub>	9.384–1	9.184–1	1.564+0	1.772–1
	3s <sub>1/2</sub>	3.523–1	1.990+0	1.236+0	–2.407–5
	3p <sub>1/2</sub>	1.120–1	9.173–1	1.461+0	1.555–1
36	3p <sub>3/2</sub>	2.006–1	9.195–1	1.474+0	1.571–1
	3d <sub>3/2</sub>	8.687–3	3.985–1	1.134+0	4.308–1
	3d <sub>5/2</sub>	1.225–2	4.023–1	1.142+0	4.405–1
	4s <sub>1/2</sub>	4.018–2	1.990+0	1.225+0	–2.412–5
	4p <sub>1/2</sub>	8.479–3	9.184–1	1.452+0	1.530–1
	4p <sub>3/2</sub>	1.493–2	9.206–1	1.465+0	1.545–1
	2s <sub>1/2</sub>	1.734+0	1.987+0	1.271+0	–3.849–5
	2p <sub>1/2</sub>	5.860–1	9.397–1	1.563+0	1.706–1
37	2p <sub>3/2</sub>	1.052+0	9.452–1	1.582+0	1.723–1
	3s <sub>1/2</sub>	3.883–1	1.991+0	1.190+0	–3.521–5
	3p <sub>1/2</sub>	1.312–1	9.435–1	1.468+0	1.496–1
	3p <sub>3/2</sub>	2.342–1	9.482–1	1.484+0	1.509–1
	3d <sub>3/2</sub>	1.137–2	4.160–1	1.161+0	4.225–1
	3d <sub>5/2</sub>	1.601–2	4.182–1	1.167+0	4.327–1
	4s <sub>1/2</sub>	4.786–2	1.991+0	1.177+0	–3.478–5
	4p <sub>1/2</sub>	1.126–2	9.447–1	1.457+0	1.469–1
38	4p <sub>3/2</sub>	1.977–2	9.495–1	1.473+0	1.481–1
	2s <sub>1/2</sub>	1.837+0	1.988+0	1.229+0	–5.361–5
	2p <sub>1/2</sub>	6.550–1	9.630–1	1.576+0	1.662–1
	2p <sub>3/2</sub>	1.172+0	9.710–1	1.599+0	1.674–1
	3s <sub>1/2</sub>	4.261–1	1.992+0	1.143+0	–4.750–5
	3p <sub>1/2</sub>	1.525–1	9.687–1	1.472+0	1.440–1
	3p <sub>3/2</sub>	2.716–1	9.760–1	1.492+0	1.449–1
	3d <sub>3/2</sub>	1.466–2	4.334–1	1.186+0	4.144–1
39	3d <sub>5/2</sub>	2.061–2	4.340–1	1.190+0	4.250–1
	4s <sub>1/2</sub>	5.612–2	1.992+0	1.129+0	–4.638–5
	4p <sub>1/2</sub>	1.448–2	9.703–1	1.460+0	1.409–1
	4p <sub>3/2</sub>	2.535–2	9.776–1	1.480+0	1.418–1
	2p <sub>1/2</sub>	7.269–1	9.851–1	1.586+0	1.620–1
	2p <sub>3/2</sub>	1.297+0	9.958–1	1.613+0	1.629–1

Table 2 (continued)

Z	Shell	$\sigma$	$\beta$	$\gamma$	$\delta$
38	3s <sub>1/2</sub>	4.653–1	1.992+0	1.098+0	–6.093–5
	3p <sub>1/2</sub>	1.759–1	9.929–1	1.475+0	1.385–1
	3p <sub>3/2</sub>	3.124–1	1.003+0	1.499+0	1.392–1
	3d <sub>3/2</sub>	1.863–2	4.507–1	1.210+0	4.065–1
	3d <sub>5/2</sub>	2.615–2	4.494–1	1.212+0	4.176–1
	4s <sub>1/2</sub>	6.748–2	1.993+0	1.082+0	–5.894–5
	4p <sub>1/2</sub>	1.994–2	9.947–1	1.460+0	1.351–1
	4p <sub>3/2</sub>	3.511–2	1.005+0	1.484+0	1.357–1
	5s <sub>1/2</sub>	3.805–3	1.993+0	1.081+0	–5.872–5
	2p <sub>3/2</sub>	1.427+0	1.020+0	1.627+0	1.586–1
39	3s <sub>1/2</sub>	5.061–1	1.993+0	1.052+0	–7.573–5
	3p <sub>1/2</sub>	2.017–1	1.016+0	1.477+0	1.333–1
	3p <sub>3/2</sub>	3.571–1	1.029+0	1.504+0	1.338–1
	3d <sub>3/2</sub>	2.339–2	4.678–1	1.233+0	3.986–1
	3d <sub>5/2</sub>	3.278–2	4.647–1	1.233+0	4.103–1
	4s <sub>1/2</sub>	7.995–2	1.994+0	1.036+0	–7.312–5
	4p <sub>1/2</sub>	2.602–2	1.019+0	1.460+0	1.296–1
	4p <sub>3/2</sub>	4.583–2	1.031+0	1.487+0	1.300–1
	5s <sub>1/2</sub>	6.959–3	1.994+0	1.034+0	–7.325–5
	3s <sub>1/2</sub>	5.486–1	1.994+0	1.007+0	–9.209–5
40	3p <sub>1/2</sub>	2.299–1	1.039+0	1.477+0	1.283–1
	3p <sub>3/2</sub>	4.061–1	1.054+0	1.508+0	1.284–1
	3d <sub>3/2</sub>	2.907–2	4.849–1	1.256+0	3.910–1
	3d <sub>5/2</sub>	4.066–2	4.798–1	1.254+0	4.033–1
	4s <sub>1/2</sub>	9.209–2	1.995+0	9.899–1	–8.877–5
	4p <sub>1/2</sub>	3.219–2	1.042+0	1.459+0	1.242–1
	4p <sub>3/2</sub>	5.656–2	1.057+0	1.489+0	1.244–1
	4d <sub>3/2</sub>	1.826–3	4.835–1	1.249+0	3.869–1
	5s <sub>1/2</sub>	8.623–3	1.995+0	9.879–1	–8.896–5
	3s <sub>1/2</sub>	5.928–1	1.995+0	9.619–1	–1.100–4
41	3p <sub>1/2</sub>	2.608–1	1.061+0	1.476+0	1.234–1
	3p <sub>3/2</sub>	4.594–1	1.079+0	1.510+0	1.233–1
	3d <sub>3/2</sub>	3.575–2	5.020–1	1.277+0	3.834–1
	3d <sub>5/2</sub>	4.994–2	4.949–1	1.274+0	3.963–1
	4s <sub>1/2</sub>	1.046–1	1.995+0	9.441–1	–1.059–4
	4p <sub>1/2</sub>	3.897–2	1.064+0	1.455+0	1.190–1
	4p <sub>3/2</sub>	6.827–2	1.082+0	1.489+0	1.189–1
	4d <sub>3/2</sub>	2.701–3	5.006–1	1.269+0	3.787–1
	5s <sub>1/2</sub>	9.996–3	1.996+0	9.418–1	–1.055–4
	3s <sub>1/2</sub>	6.387–1	1.996+0	9.169–1	–1.298–4
42	3p <sub>1/2</sub>	2.943–1	1.082+0	1.473+0	1.186–1
	3p <sub>3/2</sub>	5.173–1	1.103+0	1.511+0	1.183–1
	3d <sub>3/2</sub>	4.361–2	5.191–1	1.299+0	3.760–1
	3d <sub>5/2</sub>	6.081–2	5.098–1	1.293+0	3.895–1
	4s <sub>1/2</sub>	1.166–1	1.996+0	8.982–1	–1.243–4
	4p <sub>1/2</sub>	4.570–2	1.086+0	1.451+0	1.139–1
	4p <sub>3/2</sub>	7.968–2	1.107+0	1.488+0	1.136–1
	4d <sub>3/2</sub>	3.351–3	5.178–1	1.289+0	3.706–1
	5s <sub>1/2</sub>	9.175–3	1.996+0	8.955–1	–1.247–4
	3s <sub>1/2</sub>	6.857–1	1.996+0	8.723–1	–1.514–4
43	3p <sub>1/2</sub>	3.304–1	1.103+0	1.469+0	1.140–1
	3p <sub>3/2</sub>	5.792–1	1.127+0	1.511+0	1.135–1
	3d <sub>3/2</sub>	5.269–2	5.362–1	1.319+0	3.686–1
	3d <sub>5/2</sub>	7.334–2	5.247–1	1.311+0	3.827–1
	4s <sub>1/2</sub>	1.301–1	1.997+0	8.527–1	–1.448–4
	4p <sub>1/2</sub>	5.383–2	1.107+0	1.445+0	1.089–1
	4p <sub>3/2</sub>	9.357–2	1.131+0	1.485+0	1.085–1
	4d <sub>3/2</sub>	4.581–3	5.350–1	1.309+0	3.625–1
	4d <sub>5/2</sub>	6.293–3	5.229–1	1.301+0	3.765–1
	5s <sub>1/2</sub>	1.006–2	1.997+0	8.496–1	–1.430–4

Table 2 (continued)

Z	Shell	$\sigma$	$\beta$	$\gamma$	$\delta$
44	3d <sub>3/2</sub>	6.308–2	5.532–1	1.339+0	3.615–1
	3d <sub>5/2</sub>	8.767–2	5.394–1	1.329+0	3.761–1
	4s <sub>1/2</sub>	1.453–1	1.997+0	8.079–1	–1.668–4
	4p <sub>1/2</sub>	6.361–2	1.127+0	1.437+0	1.041–1
	4p <sub>3/2</sub>	1.104–1	1.154+0	1.481+0	1.036–1
	4d <sub>3/2</sub>	6.626–3	5.521–1	1.327+0	3.545–1
	4d <sub>5/2</sub>	9.123–3	5.376–1	1.317+0	3.691–1
	5s <sub>1/2</sub>	1.343–2	1.998+0	8.047–1	–1.651–4
	3s <sub>1/2</sub>	7.834–1	1.997+0	7.844–1	–2.009–4
	3p <sub>1/2</sub>	4.106–1	1.142+0	1.456+0	1.052–1
45	3p <sub>3/2</sub>	7.163–1	1.172+0	1.505+0	1.044–1
	3d <sub>3/2</sub>	7.511–2	5.706–1	1.359+0	3.544–1
	3d <sub>5/2</sub>	1.042–1	5.543–1	1.346+0	3.697–1
	4s <sub>1/2</sub>	1.586–1	1.998+0	7.631–1	–1.911–4
	4p <sub>1/2</sub>	7.247–2	1.147+0	1.428+0	9.943–2
	4p <sub>3/2</sub>	1.251–1	1.177+0	1.475+0	9.873–2
	4d <sub>3/2</sub>	7.852–3	5.697–1	1.346+0	3.467–1
	4d <sub>5/2</sub>	1.075–2	5.526–1	1.333+0	3.619–1
	5s <sub>1/2</sub>	1.164–2	1.998+0	7.595–1	–1.904–4
	3s <sub>1/2</sub>	8.339–1	1.998+0	7.410–1	–2.291–4
46	3p <sub>1/2</sub>	4.547–1	1.161+0	1.448+0	1.010–1
	3p <sub>3/2</sub>	7.915–1	1.194+0	1.500+0	1.001–1
	3d <sub>3/2</sub>	8.873–2	5.877–1	1.377+0	3.474–1
	3d <sub>5/2</sub>	1.229–1	5.689–1	1.363+0	3.634–1
	4s <sub>1/2</sub>	1.737–1	1.998+0	7.190–1	–2.175–4
	4p <sub>1/2</sub>	8.303–2	1.167+0	1.417+0	9.492–2
	4p <sub>3/2</sub>	1.429–1	1.200+0	1.468+0	9.413–2
	4d <sub>3/2</sub>	9.970–3	5.872–1	1.363+0	3.389–1
	4d <sub>5/2</sub>	1.361–2	5.676–1	1.348+0	3.548–1
	5s <sub>1/2</sub>	1.237–2	1.998+0	7.152–1	–2.168–4
47	3s <sub>1/2</sub>	8.857–1	1.998+0	6.980–1	–2.600–4
	3p <sub>1/2</sub>	5.020–1	1.179+0	1.439+0	9.698–2
	3p <sub>3/2</sub>	8.718–1	1.215+0	1.494+0	9.591–2
	3d <sub>3/2</sub>	1.043–1	6.050–1	1.396+0	3.406–1
	3d <sub>5/2</sub>	1.442–1	5.836–1	1.379+0	3.572–1
	4s <sub>1/2</sub>	1.885–1	1.999+0	6.754–1	–2.462–4
	4p <sub>1/2</sub>	9.371–2	1.185+0	1.405+0	9.055–2
	4p <sub>3/2</sub>	1.605–1	1.222+0	1.459+0	8.969–2
	4d <sub>3/2</sub>	1.159–2	6.050–1	1.379+0	3.313–1
	4d <sub>5/2</sub>	1.570–2	5.827–1	1.362+0	3.477–1
48	3s <sub>1/2</sub>	9.373–1	1.998+0	6.561–1	–2.935–4
	3p <sub>1/2</sub>	5.510–1	1.196+0	1.428+0	9.311–2
	3p <sub>3/2</sub>	9.548–1	1.236+0	1.487+0	9.197–2
	3d <sub>3/2</sub>	1.215–1	6.221–1	1.413+0	3.339–1
	3d <sub>5/2</sub>	1.677–1	5.981–1	1.394+0	3.512–1
	4s <sub>1/2</sub>	2.054–1	1.999+0	6.332–1	–2.772–4
	4p <sub>1/2</sub>	1.068–1	1.204+0	1.391+0	8.637–2
	4p <sub>3/2</sub>	1.825–1	1.243+0	1.449+0	8.548–2
	4d <sub>3/2</sub>	1.538–2	6.226–1	1.394+0	3.238–1
	4d <sub>5/2</sub>	2.090–2	5.975–1	1.375+0	3.408–1
49	5s <sub>1/2</sub>	1.372–2	1.999+0	6.289–1	–2.737–4
	3s <sub>1/2</sub>	9.893–1	1.999+0	6.151–1	–3.299–4
	3p <sub>1/2</sub>	6.023–1	1.212+0	1.416+0	8.941–2
	3p <sub>3/2</sub>	1.042+0	1.255+0	1.479+0	8.822–2
	3d <sub>3/2</sub>	1.406–1	6.392–1	1.430+0	3.274–1
	3d <sub>5/2</sub>	1.938–1	6.124–1	1.409+0	3.454–1
	4s <sub>1/2</sub>	2.235–1	1.999+0	5.922–1	–3.108–4
	4p <sub>1/2</sub>	1.213–1	1.221+0	1.377+0	8.237–2
	4p <sub>3/2</sub>	2.069–1	1.264+0	1.438+0	8.148–2
	4d <sub>3/2</sub>	1.984–2	6.400–1	1.408+0	3.163–1
50	4d <sub>5/2</sub>	2.700–2	6.122–1	1.386+0	3.340–1
	5s <sub>1/2</sub>	1.819–2	1.999+0	5.878–1	–3.079–4
	(continued on next page)				

Table 2 (continued)

Z	Shell	$\sigma$	$\beta$	$\gamma$	$\delta$
49	$3s_{1/2}$	1.041+0	1.999+0	5.751–1	–3.694–4
	$3p_{3/2}$	1.132+0	1.275+0	1.470+0	8.467–2
	$3d_{3/2}$	1.618–1	6.561–1	1.446+0	3.211–1
	$3p_{1/2}$	6.557–1	1.229+0	1.404+0	8.587–2
	$3d_{5/2}$	2.226–1	6.266–1	1.422+0	3.397–1
	$4s_{1/2}$	2.423–1	1.999+0	5.524–1	–3.471–4
	$4p_{1/2}$	1.370–1	1.238+0	1.362+0	7.855–2
	$4p_{3/2}$	2.335–1	1.284+0	1.426+0	7.768–2
	$4d_{3/2}$	2.519–2	6.575–1	1.420+0	3.092–1
	$4d_{5/2}$	3.428–2	6.268–1	1.397+0	3.275–1
	$5s_{1/2}$	2.459–2	1.999+0	5.478–1	–3.440–4
	$5p_{1/2}$	6.957–3	1.240+0	1.356+0	7.742–2
50	$3s_{1/2}$	1.094+0	1.999+0	5.361–1	–4.123–4
	$3p_{1/2}$	7.114–1	1.244+0	1.390+0	8.248–2
	$3p_{3/2}$	1.225+0	1.293+0	1.460+0	8.129–2
	$3d_{3/2}$	1.852–1	6.730–1	1.461+0	3.150–1
	$3d_{5/2}$	2.543–1	6.407–1	1.435+0	3.343–1
	$4s_{1/2}$	2.621–1	1.999+0	5.136–1	–3.862–4
	$4p_{1/2}$	1.542–1	1.254+0	1.345+0	7.485–2
	$4p_{3/2}$	2.624–1	1.303+0	1.413+0	7.406–2
	$4d_{3/2}$	3.138–2	6.750–1	1.433+0	3.021–1
	$4d_{5/2}$	4.271–2	6.413–1	1.407+0	3.211–1
	$5s_{1/2}$	3.024–2	2.000+0	5.087–1	–3.818–4
	$5p_{1/2}$	1.054–2	1.257+0	1.340+0	7.363–2
51	$3s_{1/2}$	1.146+0	1.999+0	4.981–1	–4.588–4
	$3p_{1/2}$	7.693–1	1.259+0	1.375+0	7.921–2
	$3p_{3/2}$	1.322+0	1.312+0	1.448+0	7.808–2
	$3d_{3/2}$	2.109–1	6.898–1	1.475+0	3.090–1
	$3d_{5/2}$	2.891–1	6.546–1	1.447+0	3.290–1
	$4s_{1/2}$	2.828–1	1.999+0	4.758–1	–4.288–4
	$4p_{1/2}$	1.728–1	1.270+0	1.328+0	7.128–2
	$4p_{3/2}$	2.936–1	1.323+0	1.399+0	7.059–2
	$4d_{3/2}$	3.854–2	6.925–1	1.444+0	2.952–1
	$4d_{5/2}$	5.241–2	6.557–1	1.416+0	3.149–1
	$5s_{1/2}$	3.607–2	1.999+0	4.708–1	–4.223–4
	$5p_{1/2}$	1.443–2	1.273+0	1.322+0	6.996–2
52	$3s_{1/2}$	1.198+0	1.998+0	4.610–1	–5.090–4
	$3p_{1/2}$	8.292–1	1.273+0	1.360+0	7.608–2
	$3p_{3/2}$	1.423+0	1.329+0	1.436+0	7.504–2
	$3d_{3/2}$	2.390–1	7.065–1	1.489+0	3.032–1
	$3d_{5/2}$	3.271–1	6.684–1	1.458+0	3.238–1
	$4s_{1/2}$	3.043–1	1.999+0	4.389–1	–4.747–4
	$4p_{1/2}$	1.927–1	1.286+0	1.310+0	6.783–2
	$4p_{3/2}$	3.271–1	1.341+0	1.384+0	6.729–2
	$4d_{3/2}$	4.673–2	7.099–1	1.455+0	2.885–1
	$4d_{5/2}$	6.350–2	6.700–1	1.425+0	3.087–1
	$5s_{1/2}$	4.208–2	1.999+0	4.338–1	–4.671–4
	$5p_{1/2}$	1.855–2	1.288+0	1.303+0	6.639–2
53	$3s_{1/2}$	1.250+0	1.998+0	4.250–1	–5.635–4
	$3p_{1/2}$	8.911–1	1.287+0	1.344+0	7.307–2
	$3p_{3/2}$	1.527+0	1.346+0	1.423+0	7.215–2
	$3d_{3/2}$	2.695–1	7.230–1	1.501+0	2.975–1
	$3d_{5/2}$	3.683–1	6.820–1	1.469+0	3.187–1
	$4s_{1/2}$	3.266–1	1.999+0	4.031–1	–5.243–4
	$4p_{1/2}$	2.140–1	1.301+0	1.292+0	6.449–2
	$4p_{3/2}$	3.628–1	1.359+0	1.369+0	6.414–2
	$4d_{3/2}$	5.604–2	7.272–1	1.465+0	2.818–1
	$4d_{5/2}$	7.607–2	6.841–1	1.434+0	3.027–1
	$5s_{1/2}$	4.835–2	1.999+0	3.977–1	–5.153–4
	$5p_{1/2}$	2.299–2	1.304+0	1.284+0	6.294–2
	$5p_{3/2}$	3.712–2	1.362+0	1.361+0	6.268–2

Table 2 (continued)

Z	Shell	$\sigma$	$\beta$	$\gamma$	$\delta$
54	$3s_{1/2}$	1.302+0	1.998+0	3.900–1	–6.225–4
	$3p_{1/2}$	9.548–1	1.301+0	1.327+0	7.016–2
	$3p_{3/2}$	1.633+0	1.363+0	1.409+0	6.941–2
	$3d_{3/2}$	3.027–1	7.396–1	1.513+0	2.919–1
	$3d_{5/2}$	4.129–1	6.954–1	1.479+0	3.138–1
	$4s_{1/2}$	3.495–1	1.999+0	3.681–1	–5.777–4
	$4p_{1/2}$	2.367–1	1.315+0	1.273+0	6.125–2
	$4p_{3/2}$	4.007–1	1.377+0	1.353+0	6.112–2
	$4d_{3/2}$	6.656–2	7.446–1	1.476+0	2.752–1
	$4d_{5/2}$	9.024–2	6.982–1	1.442+0	2.968–1
	$5s_{1/2}$	5.488–2	1.999+0	3.626–1	–5.673–4
	$5p_{1/2}$	2.779–2	1.319+0	1.264+0	5.959–2
55	$5p_{3/2}$	4.489–2	1.380+0	1.343+0	5.957–2
	$3s_{1/2}$	1.353+0	1.998+0	3.563–1	–6.860–4
	$3p_{1/2}$	1.019+0	1.313+0	1.310+0	6.740–2
	$3p_{3/2}$	1.741+0	1.379+0	1.395+0	6.684–2
	$3d_{3/2}$	3.381–1	7.557–1	1.524+0	2.864–1
	$3d_{5/2}$	4.603–1	7.084–1	1.487+0	3.091–1
	$4s_{1/2}$	3.731–1	1.998+0	3.345–1	–6.352–4
	$4p_{1/2}$	2.606–1	1.329+0	1.253+0	5.814–2
	$4p_{3/2}$	4.406–1	1.394+0	1.336+0	5.828–2
	$4d_{3/2}$	7.835–2	7.616–1	1.485+0	2.687–1
	$4d_{5/2}$	1.061–1	7.118–1	1.449+0	2.909–1
	$5s_{1/2}$	6.393–2	1.998+0	3.286–1	–6.240–4
56	$5p_{1/2}$	3.577–2	1.333+0	1.243+0	5.637–2
	$5p_{3/2}$	5.880–2	1.398+0	1.325+0	5.662–2
	$6s_{1/2}$	4.155–3	1.998+0	3.273–1	–6.217–4
	$3s_{1/2}$	1.404+0	1.997+0	3.235–1	–7.547–4
	$3p_{1/2}$	1.085+0	1.326+0	1.292+0	6.473–2
	$3p_{3/2}$	1.851+0	1.395+0	1.380+0	6.441–2
	$3d_{3/2}$	3.760–1	7.718–1	1.534+0	2.812–1
	$3d_{5/2}$	5.110–1	7.214–1	1.496+0	3.044–1
	$4s_{1/2}$	3.973–1	1.998+0	3.016–1	–6.972–4
	$4p_{1/2}$	2.859–1	1.343+0	1.232+0	5.514–2
	$4p_{3/2}$	4.829–1	1.411+0	1.318+0	5.556–2
	$4d_{3/2}$	9.157–2	7.788–1	1.493+0	2.624–1
57	$4d_{5/2}$	1.238–1	7.255–1	1.456+0	2.853–1
	$5s_{1/2}$	7.352–2	1.998+0	2.959–1	–6.845–4
	$5p_{1/2}$	4.401–2	1.347+0	1.222+0	5.324–2
	$5p_{3/2}$	7.278–2	1.415+0	1.306+0	5.379–2
	$6s_{1/2}$	7.245–3	1.998+0	2.945–1	–6.842–4
	$3s_{1/2}$	1.455+0	1.996+0	2.913–1	–8.287–4
	$3p_{1/2}$	1.154+0	1.338+0	1.273+0	6.213–2
	$3p_{3/2}$	1.965+0	1.410+0	1.364+0	6.207–2
	$3d_{3/2}$	4.170–1	7.879–1	1.544+0	2.760–1
	$3d_{5/2}$	5.658–1	7.343–1	1.503+0	2.999–1
	$4s_{1/2}$	4.224–1	1.997+0	2.695–1	–7.639–4
	$4p_{1/2}$	3.127–1	1.356+0	1.211+0	5.219–2
58	$4p_{3/2}$	5.279–1	1.428+0	1.299+0	5.295–2
	$4d_{3/2}$	1.064–1	7.961–1	1.501+0	2.561–1
	$4d_{5/2}$	1.437–1	7.393–1	1.462+0	2.796–1
	$5s_{1/2}$	8.253–2	1.997+0	2.638–1	–7.488–4
	$5p_{1/2}$	5.172–2	1.360+0	1.200+0	5.019–2
	$5p_{3/2}$	8.553–2	1.432+0	1.287+0	5.109–2
	$5d_{3/2}$	8.863–3	7.979–1	1.498+0	2.534–1
	$6s_{1/2}$	8.759–3	1.997+0	2.624–1	–7.465–4
	$3s_{1/2}$	1.510+0	1.996+0	2.587–1	–9.094–4
	$3p_{1/2}$	1.228+0	1.350+0	1.253+0	5.948–2
	$3p_{3/2}$	2.090+0	1.426+0	1.347+0	5.973–2
	$3d_{3/2}$	4.643–1	8.046–1	1.554+0	2.708–1
59	$3d_{5/2}$	6.289–1	7.477–1	1.512+0	2.954–1
	$4s_{1/2}$	4.429–1	1.996+0	2.369–1	–8.363–4
	$4p_{1/2}$	3.360–1	1.370+0	1.188+0	4.923–2

Table 2 (continued)

Z	Shell	$\sigma$	$\beta$	$\gamma$	$\delta$
59	4p <sub>3/2</sub>	5.653–1	1.444+0	1.279+0	5.037–2
	4d <sub>3/2</sub>	1.189–1	8.140–1	1.509+0	2.499–1
	4d <sub>5/2</sub>	1.602–1	7.537–1	1.468+0	2.740–1
	4f <sub>5/2</sub>	2.051–3	4.420–1	1.206+0	5.099–1
	5s <sub>1/2</sub>	8.205–2	1.996+0	2.311–1	–8.200–4
	5p <sub>1/2</sub>	5.154–2	1.374+0	1.176+0	4.718–2
	5p <sub>3/2</sub>	8.448–2	1.448+0	1.266+0	4.849–2
	6s <sub>1/2</sub>	7.735–3	1.996+0	2.296–1	–8.167–4
	3s <sub>1/2</sub>	1.562+0	1.995+0	2.276–1	–9.959–4
	3p <sub>1/2</sub>	1.302+0	1.362+0	1.232+0	5.696–2
	3p <sub>3/2</sub>	2.214+0	1.441+0	1.329+0	5.758–2
	3d <sub>3/2</sub>	5.137–1	8.209–1	1.563+0	2.657–1
	3d <sub>5/2</sub>	6.947–1	7.607–1	1.519+0	2.909–1
60	4s <sub>1/2</sub>	4.660–1	1.995+0	2.058–1	–9.135–4
	4p <sub>1/2</sub>	3.626–1	1.383+0	1.165+0	4.640–2
	4p <sub>3/2</sub>	6.086–1	1.460+0	1.258+0	4.796–2
	4d <sub>3/2</sub>	1.344–1	8.317–1	1.516+0	2.438–1
	4d <sub>5/2</sub>	1.806–1	7.677–1	1.473+0	2.684–1
	4f <sub>5/2</sub>	2.614–3	4.496–1	1.224+0	5.042–1
	5s <sub>1/2</sub>	8.612–2	1.995+0	2.001–1	–8.950–4
	5p <sub>1/2</sub>	5.528–2	1.387+0	1.152+0	4.431–2
	5p <sub>3/2</sub>	9.020–2	1.465+0	1.244+0	4.605–2
	6s <sub>1/2</sub>	7.941–3	1.995+0	1.985–1	–8.913–4
61	3s <sub>1/2</sub>	1.615+0	1.994+0	1.973–1	–1.089–3
	3p <sub>1/2</sub>	1.378+0	1.373+0	1.211+0	5.450–2
	3p <sub>3/2</sub>	2.342+0	1.456+0	1.310+0	5.553–2
	3d <sub>3/2</sub>	5.665–1	8.371–1	1.571+0	2.607–1
	3d <sub>5/2</sub>	7.649–1	7.735–1	1.525+0	2.865–1
	4s <sub>1/2</sub>	4.895–1	1.994+0	1.757–1	–9.961–4
	4p <sub>1/2</sub>	3.901–1	1.395+0	1.140+0	4.367–2
	4p <sub>3/2</sub>	6.534–1	1.476+0	1.235+0	4.569–2
	4d <sub>3/2</sub>	1.512–1	8.494–1	1.521+0	2.378–1
	4d <sub>5/2</sub>	2.028–1	7.817–1	1.477+0	2.629–1
	4f <sub>5/2</sub>	3.279–3	4.576–1	1.241+0	4.985–1
	5s <sub>1/2</sub>	9.013–2	1.994+0	1.701–1	–9.744–4
	5p <sub>1/2</sub>	5.906–2	1.400+0	1.127+0	4.153–2
	5p <sub>3/2</sub>	9.592–2	1.481+0	1.221+0	4.375–2
62	6s <sub>1/2</sub>	8.136–3	1.994+0	1.686–1	–9.706–4
63	3s <sub>1/2</sub>	1.667+0	1.992+0	1.680–1	–1.189–3
	3p <sub>1/2</sub>	1.456+0	1.384+0	1.189+0	5.213–2
	3p <sub>3/2</sub>	2.472+0	1.470+0	1.290+0	5.360–2
	3d <sub>3/2</sub>	6.230–1	8.532–1	1.578+0	2.559–1
	3d <sub>5/2</sub>	8.398–1	7.862–1	1.531+0	2.822–1
	4s <sub>1/2</sub>	5.132–1	1.993+0	1.466–1	–1.085–3
	4p <sub>1/2</sub>	4.186–1	1.407+0	1.115+0	4.104–2
	4p <sub>3/2</sub>	6.997–1	1.491+0	1.212+0	4.355–2
	4d <sub>3/2</sub>	1.694–1	8.670–1	1.525+0	2.318–1
	4d <sub>5/2</sub>	2.267–1	7.956–1	1.479+0	2.575–1
	4f <sub>5/2</sub>	4.061–3	4.660–1	1.258+0	4.929–1
	5s <sub>1/2</sub>	9.411–2	1.993+0	1.412–1	–1.061–3
	5p <sub>1/2</sub>	6.289–2	1.413+0	1.101+0	3.884–2
	5p <sub>3/2</sub>	1.017–1	1.496+0	1.197+0	4.158–2
	6s <sub>1/2</sub>	8.320–3	1.993+0	1.397–1	–1.056–3
64	3s <sub>1/2</sub>	1.718+0	1.991+0	1.396–1	–1.296–3
	3p <sub>1/2</sub>	1.535+0	1.394+0	1.166+0	4.983–2
	3p <sub>3/2</sub>	2.604+0	1.484+0	1.269+0	5.179–2
	3d <sub>3/2</sub>	6.831–1	8.692–1	1.585+0	2.511–1
	3d <sub>5/2</sub>	9.193–1	7.988–1	1.536+0	2.780–1
	4s <sub>1/2</sub>	5.371–1	1.991+0	1.187–1	–1.179–3
	4p <sub>1/2</sub>	4.480–1	1.419+0	1.089+0	3.850–2
	4p <sub>3/2</sub>	7.473–1	1.506+0	1.189+0	4.157–2
	4d <sub>3/2</sub>	1.891–1	8.846–1	1.528+0	2.261–1
	4d <sub>5/2</sub>	2.525–1	8.094–1	1.481+0	2.522–1
65	3s <sub>1/2</sub>	1.868+0	1.986+0	1.986–1	6.043–2
	3p <sub>1/2</sub>	1.777+0	1.424+0	1.094+0	4.340–2
	3p <sub>3/2</sub>	3.014+0	1.523+0	1.204+0	4.710–2
	3d <sub>3/2</sub>	8.862–1	9.162–1	1.600+0	2.377–1
	3d <sub>5/2</sub>	1.187+0	8.355–1	1.548+0	2.661–1
	4s <sub>1/2</sub>	6.100–1	1.986+0	4.162–2	–1.505–3
	4p <sub>1/2</sub>	5.421–1	1.453+0	1.008+0	3.147–2
	4p <sub>3/2</sub>	8.995–1	1.549+0	1.113+0	3.641–2
	4d <sub>3/2</sub>	2.576–1	9.369–1	1.531+0	2.097–1
	4d <sub>5/2</sub>	3.417–1	8.503–1	1.482+0	2.371–1
	4f <sub>5/2</sub>	8.744–3	5.026–1	1.318+0	4.706–1
	5s <sub>1/2</sub>	1.109–1	1.988+0	6.202–2	–1.354–3
	5p <sub>1/2</sub>	7.979–2	1.448+0	1.020+0	3.144–2
	5p <sub>3/2</sub>	1.280–1	1.541+0	1.122+0	3.596–2
66	5d <sub>3/2</sub>	1.505–2	9.228–1	1.524+0	2.112–1
	6s <sub>1/2</sub>	1.035–2	1.988+0	6.058–2	–1.349–3
67	3s <sub>1/2</sub>	1.868+0	1.986+0	6.043–2	–1.668–3
	3p <sub>1/2</sub>	1.777+0	1.424+0	1.094+0	4.340–2
	3p <sub>3/2</sub>	3.014+0	1.523+0	1.204+0	4.710–2
	3d <sub>3/2</sub>	8.862–1	9.162–1	1.600+0	2.377–1
	3d <sub>5/2</sub>	1.187+0	8.355–1	1.548+0	2.661–1
	4s <sub>1/2</sub>	6.100–1	1.986+0	4.162–2	–1.505–3
	4p <sub>1/2</sub>	5.421–1	1.453+0	1.008+0	3.147–2
	4p <sub>3/2</sub>	8.995–1	1.549+0	1.113+0	3.641–2
	4d <sub>3/2</sub>	2.576–1	9.369–1	1.531+0	2.097–1
	4d <sub>5/2</sub>	3.417–1	8.503–1	1.482+0	2.371–1
	4f <sub>5/2</sub>	8.744–3	5.026–1	1.318+0	4.706–1
	5f <sub>7/2</sub>	1.073–2	4.954–1	1.291+0	4.883–1
	5s <sub>1/2</sub>	1.100–1	1.986+0	3.717–2	–1.467–3
	5p <sub>1/2</sub>	7.896–2	1.460+0	9.915–1	2.917–2
	5p <sub>3/2</sub>	1.253–1	1.555+0	1.095+0	3.437–2
	6s <sub>1/2</sub>	9.019–3	1.986+0	3.580–2	–1.465–3
68	3s <sub>1/2</sub>	1.718+0	1.991+0	1.396–1	–1.296–3
	3p <sub>1/2</sub>	1.535+0	1.394+0	1.166+0	4.983–2
	3p <sub>3/2</sub>	2.604+0	1.484+0	1.269+0	5.179–2
	3d <sub>3/2</sub>	6.831–1	8.692–1	1.585+0	2.511–1
	3d <sub>5/2</sub>	9.193–1	7.988–1	1.536+0	2.780–1
	4s <sub>1/2</sub>	5.371–1	1.991+0	1.187–1	–1.179–3
	4p <sub>1/2</sub>	4.480–1	1.419+0	1.089+0	3.850–2
	4p <sub>3/2</sub>	7.473–1	1.506+0	1.189+0	4.157–2
	4d <sub>3/2</sub>	1.891–1	8.846–1	1.528+0	2.261–1
	4d <sub>5/2</sub>	2.525–1	8.094–1	1.481+0	2.522–1
69	3s <sub>1/2</sub>	1.718+0	1.991+0	1.396–1	–1.296–3
	3p <sub>1/2</sub>	1.535+0	1.394+0	1.166+0	4.983–2
	3p <sub>3/2</sub>	2.604+0	1.484+0	1.269+0	5.179–2
	3d <sub>3/2</sub>	6.831–1	8.692–1	1.585+0	2.511–1
	3d <sub>5/2</sub>	9.193–1	7.988–1	1.536+0	2.780–1
	4s <sub>1/2</sub>	5.371–1	1.991+0	1.187–1	–1.179–3
	4p <sub>1/2</sub>	4.480–1	1.419+0	1.089+0	3.850–2
	4p <sub>3/2</sub>	7.473–1	1.506+0	1.189+0	4.157–2
	4d <sub>3/2</sub>	1.891–1	8.846–1	1.528+0	2.261–1
	4d <sub>5/2</sub>	2.525–1	8.094–1	1.481+0	2.522–1
70	3s <sub>1/2</sub>	1.718+0	1.991+0	1.396–1	–1.296–3
	3p <sub>1/2</sub>	1.535+0	1.394+0	1.166+0	4.983–2
	3p <sub>3/2</sub>	2.604+0	1.484+0	1.269+0	5.179–2
	3d <sub>3/2</sub>	6.831–1	8.692–1	1.585+0	2.511–1
	3d <sub>5/2</sub>	9.193–1	7.988–1	1.536+0	2.780–1
	4s <sub>1/2</sub>	5.371–1	1.991+0	1.187–1	–1.179–3
	4p <sub>1/2</sub>	4.480–1	1.419+0	1.089+0	3.850–2
	4p <sub>3/2</sub>	7.473–1	1.506+0	1.189+0	4.157–2
	4d <sub>3/2</sub>	1.891–1	8.846–1	1.528+0	2.261–1
	4d <sub>5/2</sub>	2.525–1	8.094–1	1.481+0	2.522–1
71	3s <sub>1/2</sub>	1.718+0	1.991+0	1.396–1	–1.296–3
	3p <sub>1/2</sub>	1.535+0	1.394+0	1.166+0	4.983–2
	3p <sub>3/2</sub>	2.604+0	1.484+0	1.269+0	5.179–2
	3d <sub>3/2</sub>	6.831–1	8.692–1	1.585+0	2.511–1
	3d <sub>5/2</sub>	9.193–1	7.988–1	1.536+0	2.780–1
	4s <sub>1/2</sub>	5.371–1	1.991+0	1.187–1	–1.179–3
	4p <sub>1/2</sub>	4.480–1	1.419+0	1.089+0	3.850–2
	4p <sub>3/2</sub>	7.473–1	1.506+0	1.189+0	4.157–2
	4d <sub>3/2</sub>	1.891–1	8.846–1	1.528+0	2.261–1
	4d <sub>5/2</sub>	2.525–1	8.094–1	1.481+0	2.522–1
72	3s <sub>1/2</sub>	1.718+0	1.991+0	1.396–1	–1.296–3
	3p <sub>1/2</sub>	1.535+0	1.394+0	1.166+0	4.983–2
	3p <sub>3/2</sub>	2.604+0	1.484+0	1.269+0	5.179–2
	3d <sub>3/2</sub>	6.831–1	8.692–1	1.585+0	2.511–1
	3d <sub>5/2</sub>	9.193–1	7.988–1	1.536+0	2.780–1
	4s <sub>1/2</sub>	5.371–1	1.991+0	1.187–1	–1.179–3
	4p <sub>1/2</sub>	4.480–1	1.419+0	1.089+0	3.850–2
	4p <sub>3/2</sub>	7.473–1	1.506+0	1.189+0	4.157–2
	4d <sub>3/2</sub>	1.891–1	8.846–1	1.52	

Table 2 (continued)

Z	Shell	$\sigma$	$\beta$	$\gamma$	$\delta$
	4f <sub>5/2</sub>	1.040–2	5.122–1	1.331+0	4.651–1
	4f <sub>7/2</sub>	1.273–2	5.042–1	1.303+0	4.830–1
	5s <sub>1/2</sub>	1.140–1	1.984+0	1.410–2	−1.585–3
	5p <sub>1/2</sub>	8.318–2	1.471+0	9.630–1	2.698–2
	5p <sub>3/2</sub>	1.314–1	1.569+0	1.068+0	3.289–2
	6s <sub>1/2</sub>	9.188–3	1.984+0	1.277–2	−1.583–3
67	3p <sub>1/2</sub>	1.942+0	1.443+0	1.044+0	3.947–2
	3p <sub>3/2</sub>	3.295+0	1.548+0	1.157+0	4.456–2
	3d <sub>3/2</sub>	1.041+0	9.467–1	1.606+0	2.294–1
	3d <sub>5/2</sub>	1.391+0	8.592–1	1.552+0	2.586–1
	4s <sub>1/2</sub>	6.593–1	1.982+0	−3.920–3	−1.760–3
	4p <sub>1/2</sub>	6.090–1	1.475+0	9.529–1	2.724–2
	4p <sub>3/2</sub>	1.008+0	1.576+0	1.060+0	3.362–2
	4d <sub>3/2</sub>	3.117–1	9.712–1	1.528+0	1.995–1
	4d <sub>5/2</sub>	4.117–1	8.771–1	1.478+0	2.276–1
	4f <sub>5/2</sub>	1.230–2	5.219–1	1.342+0	4.597–1
	4f <sub>7/2</sub>	1.502–2	5.130–1	1.314+0	4.778–1
	5s <sub>1/2</sub>	1.180–1	1.982+0	−7.755–3	−1.711–3
	5p <sub>1/2</sub>	8.748–2	1.482+0	9.342–1	2.488–2
	5p <sub>3/2</sub>	1.375–1	1.583+0	1.041+0	3.155–2
	6s <sub>1/2</sub>	9.354–3	1.982+0	−9.038–3	−1.709–3
68	3p <sub>3/2</sub>	3.438+0	1.560+0	1.132+0	4.349–2
	3d <sub>3/2</sub>	1.125+0	9.616–1	1.608+0	2.254–1
	3d <sub>5/2</sub>	1.500+0	8.707–1	1.554+0	2.551–1
	4s <sub>1/2</sub>	6.844–1	1.980+0	−2.488–2	−1.899–3
	4p <sub>1/2</sub>	6.438–1	1.485+0	9.246–1	2.528–2
	4p <sub>3/2</sub>	1.065+0	1.589+0	1.033+0	3.243–2
	4d <sub>3/2</sub>	3.415–1	9.881–1	1.525+0	1.946–1
	4d <sub>5/2</sub>	4.500–1	8.902–1	1.475+0	2.231–1
	4f <sub>5/2</sub>	1.445–2	5.316–1	1.353+0	4.542–1
	4f <sub>7/2</sub>	1.762–2	5.218–1	1.325+0	4.726–1
	5s <sub>1/2</sub>	1.220–1	1.980+0	−2.839–2	−1.846–3
	5p <sub>1/2</sub>	9.186–2	1.493+0	9.050–1	2.286–2
	5p <sub>3/2</sub>	1.437–1	1.596+0	1.013+0	3.032–2
	6s <sub>1/2</sub>	9.519–3	1.980+0	−2.965–2	−1.839–3
69	3p <sub>3/2</sub>	3.581+0	1.571+0	1.107+0	4.250–2
	3d <sub>3/2</sub>	1.212+0	9.763–1	1.609+0	2.216–1
	3d <sub>5/2</sub>	1.614+0	8.821–1	1.554+0	2.516–1
	4s <sub>1/2</sub>	7.095–1	1.977+0	−4.464–2	−2.048–3
	4p <sub>1/2</sub>	6.794–1	1.495+0	8.958–1	2.336–2
	4p <sub>3/2</sub>	1.122+0	1.602+0	1.005+0	3.134–2
	4d <sub>3/2</sub>	3.732–1	1.005+0	1.521+0	1.899–1
	4d <sub>5/2</sub>	4.907–1	9.032–1	1.472+0	2.187–1
	4f <sub>5/2</sub>	1.690–2	5.413–1	1.363+0	4.490–1
	4f <sub>7/2</sub>	2.055–2	5.307–1	1.334+0	4.675–1
	5s <sub>1/2</sub>	1.261–1	1.977+0	−4.780–2	−1.989–3
	5p <sub>1/2</sub>	9.633–2	1.503+0	8.755–1	2.092–2
	5p <sub>3/2</sub>	1.500–1	1.608+0	9.842–1	2.921–2
	6s <sub>1/2</sub>	9.683–3	1.977+0	−4.900–2	−1.982–3
70	3p <sub>3/2</sub>	3.726+0	1.582+0	1.082+0	4.162–2
	3d <sub>3/2</sub>	1.304+0	9.909–1	1.609+0	2.179–1
	3d <sub>5/2</sub>	1.734+0	8.933–1	1.554+0	2.482–1
	4s <sub>1/2</sub>	7.346–1	1.974+0	−6.314–2	−2.206–3
	4p <sub>1/2</sub>	7.159–1	1.504+0	8.668–1	2.152–2
	4p <sub>3/2</sub>	1.182+0	1.614+0	9.772–1	3.036–2
	4d <sub>3/2</sub>	4.069–1	1.022+0	1.517+0	1.854–1
	4d <sub>5/2</sub>	5.337–1	9.161–1	1.467+0	2.143–1
	4f <sub>5/2</sub>	1.966–2	5.511–1	1.372+0	4.438–1
	4f <sub>7/2</sub>	2.385–2	5.396–1	1.343+0	4.624–1
	5s <sub>1/2</sub>	1.301–1	1.974+0	−6.595–2	−2.141–3
	5p <sub>1/2</sub>	1.009–1	1.513+0	8.458–1	1.906–2
	5p <sub>3/2</sub>	1.564–1	1.621+0	9.554–1	2.822–2
	6s <sub>1/2</sub>	9.842–3	1.974+0	−6.709–2	−2.134–3

Table 2 (continued)

Z	Shell	$\sigma$	$\beta$	$\gamma$	$\delta$
71	3d <sub>3/2</sub>	1.395+0	1.005+0	1.608+0	2.144–1
	3d <sub>5/2</sub>	1.853+0	9.040–1	1.554+0	2.450–1
	4s <sub>1/2</sub>	7.606–1	1.971+0	−8.000–2	−2.374–3
	4p <sub>1/2</sub>	7.544–1	1.514+0	8.378–1	1.978–2
	4p <sub>3/2</sub>	1.245+0	1.625+0	9.492–1	2.952–2
	4d <sub>3/2</sub>	4.443–1	1.038+0	1.511+0	1.810–1
	4d <sub>5/2</sub>	5.818–1	9.286–1	1.462+0	2.101–1
	4f <sub>5/2</sub>	2.383–2	5.606–1	1.380+0	4.387–1
	4f <sub>7/2</sub>	2.896–2	5.482–1	1.351+0	4.574–1
	5s <sub>1/2</sub>	1.395–1	1.971+0	−8.244–2	−2.302–3
	5p <sub>1/2</sub>	1.117–1	1.522+0	8.166–1	1.730–2
	5p <sub>3/2</sub>	1.739–1	1.633+0	9.269–1	2.735–2
	5d <sub>3/2</sub>	2.108–2	1.044+0	1.498+0	1.762–1
	6s <sub>1/2</sub>	1.194–2	1.971+0	−8.352–2	−2.298–3
72	3d <sub>3/2</sub>	1.490+0	1.019+0	1.606+0	2.111–1
	3d <sub>5/2</sub>	1.975+0	9.145–1	1.552+0	2.420–1
	4s <sub>1/2</sub>	7.866–1	1.968+0	−9.563–2	−2.553–3
	4p <sub>1/2</sub>	7.933–1	1.523+0	8.095–1	1.813–2
	4p <sub>3/2</sub>	1.310+0	1.637+0	9.215–1	2.879–2
	4d <sub>3/2</sub>	4.842–1	1.054+0	1.505+0	1.768–1
	4d <sub>5/2</sub>	6.332–1	9.409–1	1.457+0	2.061–1
	4f <sub>5/2</sub>	2.859–2	5.700–1	1.388+0	4.338–1
	4f <sub>7/2</sub>	3.478–2	5.567–1	1.359+0	4.527–1
	5s <sub>1/2</sub>	1.493–1	1.968+0	−9.771–2	−2.473–3
	5p <sub>1/2</sub>	1.232–1	1.532+0	7.873–1	1.560–2
	5p <sub>3/2</sub>	1.924–1	1.644+0	8.983–1	2.657–2
	5d <sub>3/2</sub>	2.803–2	1.060+0	1.490+0	1.717–1
	6s <sub>1/2</sub>	1.361–2	1.968+0	−9.876–2	−2.462–3
73	3d <sub>3/2</sub>	1.587+0	1.032+0	1.604+0	2.079–1
	3d <sub>5/2</sub>	2.102+0	9.248–1	1.551+0	2.390–1
	4s <sub>1/2</sub>	8.130–1	1.965+0	−1.100–1	−2.743–3
	4p <sub>1/2</sub>	8.333–1	1.531+0	7.811–1	1.655–2
	4p <sub>3/2</sub>	1.377+0	1.648+0	8.936–1	2.817–2
	4d <sub>3/2</sub>	5.270–1	1.070+0	1.498+0	1.728–1
	4d <sub>5/2</sub>	6.880–1	9.530–1	1.451+0	2.022–1
	4f <sub>5/2</sub>	3.400–2	5.794–1	1.395+0	4.289–1
	4f <sub>7/2</sub>	4.139–2	5.651–1	1.367+0	4.479–1
	5s <sub>1/2</sub>	1.596–1	1.965+0	−1.117–1	−2.654–3
	5p <sub>1/2</sub>	1.353–1	1.541+0	7.581–1	1.398–2
	5p <sub>3/2</sub>	2.119–1	1.655+0	8.695–1	2.590–2
	5d <sub>3/2</sub>	3.531–2	1.077+0	1.482+0	1.674–1
	6s <sub>1/2</sub>	1.507–2	1.965+0	−1.127–1	−2.640–3
74	3d <sub>3/2</sub>	1.688+0	1.046+0	1.601+0	2.050–1
	3d <sub>5/2</sub>	2.231+0	9.349–1	1.549+0	2.362–1
	4s <sub>1/2</sub>	8.396–1	1.961+0	−1.232–1	−2.944–3
	4p <sub>1/2</sub>	8.744–1	1.540+0	7.525–1	1.503–2
	4p <sub>3/2</sub>	1.446+0	1.658+0	8.653–1	2.764–2
	4d <sub>3/2</sub>	5.725–1	1.086+0	1.489+0	1.689–1
	4d <sub>5/2</sub>	7.464–1	9.651–1	1.444+0	1.984–1
	4f <sub>5/2</sub>	4.014–2	5.887–1	1.402+0	4.241–1
	4f <sub>7/2</sub>	4.886–2	5.735–1	1.374+0	4.432–1
	5s <sub>1/2</sub>	1.702–1	1.961+0	−1.245–1	−2.846–3
	5p <sub>1/2</sub>	1.481–1	1.550+0	7.288–1	1.242–2
	5p <sub>3/2</sub>	2.323–1	1.666+0	8.405–1	2.532–2
	5d <sub>3/2</sub>	4.311–2	1.093+0	1.473+0	1.632–1
	6s <sub>1/2</sub>	1.642–2	1.961+0	−1.255–1	−2.830–3
75	3d <sub>3/2</sub>	1.791+0	1.059+0	1.598+0	2.021–1
	3d <sub>5/2</sub>	2.364+0	9.448–1	1.546+0	2.335–1
	4s <sub>1/2</sub>	8.663–1	1.957+0	−1.350–1	−3.157–3
	4p <sub>1/2</sub>	9.162–1	1.548+0	7.239–1	1.357–2
	4p <sub>3/2</sub>	1.518+0	1.668+0	8.369–1	2.720–2
	4d <sub>3/2</sub>	6.209–1	1.101+0	1.481+0	1.652–1
	4d <sub>5/2</sub>	8.082–1	9.770–1	1.437+0	1.946–1

Table 2 (continued)

Z	Shell	$\sigma$	$\beta$	$\gamma$	$\delta$
	4f <sub>5/2</sub>	4.706–2	5.979–1	1.409+0	4.194–1
	4f <sub>7/2</sub>	5.728–2	5.818–1	1.381+0	4.385–1
	5s <sub>1/2</sub>	1.812–1	1.957+0	−1.360–1	−3.049–3
	5p <sub>1/2</sub>	1.615–1	1.559+0	6.995–1	1.093–2
	5p <sub>3/2</sub>	2.540–1	1.677+0	8.114–1	2.484–2
	5d <sub>3/2</sub>	5.187–2	1.109+0	1.462+0	1.592–1
	5d <sub>5/2</sub>	6.442–2	9.832–1	1.421+0	1.883–1
	6s <sub>1/2</sub>	1.780–2	1.957+0	−1.369–1	−3.033–3
76	3d <sub>5/2</sub>	2.500+0	9.546–1	1.543+0	2.308–1
	4s <sub>1/2</sub>	8.930–1	1.953+0	−1.456–1	−3.383–3
	4p <sub>1/2</sub>	9.587–1	1.556+0	6.954–1	1.217–2
	4p <sub>3/2</sub>	1.591+0	1.678+0	8.084–1	2.685–2
	4d <sub>3/2</sub>	6.721–1	1.117+0	1.471+0	1.616–1
	4d <sub>5/2</sub>	8.737–1	9.887–1	1.429+0	1.910–1
	4f <sub>5/2</sub>	5.483–2	6.072–1	1.415+0	4.147–1
	4f <sub>7/2</sub>	6.671–2	5.900–1	1.388+0	4.339–1
	5s <sub>1/2</sub>	1.925–1	1.953+0	−1.462–1	−3.263–3
	5p <sub>1/2</sub>	1.755–1	1.567+0	6.703–1	9.495–3
	5p <sub>3/2</sub>	2.765–1	1.687+0	7.823–1	2.445–2
	5d <sub>3/2</sub>	6.132–2	1.125+0	1.451+0	1.553–1
	5d <sub>5/2</sub>	7.619–2	9.954–1	1.412+0	1.844–1
	6s <sub>1/2</sub>	1.909–2	1.953+0	−1.470–1	−3.248–3
77	4s <sub>1/2</sub>	9.197–1	1.948+0	−1.550–1	−3.622–3
	4p <sub>1/2</sub>	1.002+0	1.563+0	6.670–1	1.083–2
	4p <sub>3/2</sub>	1.666+0	1.687+0	7.799–1	2.659–2
	4d <sub>3/2</sub>	7.261–1	1.132+0	1.461+0	1.582–1
	4d <sub>5/2</sub>	9.426–1	1.000+0	1.421+0	1.875–1
	4f <sub>5/2</sub>	6.351–2	6.163–1	1.421+0	4.101–1
	4f <sub>7/2</sub>	7.724–2	5.982–1	1.394+0	4.294–1
	5s <sub>1/2</sub>	2.041–1	1.948+0	−1.552–1	−3.490–3
	5p <sub>1/2</sub>	1.900–1	1.576+0	6.412–1	8.122–3
	5p <sub>3/2</sub>	2.999–1	1.696+0	7.530–1	2.414–2
	5d <sub>3/2</sub>	7.154–2	1.141+0	1.439+0	1.515–1
	5d <sub>5/2</sub>	8.884–2	1.007+0	1.402+0	1.805–1
	6s <sub>1/2</sub>	2.031–2	1.948+0	−1.559–1	−3.473–3
78	4s <sub>1/2</sub>	9.466–1	1.943+0	−1.631–1	−3.875–3
	4p <sub>1/2</sub>	1.046+0	1.571+0	6.384–1	9.527–3
	4p <sub>3/2</sub>	1.743+0	1.696+0	7.511–1	2.641–2
	4d <sub>3/2</sub>	7.835–1	1.147+0	1.450+0	1.549–1
	4d <sub>5/2</sub>	1.016+0	1.012+0	1.412+0	1.841–1
	4f <sub>5/2</sub>	7.323–2	6.255–1	1.427+0	4.056–1
	4f <sub>7/2</sub>	8.901–2	6.063–1	1.401+0	4.249–1
	5s <sub>1/2</sub>	2.150–1	1.943+0	−1.630–1	−3.730–3
	5p <sub>1/2</sub>	2.037–1	1.584+0	6.120–1	6.796–3
	5p <sub>3/2</sub>	3.209–1	1.706+0	7.234–1	2.390–2
	5d <sub>3/2</sub>	7.835–2	1.157+0	1.427+0	1.479–1
	5d <sub>5/2</sub>	9.630–2	1.020+0	1.392+0	1.767–1
	6s <sub>1/2</sub>	1.891–2	1.943+0	−1.635–1	−3.713–3
79	4s <sub>1/2</sub>	9.729–1	1.938+0	−1.698–1	−4.143–3
	4p <sub>1/2</sub>	1.090+0	1.578+0	6.103–1	8.287–3
	4p <sub>3/2</sub>	1.821+0	1.704+0	7.225–1	2.631–2
	4d <sub>3/2</sub>	8.433–1	1.161+0	1.438+0	1.518–1
	4d <sub>5/2</sub>	1.092+0	1.023+0	1.403+0	1.808–1
	4f <sub>5/2</sub>	8.395–2	6.345–1	1.432+0	4.012–1
	4f <sub>7/2</sub>	1.020–1	6.143–1	1.407+0	4.206–1
	5s <sub>1/2</sub>	2.269–1	1.938+0	−1.693–1	−3.982–3
	5p <sub>1/2</sub>	2.192–1	1.591+0	5.831–1	5.534–3
	5p <sub>3/2</sub>	3.459–1	1.714+0	6.941–1	2.375–2
	5d <sub>3/2</sub>	8.995–2	1.172+0	1.413+0	1.445–1
	5d <sub>5/2</sub>	1.105–1	1.031+0	1.381+0	1.730–1
	6s <sub>1/2</sub>	1.987–2	1.938+0	−1.698–1	−3.962–3

Table 2 (continued)

Z	Shell	$\sigma$	$\beta$	$\gamma$	$\delta$
80	4s <sub>1/2</sub>	9.983–1	1.932+0	−1.753–1	−4.427–3
	4p <sub>1/2</sub>	1.134+0	1.585+0	5.827–1	7.105–3
	4p <sub>3/2</sub>	1.900+0	1.712+0	6.944–1	2.630–2
	4d <sub>3/2</sub>	9.050–1	1.175+0	1.425+0	1.489–1
	4d <sub>5/2</sub>	1.170+0	1.034+0	1.394+0	1.776–1
	4f <sub>5/2</sub>	9.570–2	6.435–1	1.438+0	3.970–1
	4f <sub>7/2</sub>	1.162–1	6.222–1	1.413+0	4.163–1
	5s <sub>1/2</sub>	2.396–1	1.932+0	−1.744–1	−4.249–3
	5p <sub>1/2</sub>	2.364–1	1.599+0	5.548–1	4.333–3
	5p <sub>3/2</sub>	3.750–1	1.723+0	6.652–1	2.367–2
	5d <sub>3/2</sub>	1.071–1	1.187+0	1.399+0	1.412–1
	5d <sub>5/2</sub>	1.325–1	1.043+0	1.370+0	1.694–1
	6s <sub>1/2</sub>	2.369–2	1.932+0	−1.746–1	−4.224–3
81	4s <sub>1/2</sub>	1.023+0	1.927+0	−1.794–1	−4.727–3
	4p <sub>1/2</sub>	1.177+0	1.592+0	5.556–1	5.974–3
	4p <sub>3/2</sub>	1.978+0	1.720+0	6.666–1	2.636–2
	4d <sub>3/2</sub>	9.691–1	1.189+0	1.412+0	1.461–1
	4d <sub>5/2</sub>	1.251+0	1.045+0	1.384+0	1.745–1
	4f <sub>5/2</sub>	1.085–1	6.523–1	1.443+0	3.929–1
	4f <sub>7/2</sub>	1.317–1	6.300–1	1.419+0	4.122–1
	5s <sub>1/2</sub>	2.526–1	1.927+0	−1.781–1	−4.532–3
	5p <sub>1/2</sub>	2.542–1	1.606+0	5.271–1	3.190–3
	5p <sub>3/2</sub>	4.057–1	1.730+0	6.368–1	2.368–2
	5d <sub>3/2</sub>	1.265–1	1.202+0	1.384+0	1.381–1
	5d <sub>5/2</sub>	1.576–1	1.054+0	1.359+0	1.660–1
	6s <sub>1/2</sub>	2.936–2	1.926+0	−1.781–1	−4.499–3
	6p <sub>1/2</sub>	1.540–2	1.609+0	5.218–1	2.723–3
82	4s <sub>1/2</sub>	1.047+0	1.920+0	−1.822–1	−5.044–3
	4p <sub>1/2</sub>	1.220+0	1.598+0	5.287–1	4.883–3
	4p <sub>3/2</sub>	2.058+0	1.727+0	6.390–1	2.648–2
	4d <sub>3/2</sub>	1.036+0	1.203+0	1.399+0	1.435–1
	4d <sub>5/2</sub>	1.336+0	1.055+0	1.374+0	1.715–1
	4f <sub>5/2</sub>	1.226–1	6.610–1	1.448+0	3.888–1
	4f <sub>7/2</sub>	1.487–1	6.377–1	1.425+0	4.082–1
	5s <sub>1/2</sub>	2.660–1	1.920+0	−1.804–1	−4.828–3
	5p <sub>1/2</sub>	2.728–1	1.613+0	4.996–1	2.094–3
	5p <sub>3/2</sub>	4.381–1	1.738+0	6.085–1	2.374–2
	5d <sub>3/2</sub>	1.473–1	1.216+0	1.368+0	1.351–1
	5d <sub>5/2</sub>	1.841–1	1.066+0	1.347+0	1.626–1
	6s <sub>1/2</sub>	3.429–2	1.920+0	−1.802–1	−4.791–3
	6p <sub>1/2</sub>	2.109–2	1.616+0	4.939–1	1.609–3
83	4s <sub>1/2</sub>	1.071+0	1.914+0	−1.835–1	−5.378–3
	4p <sub>1/2</sub>	1.263+0	1.604+0	5.021–1	3.833–3
	4p <sub>3/2</sub>	2.139+0	1.733+0	6.114–1	2.667–2
	4d <sub>3/2</sub>	1.105+0	1.216+0	1.384+0	1.410–1
	4d <sub>5/2</sub>	1.424+0	1.066+0	1.364+0	1.686–1
	4f <sub>5/2</sub>	1.380–1	6.697–1	1.452+0	3.849–1
	4f <sub>7/2</sub>	1.672–1	6.454–1	1.430+0	4.042–1
	5s <sub>1/2</sub>	2.795–1	1.914+0	−1.813–1	−5.141–3
	5p <sub>1/2</sub>	2.919–1	1.620+0	4.725–1	1.044–3
	5p <sub>3/2</sub>	4.719–1	1.745+0	5.804–1	2.386–2
	5d <sub>3/2</sub>	1.697–1	1.230+0	1.352+0	1.323–1
	5d <sub>5/2</sub>	2.128–1	1.077+0	1.334+0	1.593–1
	6s <sub>1/2</sub>	3.966–2	1.914+0	−1.810–1	−5.094–3
	6p <sub>1/2</sub>	2.762–2	1.623+0	4.664–1	5.416–4
	6p <sub>3/2</sub>	3.640–2	1.747+0	5.742–1	2.341–2
	4f <sub>5/2</sub>	8.395–2	6.345–1	1.432+0	4.012–1
	4f <sub>7/2</sub>	1.020–1	6.143–1	1.407+0	4.206–1
	5s <sub>1/2</sub>	2.269–1	1.938+0	−1.693–1	−3.982–3
	5p <sub>1/2</sub>	2.192–1	1.591+0	5.831–1	5.534–3
	5p <sub>3/2</sub>	3.459–1	1.714+0	6.941–1	2.375–2
	5d <sub>3/2</sub>	8.995–2	1.172+0	1.413+0	1.445–1
	5d <sub>5/2</sub>	1.105–1	1.031+0	1.381+0	1.730–1
	6s <sub>1/2</sub>	1.987–2	1.938+0	−1.698–1	−3.962–3

(continued on next page)

Table 2 (continued)

Z	Shell	$\sigma$	$\beta$	$\gamma$	$\delta$
85	4f <sub>7/2</sub>	1.873–1	6.529–1	1.436+0	4.003–1
	5s <sub>1/2</sub>	2.933–1	1.907+0	−1.808–1	−5.466–3
	5p <sub>1/2</sub>	3.115–1	1.627+0	4.456–1	3.999–5
	5p <sub>3/2</sub>	5.071–1	1.751+0	5.523–1	2.403–2
	5d <sub>3/2</sub>	1.937–1	1.244+0	1.335+0	1.297–1
	5d <sub>5/2</sub>	2.434–1	1.088+0	1.321+0	1.562–1
	6s <sub>1/2</sub>	4.494–2	1.906+0	−1.804–1	−5.416–3
	6p <sub>1/2</sub>	3.385–2	1.630+0	4.393–1	−4.835–4
	6p <sub>3/2</sub>	4.637–2	1.753+0	5.460–1	2.356–2
	4s <sub>1/2</sub>	1.117+0	1.899+0	−1.820–1	−6.096–3
	4p <sub>1/2</sub>	1.349+0	1.615+0	4.497–1	1.841–3
	4p <sub>3/2</sub>	2.305+0	1.745+0	5.563–1	2.718–2
	4d <sub>3/2</sub>	1.252+0	1.242+0	1.353+0	1.366–1
	4d <sub>5/2</sub>	1.609+0	1.086+0	1.341+0	1.632–1
86	4f <sub>5/2</sub>	1.729–1	6.869–1	1.460+0	3.772–1
	4f <sub>7/2</sub>	2.091–1	6.604–1	1.441+0	3.965–1
	5s <sub>1/2</sub>	3.072–1	1.899+0	−1.790–1	−5.811–3
	5p <sub>1/2</sub>	3.317–1	1.633+0	4.192–1	−9.267–4
	5p <sub>3/2</sub>	5.437–1	1.757+0	5.245–1	2.425–2
	5d <sub>3/2</sub>	2.192–1	1.258+0	1.316+0	1.272–1
	5d <sub>5/2</sub>	2.759–1	1.099+0	1.308+0	1.531–1
	6s <sub>1/2</sub>	5.027–2	1.899+0	−1.785–1	−5.754–3
	6p <sub>1/2</sub>	4.009–2	1.636+0	4.127–1	−1.467–3
	6p <sub>3/2</sub>	5.628–2	1.759+0	5.180–1	2.375–2
	4s <sub>1/2</sub>	1.139+0	1.891+0	−1.791–1	−6.485–3
	4p <sub>1/2</sub>	1.392+0	1.621+0	4.241–1	8.878–4
	4p <sub>3/2</sub>	2.389+0	1.750+0	5.292–1	2.751–2
	4d <sub>3/2</sub>	1.330+0	1.255+0	1.336+0	1.345–1
87	4d <sub>5/2</sub>	1.707+0	1.096+0	1.329+0	1.605–1
	4f <sub>5/2</sub>	1.926–1	6.953–1	1.464+0	3.735–1
	4f <sub>7/2</sub>	2.328–1	6.678–1	1.446+0	3.927–1
	5s <sub>1/2</sub>	3.212–1	1.891+0	−1.757–1	−6.172–3
	5p <sub>1/2</sub>	3.523–1	1.639+0	3.934–1	−1.860–3
	5p <sub>3/2</sub>	5.814–1	1.762+0	4.972–1	2.452–2
	5d <sub>3/2</sub>	2.463–1	1.271+0	1.297+0	1.248–1
	5d <sub>5/2</sub>	3.102–1	1.109+0	1.293+0	1.501–1
	6s <sub>1/2</sub>	5.566–2	1.891+0	−1.750–1	−6.104–3
	6p <sub>1/2</sub>	4.646–2	1.643+0	3.865–1	−2.413–3
	6p <sub>3/2</sub>	6.633–2	1.765+0	4.904–1	2.398–2
	4s <sub>1/2</sub>	1.160+0	1.882+0	−1.748–1	−6.896–3
	4p <sub>1/2</sub>	1.433+0	1.626+0	3.993–1	−2.825–5
	4p <sub>3/2</sub>	2.472+0	1.754+0	5.028–1	2.789–2
88	4d <sub>3/2</sub>	1.408+0	1.266+0	1.319+0	1.327–1
	4d <sub>5/2</sub>	1.806+0	1.106+0	1.316+0	1.580–1
	4f <sub>5/2</sub>	2.136–1	7.037–1	1.467+0	3.698–1
	4f <sub>7/2</sub>	2.580–1	6.751–1	1.450+0	3.890–1
	5s <sub>1/2</sub>	3.351–1	1.882+0	−1.711–1	−6.552–3
	5p <sub>1/2</sub>	3.730–1	1.645+0	3.683–1	−2.752–3
	5p <sub>3/2</sub>	6.201–1	1.767+0	4.706–1	2.483–2
	5d <sub>3/2</sub>	2.751–1	1.284+0	1.278+0	1.226–1
	5d <sub>5/2</sub>	3.468–1	1.120+0	1.279+0	1.472–1
	6s <sub>1/2</sub>	6.261–2	1.882+0	−1.703–1	−6.478–3
	6p <sub>1/2</sub>	5.605–2	1.649+0	3.613–1	−3.311–3
	6p <sub>3/2</sub>	8.487–2	1.770+0	4.635–1	2.426–2
	7s <sub>1/2</sub>	4.405–3	1.882+0	−1.702–1	−6.480–3

Table 2 (continued)

Z	Shell	$\sigma$	$\beta$	$\gamma$	$\delta$
89	5p <sub>1/2</sub>	3.940–1	1.650+0	3.438–1	−3.610–3
	5p <sub>3/2</sub>	6.601–1	1.771+0	4.443–1	2.517–2
	5d <sub>3/2</sub>	3.057–1	1.297+0	1.258+0	1.207–1
	5d <sub>5/2</sub>	3.856–1	1.130+0	1.265+0	1.445–1
	6s <sub>1/2</sub>	6.981–2	1.873+0	−1.642–1	−6.869–3
	6p <sub>1/2</sub>	6.555–2	1.655+0	3.367–1	−4.185–3
	6p <sub>3/2</sub>	1.020–1	1.774+0	4.371–1	2.457–2
	7s <sub>1/2</sub>	7.188–3	1.873+0	−1.639–1	−6.859–3
	4s <sub>1/2</sub>	1.198+0	1.864+0	−1.618–1	−7.780–3
	4p <sub>1/2</sub>	1.511+0	1.635+0	3.512–1	−1.792–3
	4p <sub>3/2</sub>	2.638+0	1.762+0	4.511–1	2.877–2
	4d <sub>3/2</sub>	1.573+0	1.289+0	1.282+0	1.295–1
	4d <sub>5/2</sub>	2.012+0	1.125+0	1.291+0	1.533–1
	4f <sub>5/2</sub>	2.606–1	7.202–1	1.470+0	3.627–1
	4f <sub>7/2</sub>	3.142–1	6.895–1	1.457+0	3.817–1
90	5s <sub>1/2</sub>	3.629–1	1.864+0	−1.575–1	−7.369–3
	5p <sub>1/2</sub>	4.154–1	1.656+0	3.197–1	−4.455–3
	5p <sub>3/2</sub>	7.014–1	1.775+0	4.184–1	2.554–2
	5d <sub>3/2</sub>	3.381–1	1.309+0	1.237+0	1.188–1
	5d <sub>5/2</sub>	4.267–1	1.140+0	1.250+0	1.418–1
	6s <sub>1/2</sub>	7.662–2	1.864+0	−1.565–1	−7.277–3
	6p <sub>1/2</sub>	7.430–2	1.660+0	3.126–1	−5.037–3
	6p <sub>3/2</sub>	1.172–1	1.778+0	4.111–1	2.491–2
	6d <sub>3/2</sub>	2.688–2	1.312+0	1.231+0	1.172–1
	7s <sub>1/2</sub>	8.853–3	1.864+0	−1.562–1	−7.265–3
	4s <sub>1/2</sub>	1.216+0	1.853+0	−1.529–1	−8.255–3
	4p <sub>1/2</sub>	1.550+0	1.639+0	3.278–1	−2.657–3
	4p <sub>3/2</sub>	2.722+0	1.765+0	4.257–1	2.926–2
	4d <sub>3/2</sub>	1.659+0	1.300+0	1.262+0	1.280–1
91	4d <sub>5/2</sub>	2.121+0	1.134+0	1.277+0	1.509–1
	4f <sub>5/2</sub>	2.868–1	7.284–1	1.471+0	3.592–1
	4f <sub>7/2</sub>	3.454–1	6.966–1	1.460+0	3.780–1
	5s <sub>1/2</sub>	3.769–1	1.854+0	−1.485–1	−7.807–3
	5p <sub>1/2</sub>	4.370–1	1.661+0	2.962–1	−5.282–3
	5p <sub>3/2</sub>	7.441–1	1.778+0	3.928–1	2.592–2
	5d <sub>3/2</sub>	3.722–1	1.321+0	1.215+0	1.170–1
	5d <sub>5/2</sub>	4.700–1	1.150+0	1.234+0	1.391–1
	6s <sub>1/2</sub>	8.333–2	1.853+0	−1.474–1	−7.707–3
	6p <sub>1/2</sub>	8.300–2	1.666+0	2.891–1	−5.874–3
	6p <sub>3/2</sub>	1.324–1	1.781+0	3.855–1	2.527–2
	6d <sub>3/2</sub>	3.496–2	1.324+0	1.208+0	1.153–1
	7s <sub>1/2</sub>	1.023–2	1.853+0	−1.469–1	−7.681–3
92	4s <sub>1/2</sub>	1.235+0	1.842+0	−1.422–1	−8.755–3
	4p <sub>1/2</sub>	1.589+0	1.644+0	3.042–1	−3.549–3
	4p <sub>3/2</sub>	2.811+0	1.767+0	3.998–1	2.975–2
	4d <sub>3/2</sub>	1.752+0	1.311+0	1.241+0	1.267–1
	4d <sub>5/2</sub>	2.237+0	1.143+0	1.262+0	1.486–1
	4f <sub>5/2</sub>	3.157–1	7.368–1	1.472+0	3.558–1
	4f <sub>7/2</sub>	3.800–1	7.039–1	1.462+0	3.744–1
	5s <sub>1/2</sub>	3.897–1	1.843+0	−1.377–1	−8.268–3
	5p <sub>1/2</sub>	4.569–1	1.666+0	2.727–1	−6.130–3
	5p <sub>3/2</sub>	7.819–1	1.781+0	3.668–1	2.632–2
	5d <sub>3/2</sub>	4.011–1	1.332+0	1.192+0	1.154–1
	5d <sub>5/2</sub>	5.052–1	1.161+0	1.217+0	1.364–1
	5f <sub>5/2</sub>	3.392–2	7.447–1	1.451+0	3.435–1
	6s <sub>1/2</sub>	8.432–2	1.842+0	−1.364–1	−8.158–3
	6p <sub>1/2</sub>	8.381–2	1.671+0	2.655–1	−6.715–3
	6p <sub>3/2</sub>	1.323–1	1.784+0	3.595–1	2.564–2
	6d <sub>3/2</sub>	3.172–2	1.336+0	1.184+0	1.136–1
	7s <sub>1/2</sub>	9.353–3	1.842+0	−1.358–1	−8.126–3
93	4s <sub>1/2</sub>	1.252+0	1.831+0	−1.299–1	−9.276–3
	4p <sub>1/2</sub>	1.627+0	1.647+0	2.815–1	−4.420–3
	4p <sub>3/2</sub>	2.899+0	1.769+0	3.745–1	3.024–2

Table 2 (continued)

Z	Shell	$\sigma$	$\beta$	$\gamma$	$\delta$
	4d <sub>3/2</sub>	1.846+0	1.321+0	1.219+0	1.255–1
	4d <sub>5/2</sub>	2.355+0	1.153+0	1.247+0	1.464–1
	4f <sub>5/2</sub>	3.463–1	7.450–1	1.472+0	3.523–1
	4f <sub>7/2</sub>	4.165–1	7.111–1	1.464+0	3.708–1
	5s <sub>1/2</sub>	4.028–1	1.831+0	–1.253–1	–8.747–3
	5p <sub>1/2</sub>	4.775–1	1.670+0	2.501–1	–6.953–3
	5p <sub>3/2</sub>	8.229–1	1.783+0	3.417–1	2.671–2
	5d <sub>3/2</sub>	4.343–1	1.343+0	1.168+0	1.139–1
	5d <sub>5/2</sub>	5.464–1	1.171+0	1.200+0	1.338–1
	5f <sub>5/2</sub>	4.036–2	7.537–1	1.449+0	3.394–1
	6s <sub>1/2</sub>	8.781–2	1.831+0	–1.239–1	–8.628–3
	6p <sub>1/2</sub>	8.818–2	1.676+0	2.428–1	–7.535–3
	6p <sub>3/2</sub>	1.391–1	1.786+0	3.344–1	2.601–2
	6d <sub>3/2</sub>	3.373–2	1.347+0	1.160+0	1.120–1
93	7s <sub>1/2</sub>	9.529–3	1.831+0	–1.232–1	–8.598–3
	4s <sub>1/2</sub>	1.268+0	1.818+0	–1.157–1	–9.823–3
	4p <sub>1/2</sub>	1.663+0	1.651+0	2.594–1	–5.290–3
	4p <sub>3/2</sub>	2.988+0	1.770+0	3.496–1	3.075–2
	4d <sub>3/2</sub>	1.943+0	1.331+0	1.196+0	1.244–1
	4d <sub>5/2</sub>	2.476+0	1.161+0	1.231+0	1.442–1
	4f <sub>5/2</sub>	3.790–1	7.532–1	1.471+0	3.490–1
	4f <sub>7/2</sub>	4.554–1	7.182–1	1.465+0	3.673–1
	5s <sub>1/2</sub>	4.157–1	1.818+0	–1.112–1	–9.249–3
	5p <sub>1/2</sub>	4.980–1	1.675+0	2.282–1	–7.773–3
	5p <sub>3/2</sub>	8.643–1	1.784+0	3.170–1	2.711–2
	5d <sub>3/2</sub>	4.686–1	1.354+0	1.143+0	1.125–1
	5d <sub>5/2</sub>	5.887–1	1.180+0	1.183+0	1.313–1
	5f <sub>5/2</sub>	4.731–2	7.626–1	1.447+0	3.353–1
	6s <sub>1/2</sub>	9.114–2	1.818+0	–1.098–1	–9.119–3
	6p <sub>1/2</sub>	9.236–2	1.680+0	2.210–1	–8.354–3
	6p <sub>3/2</sub>	1.457–1	1.788+0	3.097–1	2.639–2
	6d <sub>3/2</sub>	3.555–2	1.358+0	1.134+0	1.106–1
94	7s <sub>1/2</sub>	9.675–3	1.818+0	–1.090–1	–9.083–3
	4s <sub>1/2</sub>	1.284+0	1.805+0	–9.966–2	–1.040–2
	4p <sub>1/2</sub>	1.699+0	1.654+0	2.376–1	–6.190–3
	4p <sub>3/2</sub>	3.080+0	1.770+0	3.247–1	3.124–2
	4d <sub>3/2</sub>	2.044+0	1.340+0	1.172+0	1.234–1
	4d <sub>5/2</sub>	2.603+0	1.170+0	1.215+0	1.419–1
	4f <sub>5/2</sub>	4.145–1	7.615–1	1.471+0	3.458–1
	4f <sub>7/2</sub>	4.976–1	7.254–1	1.467+0	3.638–1
	5s <sub>1/2</sub>	4.280–1	1.805+0	–9.517–2	–9.775–3
	5p <sub>1/2</sub>	5.177–1	1.679+0	2.069–1	–8.618–3
	5p <sub>3/2</sub>	9.040–1	1.785+0	2.926–1	2.749–2
	5d <sub>3/2</sub>	5.013–1	1.364+0	1.117+0	1.112–1
	5d <sub>5/2</sub>	6.282–1	1.190+0	1.164+0	1.288–1
	5f <sub>5/2</sub>	5.113–2	7.717–1	1.444+0	3.313–1
	6s <sub>1/2</sub>	9.161–2	1.805+0	–9.366–2	–9.632–3
	6p <sub>1/2</sub>	9.238–2	1.685+0	1.996–1	–9.181–3
	6p <sub>3/2</sub>	1.435–1	1.788+0	2.853–1	2.675–2
95	7s <sub>1/2</sub>	8.449–3	1.805+0	–9.276–2	–9.588–3
	4s <sub>1/2</sub>	1.298+0	1.790+0	–8.181–2	–1.100–2
	4p <sub>1/2</sub>	1.733+0	1.657+0	2.169–1	–7.076–3
	4p <sub>3/2</sub>	3.170+0	1.770+0	3.008–1	3.174–2
	4d <sub>3/2</sub>	2.146+0	1.349+0	1.147+0	1.226–1
	4d <sub>5/2</sub>	2.731+0	1.179+0	1.198+0	1.399–1
	4f <sub>5/2</sub>	4.517–1	7.696–1	1.469+0	3.425–1
	4f <sub>7/2</sub>	5.417–1	7.324–1	1.467+0	3.604–1
	5s <sub>1/2</sub>	4.403–1	1.791+0	–7.749–2	–1.032–2
	5p <sub>1/2</sub>	5.377–1	1.683+0	1.867–1	–9.448–3
	5p <sub>3/2</sub>	9.465–1	1.785+0	2.691–1	2.787–2
	5d <sub>3/2</sub>	5.381–1	1.374+0	1.091+0	1.101–1
95	5d <sub>5/2</sub>	6.735–1	1.200+0	1.146+0	1.264–1
	5f <sub>5/2</sub>	5.926–2	7.806–1	1.440+0	3.274–1
	5f <sub>7/2</sub>	6.850–2	7.418–1	1.441+0	3.449–1

Table 2 (continued)

Z	Shell	$\sigma$	$\beta$	$\gamma$	$\delta$
	6s <sub>1/2</sub>	9.468–2	1.790+0	–7.592–2	–1.016–2
	6p <sub>1/2</sub>	9.627–2	1.689+0	1.794–1	–1.000–2
	6p <sub>3/2</sub>	1.495–1	1.788+0	2.619–1	2.711–2
	7s <sub>1/2</sub>	8.535–3	1.790+0	–7.498–2	–1.012–2
96	4s <sub>1/2</sub>	1.310+0	1.775+0	–6.225–2	–1.162–2
	4p <sub>1/2</sub>	1.764+0	1.660+0	1.975–1	–7.963–3
	4p <sub>3/2</sub>	3.259+0	1.769+0	2.778–1	3.223–2
	4d <sub>3/2</sub>	2.247+0	1.357+0	1.123+0	1.219–1
	4d <sub>5/2</sub>	2.858+0	1.187+0	1.182+0	1.379–1
	4f <sub>5/2</sub>	4.904–1	7.775–1	1.466+0	3.394–1
	4f <sub>7/2</sub>	5.875–1	7.392–1	1.467+0	3.571–1
	5s <sub>1/2</sub>	4.525–1	1.776+0	–5.819–2	–1.089–2
	5p <sub>1/2</sub>	5.577–1	1.686+0	1.677–1	–1.028–2
	5p <sub>3/2</sub>	9.915–1	1.784+0	2.468–1	2.824–2
	5d <sub>3/2</sub>	5.788–1	1.383+0	1.065+0	1.091–1
	5d <sub>5/2</sub>	7.242–1	1.209+0	1.128+0	1.241–1
	5f <sub>5/2</sub>	7.198–2	7.894–1	1.436+0	3.235–1
	5f <sub>7/2</sub>	8.375–2	7.493–1	1.440+0	3.407–1
	6s <sub>1/2</sub>	1.003–1	1.775+0	–5.660–2	–1.072–2
	6p <sub>1/2</sub>	1.041–1	1.693+0	1.605–1	–1.083–2
	6p <sub>3/2</sub>	1.641–1	1.788+0	2.396–1	2.744–2
	6d <sub>3/2</sub>	4.026–2	1.388+0	1.055+0	1.070–1
	7s <sub>1/2</sub>	1.004–2	1.775+0	–5.565–2	–1.067–2
97	4s <sub>1/2</sub>	1.322+0	1.759+0	–4.046–2	–1.227–2
	4p <sub>1/2</sub>	1.794+0	1.662+0	1.785–1	–8.893–3
	4p <sub>3/2</sub>	3.349+0	1.768+0	2.552–1	3.270–2
	4d <sub>3/2</sub>	2.354+0	1.365+0	1.097+0	1.214–1
	4d <sub>5/2</sub>	2.992+0	1.196+0	1.165+0	1.359–1
	4f <sub>5/2</sub>	5.320–1	7.853–1	1.464+0	3.364–1
	4f <sub>7/2</sub>	6.369–1	7.461–1	1.467+0	3.537–1
	5s <sub>1/2</sub>	4.642–1	1.759+0	–3.677–2	–1.148–2
	5p <sub>1/2</sub>	5.769–1	1.689+0	1.494–1	–1.115–2
	5p <sub>3/2</sub>	1.035+0	1.783+0	2.247–1	2.857–2
	5d <sub>3/2</sub>	6.183–1	1.392+0	1.038+0	1.083–1
	5d <sub>5/2</sub>	7.724–1	1.219+0	1.109+0	1.218–1
	5f <sub>5/2</sub>	8.171–2	7.982–1	1.432+0	3.196–1
	5f <sub>7/2</sub>	9.494–2	7.570–1	1.438+0	3.366–1
	6s <sub>1/2</sub>	1.032–1	1.759+0	–3.515–2	–1.129–2
	6p <sub>1/2</sub>	1.078–1	1.696+0	1.423–1	–1.168–2
	6p <sub>3/2</sub>	1.701–1	1.786+0	2.176–1	2.774–2
	6d <sub>3/2</sub>	4.163–2	1.397+0	1.027+0	1.061–1
	7s <sub>1/2</sub>	1.014–2	1.759+0	–3.421–2	–1.124–2
98	4s <sub>1/2</sub>	1.333+0	1.742+0	–1.630–2	–1.295–2
	4p <sub>1/2</sub>	1.823+0	1.664+0	1.602–1	–9.874–3
	4p <sub>3/2</sub>	3.442+0	1.765+0	2.327–1	3.314–2
	4d <sub>3/2</sub>	2.465+0	1.372+0	1.070+0	1.209–1
	4d <sub>5/2</sub>	3.132+0	1.204+0	1.147+0	1.340–1
	4f <sub>5/2</sub>	5.770–1	7.932–1	1.462+0	3.335–1
	4f <sub>7/2</sub>	6.902–1	7.529–1	1.467+0	3.506–1
	5s <sub>1/2</sub>	4.754–1	1.742+0	–1.307–2	–1.209–2
	5p <sub>1/2</sub>	5.951–1	1.692+0	1.318–1	–1.207–2
	5p <sub>3/2</sub>	1.077+0	1.780+0	2.030–1	2.887–2
	5d <sub>3/2</sub>	6.564–1	1.400+0	1.009+0	1.075–1
	5d <sub>5/2</sub>	8.180–1	1.228+0	1.090+0	1.196–1
	5f <sub>5/2</sub>	8.786–2	8.071–1	1.427+0	3.159–1
	5f <sub>7/2</sub>	1.013–1	7.647–1	1.436+0	3.326–1
	6s <sub>1/2</sub>	1.032–1	1.741+0	–1.144–2	–1.189–2
	6p <sub>1/2</sub>	1.071–1	1.699+0	1.248–1	–1.258–2
	6p <sub>3/2</sub>	1.662–1	1.784+0	1.959–1	2.801–2
	7s <sub>1/2</sub>	8.719–3	1.741+0	–1.049–2	–1.183–2
99	4s <sub>1/2</sub>	1.342+0	1.723+0	9.758–3	–1.366–2
	4p <sub>1/2</sub>	1.848+0	1.666+0	1.432–1	–1.087–2
	4p <sub>3/2</sub>	3.533+0	1.762+0	2.113–1	3.355–2

(continued on next page)

Table 2 (continued)

Z	Shell	$\sigma$	$\beta$	$\gamma$	$\delta$
	4d <sub>3/2</sub>	2.577+0	1.378+0	1.043+0	1.206–1
	4d <sub>5/2</sub>	3.270+0	1.212+0	1.129+0	1.321–1
	4f <sub>5/2</sub>	6.236–1	8.009–1	1.458+0	3.307–1
	4f <sub>7/2</sub>	7.452–1	7.596–1	1.466+0	3.475–1
	5s <sub>1/2</sub>	4.865–1	1.723+0	1.241–2	–1.273–2
	5p <sub>1/2</sub>	6.133–1	1.695+0	1.156–1	–1.300–2
	5p <sub>3/2</sub>	1.121+0	1.777+0	1.825–1	2.914–2
	5d <sub>3/2</sub>	6.982–1	1.408+0	9.814–1	1.069–1
	5d <sub>5/2</sub>	8.691–1	1.237+0	1.070+0	1.174–1
	5f <sub>5/2</sub>	9.895–2	8.158–1	1.422+0	3.122–1
	5f <sub>7/2</sub>	1.139–1	7.722–1	1.433+0	3.285–1
	6s <sub>1/2</sub>	1.058–1	1.723+0	1.402–2	–1.251–2
	6p <sub>1/2</sub>	1.105–1	1.702+0	1.088–1	–1.349–2
	6p <sub>3/2</sub>	1.715–1	1.781+0	1.755–1	2.824–2
	7s <sub>1/2</sub>	8.762–3	1.723+0	1.492–2	–1.245–2
100	4s <sub>1/2</sub>	1.350+0	1.704+0	3.807–2	–1.439–2
	4p <sub>1/2</sub>	1.871+0	1.667+0	1.273–1	–1.192–2
	4p <sub>3/2</sub>	3.622+0	1.758+0	1.908–1	3.394–2
	4d <sub>3/2</sub>	2.690+0	1.384+0	1.015+0	1.204–1
	4d <sub>5/2</sub>	3.411+0	1.220+0	1.111+0	1.303–1
	4f <sub>5/2</sub>	6.729–1	8.085–1	1.455+0	3.279–1
	4f <sub>7/2</sub>	8.033–1	7.662–1	1.465+0	3.444–1
	5s <sub>1/2</sub>	4.971–1	1.703+0	4.002–2	–1.339–2
	5p <sub>1/2</sub>	6.309–1	1.697+0	1.007–1	–1.398–2
	5p <sub>3/2</sub>	1.166+0	1.774+0	1.628–1	2.936–2
	5d <sub>3/2</sub>	7.412–1	1.415+0	9.528–1	1.065–1
	5d <sub>5/2</sub>	9.216–1	1.246+0	1.051+0	1.153–1
	5f <sub>5/2</sub>	1.109–1	8.245–1	1.416+0	3.085–1
	5f <sub>7/2</sub>	1.274–1	7.797–1	1.430+0	3.245–1
	6s <sub>1/2</sub>	1.084–1	1.703+0	4.157–2	–1.314–2
	6p <sub>1/2</sub>	1.137–1	1.705+0	9.405–2	–1.447–2
	6p <sub>3/2</sub>	1.766–1	1.777+0	1.560–1	2.842–2
	7s <sub>1/2</sub>	8.798–3	1.703+0	4.243–2	–1.307–2